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# THERMODYNAMIC AND TRANSPORT PROPERTIES OF GASEOUS TETRAFLUOROMETHANE IN CHEMICAL EQUILIBRIUM

by James L. Hunt and Lillian R. Boney Langley Research Center Hampton, Va. 23665

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#### **ERRATA**

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The reference enthalpy  $(4.6489 \times 10^5 \ \mathrm{Jkg^{-1}})$  and the reference entropy  $(3.548 \times 10^3 \ \mathrm{Jkg^{-1}K^{-1}})$  used in the subject report are in error. The correct reference enthalpy is  $4.6571 \times 10^5 \ \mathrm{Jkg^{-1}}$  and the correct reference entropy is  $3.542 \ \mathrm{Jkg^{-1}K^{-1}}$ .

The enthalpy equation for  $CF_4$  (eq. (8), p. 9) contains erroneous terms. For values of specific volume V above  $0.030~\rm m^3kg^{-1}$ , the error in enthalpy is negligible. Between  $V = 0.030~\rm and~0.0055~\rm m^3kg^{-1}$ , the error in enthalpy is of the order of 0.5 percent. For the range of V from  $0.0055~\rm to~0.0026~\rm m^3kg^{-1}$ , the error increases up to a maximum of 4.5 percent at  $V = 0.0026~\rm m^3kg^{-1}$ . All errors are positive (that is, too large).

In equation (8) beginning with line 6, replace the following terms within braces

$$+ \left\{ \frac{V^{2}}{2} \left[ \frac{-4B_{4}T}{(V-b)^{5}} + A_{6}\alpha e^{\alpha V} + B_{6}T\alpha e^{\alpha V} \right] + V \left[ \frac{B_{4}T}{(V-b)^{4}} + A_{6}e^{\alpha V} + B_{6}Te^{\alpha V} \right] - \frac{V_{r}^{2}}{2} \left[ \frac{-4B_{4}T}{(V_{r}-b)^{5}} + A_{6}\alpha e^{\alpha V_{r}} + B_{6}T\alpha e^{\alpha V_{r}} \right] - V_{r} \left[ \frac{B_{4}T}{(V_{r}-b)^{4}} + A_{6}e^{\alpha V_{r}} + B_{6}Te^{\alpha V_{r}} \right] \right\}$$

with

$$\begin{split} &-4 \mathbf{B_4 T} \left[ \frac{1}{3 \left(\mathbf{V_r} - \mathbf{b}\right)^3} + \frac{\mathbf{b}}{4 \left(\mathbf{V_r} - \mathbf{b}\right)^4} - \frac{1}{3 (\mathbf{V} - \mathbf{b})^3} - \frac{\mathbf{b}}{4 (\mathbf{V} - \mathbf{b})^4} \right] \\ &+ \left( \mathbf{A_6} + \mathbf{B_6 T} \right) \left[ \frac{\mathbf{e}^{\alpha \mathbf{V}} (\alpha \mathbf{V} - \mathbf{1}) - \mathbf{e}^{\alpha \mathbf{V}} \mathbf{r} \left(\alpha \mathbf{V_r} - \mathbf{1}\right)}{\alpha} \right] \end{split}$$

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# THERMODYNAMIC AND TRANSPORT PROPERTIES OF GASEOUS TETRAFLUOROMETHANE IN CHEMICAL EQUILIBRIUM

By James L. Hunt and Lillian R. Boney Langley Research Center

#### SUMMARY

Equations and computer code are presented for the thermodynamic and transport properties of gaseous, undissociated tetrafluoromethane  $(CF_4)$  in chemical equilibrium. The computer code calculates the thermodynamic and transport properties of  $CF_4$  when given any two of five thermodynamic variables (entropy, temperature, volume, pressure, and enthalpy).

Equilibrium thermodynamic and transport property data are tabulated for gaseous CF<sub>4</sub> from a dimensionless entropy S/R of 24.0 to 46.0 and from a temperature of 89.45 K to 845 K. These data are listed at constant entropy in increments of 0.25 with temperature increments of 10 K. Pressure-enthalpy diagrams generated with data from the computer code which contain lines of constant entropy, temperature, volume, speed of sound, isentropic expansion exponent, and compressibility factor are presented. Transport property and specific heat data are also tabulated over a specific volume range from  $0.002~\mathrm{m}^3\mathrm{kg}^{-1}$  to 80 m $^3\mathrm{kg}^{-1}$  for five values of temperature from 100 K to 800 K.

#### INTRODUCTION

Tetrafluoromethane is currently being used in hypersonic tunnels at enthalpy levels below that at which dissociation occurs to simulate the inviscid flow field on blunt or lifting bodies in hypersonic flight where dissociation of the gas in the shock layer does occur. (See ref. 1.) This use of gaseous  $CF_4$  has generated interest in the thermodynamic and transport properties of  $CF_4$  in a higher enthalpy range and different form than that presently available (ref. 2) which covers the range of conditions where tetrafluoromethane is normally expected to be used as a refrigerant. Also, more recent and extensive pressure-volume-temperature measurements (information received from E. I. du Pont de Nemours & Co. as generated by Dr. J. J. Martin of the University of Michigan) resulted in an equation of state somewhat different from that used in reference 2.

Equations and computer code are presented for the thermodynamic and transport properties of gaseous, undissociated tetrafluoromethane (CF4) in chemical equilibrium.

The computer code calculates the thermodynamic and transport properties of CF<sub>4</sub> when given any two of five thermodynamic variables (entropy, temperature, volume, pressure, and enthalpy).

Equilibrium thermodynamic and transport property data are tabulated for gaseous CF4 from a dimensionless entropy (S/R) of 24.0 to 46.0 and from a temperature of 89.45 K to 845 K. These data are listed at constant entropy in increments of 0.25 with temperature increments of 10 K. Pressure-enthalpy diagrams generated with data from the computer codes are presented which contain lines of constant entropy, temperature, volume, speed of sound, isentropic expansion exponent, and compressibility factor. Transport property and specific heat data are also tabulated over a specific volume range from 0.002  $\rm m^3kg^{-1}$  to 80  $\rm m^3kg^{-1}$  for five values of temperature from 100 K to 800 K.

#### SYMBOLS

A	constant in saturation pressure equation (eq. (16))
A <sub>2</sub> ,A <sub>3</sub> ,A <sub>4</sub> ,A <sub>5</sub> ,A <sub>6</sub>	constants in equation of state (eq. (1))
a	speed of sound
a <sub>4</sub>	constant in equation for specific heat at zero pressure (eq. (3))
В	constant in saturation pressure equation (eq. (16))
B <sub>2</sub> ,B <sub>3</sub> ,B <sub>4</sub> ,B <sub>5</sub> ,B <sub>6</sub>	constants in equation of state (eq. (1))
b	constant in equation of state (eq. (1))
<b>b</b> <sub>4</sub>	constant in equation for specific heat at zero pressure (eq. (3))
C	constant in saturation pressure equation (eq. (16))
$c_2,c_3,c_5$	constants in equation of state (eq. (1))
<b>c</b> <sub>4</sub>	constant in equation for specific heat at zero pressure (eq. (3))
$c_{\mathbf{p}}$	specific heat at constant pressure

c <sub>p</sub> '	ideal-gas specific heat at constant pressure
$\mathbf{c}_{\mathbf{v}}$	specific heat at constant volume
c <sub>v</sub> '	ideal-gas specific heat at constant volume
<b>D</b>	constant in saturation pressure (eq. (16))
$d_4$	constant in equation for specific heat at zero pressure (eq. (3))
E	constant in saturation pressure equation (eq. (16))
F	constant in saturation pressure equation (eq. (16))
f	functional notation
G	constant in equation (16)
Н	enthalpy
J	unit conversion factor
<b>K</b> '	constant in equation of state (eq. (1))
k	thermal conductivity
<b>k</b> *	thermal conductivity at atmospheric pressure
M	molecular weight
m,n	exponents in equation (18)
$N_{\mathbf{Pr}}$	Prandtl number, $\mu c_{ m p}/{ m k}$
p	pressure
R	gas constant
<b>S</b> -	entropy

```
\mathbf{T}
                     temperature
                     specific volume
\mathbf{v}
\mathbf{Z}
                     compressibility factor, pV/RT
                     constant in equation of state (eq. (1))
\alpha
                     proportionality constant (eq. (18))
β
                     ratio of specific heats, \ c_p/c_v
γ
                     isentropic exponent (eq. (12))
\gamma_{\mathbf{e}}
                     viscosity
\mu
\mu^*
                     viscosity at atmospheric pressure
                     viscosity parameter, T_c^{1/6}/M^{1/2}p_c^{2/3}
ξ
                     density, 1/V
ρ
                     reduced density, V_c/V
^{
ho}{
m R}
Subscripts:
                     critical
C,
                     ice point of water, 273.15 K
                     reference conditions (eq. (5))
\mathbf{r}
                     saturation
s
```

#### CHARACTERISTICS

Tetrafluoromethane  $(CF_4)$  is a nonlinear polyatomic molecule (ref. 3). Its nine vibrational energy modes (ref. 3) display anharmonic oscillator characteristics having four fundamental frequencies; two are threefold degenerate, one is twofold degenerate,

and one is onefold degenerate. The acute temperature dependence of the vibrational energy of this molecule reveals itself in the specific heats at constant pressure and volume and their ratio  $\gamma$  along with the isentropic expansion exponent.

In the gaseous state, tetrafluoromethane is colorless, odorless, and nontoxic. It has a low ratio of specific heats, low boiling point, and short vibrational relaxation time. (See ref. 4.) Some of the physical properties of  $CF_4$  (obtained from E. I. du Pont de Nemours & Co.) are given in the following table. (Note that 1 atmosphere = 101 kN m<sup>-2</sup>.)

Molecular weight
Boiling point at 1 atm, K
Freezing point, K
Critical temperature, K
Critical pressure, atm
Critical volume, $cm^3mole^{-1}$
Critical density, $kg m^{-3} \dots \dots$
Density, liquid at 193 K, $kg m^{-3}$
Density, saturated vapors at boiling point, kg m <sup>-3</sup> 7.62
Specific heat, liquid at 193 K, $J kg^{-1}K^{-1} \dots \dots$
Specific heat, vapor at 1 atm and 298 K, J kg <sup>-1</sup> K <sup>-1</sup>
Specific-heat ratio at 1 atm and 298 K
Heat of vaporization at boiling point, $J kg^{-1} \dots 136.0 \times 10^3$
Vibrational relaxation time at 298 K and 1 atm, sec $\dots \dots \dots$

The method of reference 5 was used to compute the equilibrium composition of CF<sub>4</sub> as a function of temperature for several pressures covering the range that would normally be used in a wind tunnel, and it was found that no dissociation occurred for temperatures lower than 1600 K.

#### GENERAL EQUATIONS

#### Thermodynamic Properties of Gaseous CF<sub>4</sub>

The equation of state of tetrafluoromethane was obtained from E. I du Pont de Nemours & Co. and is

$$p = \frac{RT}{V - b} + \frac{A_2 + B_2T + C_2e^{-KT}}{(V - b)^2} + \frac{A_3 + B_3T + C_3e^{-KT}}{(V - b)^3} + \frac{A_4 + B_4T}{(V - b)^4} + \frac{A_5 + B_5T + C_5e^{-KT}}{(V - b)^5} + (A_6 + B_6T)e^{\alpha V}$$
(1)

where p is given in  $N m^{-2}$ , V in  $m^3 kg^{-1}$ , and T in K, and where the virial coefficients are

$$A_2 = -5.811999 \times 10^1$$

$$B_2 = 1.032692 \times 10^{-1}$$

$$C_2 = -5.089595 \times 10^2$$

$$A_3 = 7.387702 \times 10^{-3}$$

$$B_3 = 3.873415 \times 10^{-5}$$

$$C_3 = 9.054616 \times 10^{-1}$$

$$A_4 = 2.01177417 \times 10^{-5}$$

$$B_4 = -7.385870 \times 10^{-8}$$

$$A_5 = -2.929506 \times 10^{-8}$$

$$B_5 = 1.066416 \times 10^{-10}$$

$$C_5 = -3.162000 \times 10^{-7}$$

$$A_6 = 4.0257244 \times 10^{11}$$

$$B_6 = -1.149705 \times 10^9$$

and

$$R = 9.447002 \times 10^{1} \,\mathrm{J\,kg^{-1}K^{-1}}$$

$$b = 9.364194 \times 10^{-5}$$

$$K = 1.758236 \times 10^{-2}$$

$$\alpha = -1.059139 \times 10^4$$

This equation was developed through an empirical approach (ref. 6) in which the 13 virial coefficients and  $\alpha$  and b were evaluated along the experimentally determined critical isotherm by Dr. J. J. Martin of the University of Michigan. This equation probably gives an accurate representation of the pressure-volume-temperature behavior of CF<sub>4</sub> at densities as high as 1.5 times the critical value. Dr. Martin (ref. 7) has since developed

an equation of state which gives an accurate representation of the pressure-volume-temperature behavior of  $CF_4$  at densities as high as 2.5 times the critical value. The specific heat at constant volume is

$$c_{V} = c_{V}' + J \int_{\infty}^{V} T \left( \frac{\partial^{2} p}{\partial T^{2}} \right)_{V} dV$$
 (2)

Two third-degree expressions in temperature were obtained from P. E. Liley of Thermophysical Properties Research Center, Purdue University, for the ideal-gas specific heat  $c_p$ '. These expressions were curve fits of spectroscopic and molecular structural data derived from statistical mechanics which were compiled from six sources. These two expressions for the ideal-gas specific heat at constant pressure were converted to specific heat at constant volume by the ideal-gas relationship  $c_v$ ' =  $c_p$ ' - R. The equation for specific heat at constant volume at zero pressure is

$$c_{v}' = a_4 + b_4 T + c_4 T^2 + d_4 T^3$$
(3)

where  $c_v$ ' is in  $J \, \mathrm{kg}^{-1} \mathrm{K}^{-1}$ . When equation (3) is fitted over the temperature interval 100 K to 615 K:

$$a_A = 1.43308 \times 10^2$$

$$b_4 = 1.51168 \times 10^0$$

$$c_4 = 5.15767 \times 10^{-4}$$

$$d_4 = -1.59381 \times 10^{-6}$$

When equation (3) is fitted over the temperature interval 615 K to 1500 K:

$$a_4 = 2.95790 \times 10^2$$

$$b_4 = 1.53754 \times 10^0$$

$$c_4 = -1.0727 \times 10^{-3}$$

$$d_4 = 2.64172 \times 10^{-7}$$

These curve fits are stated to fit the enumerated values with mean deviations of 0.66 and 0.09 percent and maximum deviations of 3.6 and 0.27 percent, respectively.

Evaluating the integral term of equation (2) with the equation of state (1) gives

$$c_{v} = c_{v}' - TK^{2}e^{-KT} \left[ \frac{C_{2}}{V - b} + \frac{C_{3}}{2(V - b)^{2}} + \frac{C_{5}}{4(V - b)^{4}} \right]$$
 (4)

The entropy S expressed as a function of T and V is

$$S - S_{r} = \int_{T_{r}}^{T} \frac{c_{V}}{T} dT + \int_{V_{r}}^{V} \left(\frac{\partial p}{\partial T}\right)_{V} dV$$
 (5)

where the subscript r represents reference conditions taken herein as

$$S_r = 3.548 \times 10^3 \text{ J kg}^{-1} \text{K}^{-1}$$

$$T_r = 4.556 \times 10^2 \text{ K}$$

$$p_{r} = 6.8948 \times 10^{3} \text{ N m}^{-2}$$

$$V_r = 6.2428 \text{ m}^3\text{kg}^{-1}$$

From the integration of equation (5), the expression for entropy becomes

$$S - S_{r} = a_{4} \log_{e} \frac{T}{T_{r}} + b_{4} (T - T_{r}) + \frac{c_{4}}{2} (T^{2} - T_{r}^{2}) + \frac{d_{4}}{3} (T^{3} - T_{r}^{3})$$

$$+ K(e^{-KT} - e^{-KT}r) \left[ \frac{C_{2}}{V_{r} - b} + \frac{C_{3}}{2(V_{r} - b)^{2}} + \frac{C_{5}}{4(V_{r} - b)^{4}} \right] + R \log_{e} \left( \frac{V - b}{V_{r} - b} \right)$$

$$- \left( B_{2} - KC_{2}e^{-KT} \right) \left( \frac{1}{V - b} - \frac{1}{V_{r} - b} \right) - \frac{B_{3} - KC_{3}e^{-KT}}{2} \left[ \frac{1}{(V - b)^{2}} - \frac{1}{(V_{r} - b)^{2}} \right]$$

$$- \frac{B_{5} - KC_{5}e^{-KT}}{4} \left[ \frac{1}{(V - b)^{4}} - \frac{1}{(V_{r} - b)^{4}} \right] - B_{4} \left[ \frac{1}{3(V - b)^{3}} - \frac{1}{3(V_{r} - b)^{3}} \right]$$

$$+ B_{6} \left( \frac{e^{\alpha V}}{\alpha} - \frac{e^{\alpha V_{r}}}{\alpha} \right)$$

$$(6)$$

The enthalpy H expressed as a function of T and V is

$$\mathbf{H} - \mathbf{H_r} = \int_{\mathbf{T_r}}^{\mathbf{T}} \left[ \mathbf{c_V} + \mathbf{V} \left( \frac{\partial \mathbf{p}}{\partial \mathbf{T}} \right)_{\mathbf{V}} \right] d\mathbf{T} + \int_{\mathbf{V_r}}^{\mathbf{V}} \left[ \mathbf{V} \left( \frac{\partial \mathbf{p}}{\partial \mathbf{V}} \right)_{\mathbf{T}} + \mathbf{T} \left( \frac{\partial \mathbf{p}}{\partial \mathbf{T}} \right)_{\mathbf{V}} \right] d\mathbf{V}$$
 (7)

and becomes in integrated form

$$\begin{split} H - H_{\mathbf{r}} &= a_{4} \left( \mathbf{T} - \mathbf{T}_{\mathbf{r}} \right) + b_{4} \frac{\mathbf{T}^{2} - \mathbf{T}_{\mathbf{r}}^{2}}{2} + c_{4} \frac{\mathbf{T}^{3} - \mathbf{T}_{\mathbf{r}}^{3}}{3} + d_{4} \frac{\mathbf{T}^{4} - \mathbf{T}_{\mathbf{r}}^{4}}{4} + \left[ e^{-KT} \left( KT + 1 \right) - e^{-KT} \mathbf{r} \left( KT_{\mathbf{r}} + 1 \right) \right] \left[ \frac{C_{2}}{V_{\mathbf{r}} - \mathbf{b}} + \frac{C_{3}}{2 \left( V_{\mathbf{r}} - \mathbf{b} \right)^{2}} + \frac{C_{5}}{4 \left( V_{\mathbf{r}} - \mathbf{b} \right)^{4}} \right] \\ + V_{\mathbf{r}} \left[ \frac{R}{V_{\mathbf{r}} - \mathbf{b}} \left( \mathbf{T} - \mathbf{T}_{\mathbf{r}} \right) + \frac{B_{2} \left( \mathbf{T} - \mathbf{T}_{\mathbf{r}} \right) + C_{2} \left( e^{-KT} - e^{-KT} \mathbf{r} \right)}{\left( V_{\mathbf{r}} - \mathbf{b} \right)^{2}} + \frac{B_{3} \left( \mathbf{T} - \mathbf{T}_{\mathbf{r}} \right) + C_{3} \left( e^{-KT} - e^{-KT} \mathbf{r} \right)}{\left( V_{\mathbf{r}} - \mathbf{b} \right)^{3}} + \frac{B_{4} \left( \mathbf{T} - \mathbf{T}_{\mathbf{r}} \right)}{\left( V_{\mathbf{r}} - \mathbf{b} \right)^{4}} \\ + \frac{B_{5} \left( \mathbf{T} - \mathbf{T}_{\mathbf{r}} \right) + C_{5} \left( e^{-KT} - e^{-KT} \mathbf{r} \right)}{\left( V_{\mathbf{r}} - \mathbf{b} \right)^{5}} + B_{6} e^{\alpha V_{\mathbf{r}}} \left( \mathbf{T} - \mathbf{T}_{\mathbf{r}} \right) \right] - \left\{ RT \left[ \log_{e} \left( \frac{V - \mathbf{b}}{V_{\mathbf{r}} - \mathbf{b}} \right) + \frac{\mathbf{b}}{V_{\mathbf{r}} - \mathbf{b}} - \frac{\mathbf{b}}{V - \mathbf{b}} \right] \right. \\ + 2 \left( A_{2} + B_{2} \mathbf{T} + C_{2} e^{-KT} \right) \left[ \frac{1}{V_{\mathbf{r}} - \mathbf{b}} + \frac{\mathbf{b}}{2 \left( V_{\mathbf{r}} - \mathbf{b} \right)^{2}} - \frac{1}{V - \mathbf{b}} - \frac{\mathbf{b}}{2 \left( V_{\mathbf{r}} - \mathbf{b} \right)^{2}} \right] + 3 \left( A_{3} + B_{3} \mathbf{T} + C_{3} e^{-KT} \right) \left[ \frac{1}{2 \left( V_{\mathbf{r}} - \mathbf{b} \right)^{3}} - \frac{1}{3 \left( V_{\mathbf{r}} - \mathbf{b} \right)^{3}} - \frac{1}{3 \left( V_{\mathbf{r}} - \mathbf{b} \right)^{3}} - \frac{1}{3 \left( V_{\mathbf{r}} - \mathbf{b} \right)^{3}} \right] \\ + 4A_{4} \left[ \frac{1}{3 \left( V_{\mathbf{r}} - \mathbf{b} \right)^{3}} + \frac{\mathbf{b}}{4 \left( V_{\mathbf{r}} - \mathbf{b} \right)^{4}} - \frac{1}{3 \left( V_{\mathbf{r}} - \mathbf{b} \right)^{3}} - \frac{\mathbf{b}}{4 \left( V_{\mathbf{r}} - \mathbf{b} \right)^{4}} \right] + 5 \left( A_{5} + B_{5} \mathbf{T} + C_{5} e^{-KT} \right) \left[ \frac{1}{4 \left( V_{\mathbf{r}} - \mathbf{b} \right)^{4}} + \frac{\mathbf{b}}{5 \left( V_{\mathbf{r}} - \mathbf{b} \right)^{3}} - \frac{1}{4 \left( V_{\mathbf{r}} - \mathbf{b} \right)^{4}} - \frac{\mathbf{b}}{3 \left( V_{\mathbf{r}} - \mathbf{b} \right)^{3}} \right] \\ + \left( \frac{V^{2}}{2} \left[ \frac{-4B_{4}T}{\left( V_{\mathbf{r}} - \mathbf{b} \right)^{4}} + A_{6} e^{\alpha V} + B_{6} \mathbf{T} \alpha e^{\alpha V} \right] \right) + V \left[ \frac{B_{4}T}{\left( V_{\mathbf{r}} - \mathbf{b} \right)^{4}} + A_{6} e^{\alpha V} + B_{6} \mathbf{T} \alpha e^{\alpha V} \right] \right] + V \left[ \frac{B_{4}T}{\left( V_{\mathbf{r}} - \mathbf{b} \right)^{4}} - \frac{1}{2 \left( V_{\mathbf{r}} - \mathbf{b} \right)^{4}} \right] - \frac{B_{5} - KC_{5} e^{-KT}}{\left( V_{\mathbf{r}} - \mathbf{b} \right)^{4}} \right] - \frac{1}{(V_{\mathbf{r}} - \mathbf{b}} \left( \frac{B_{2}}{2} \right) \right] \\ -$$

where  $H_r = 4.6489 \times 10^5 \,\mathrm{J\,kg^{-1}}$  at reference conditions. (See ref. 2.)

The pressure, entropy, and enthalpy are now expressed as a function of temperature and volume. A computer code (see appendix) was developed which computes all these thermodynamic variables when any two are known. The computer code also calculates specific heat at constant pressure  $c_p$ , ratio of specific heats  $\gamma$ , isentropic exponent  $\gamma_e$ , speed of sound a, and compressibility factor Z at the same thermodynamic point as the first five variables. The equations for these thermodynamic properties are

Specific heat at constant pressure:

$$c_{p} = c_{v} - T \frac{\left[ \left( \frac{\partial p}{\partial T} \right)_{V} \right]^{2}}{\left( \frac{\partial p}{\partial V} \right)_{T}}$$
(9)

Specific heat ratio:

$$\gamma = \frac{c_{p}}{c_{v}} = 1 - \frac{T \left[ \left( \frac{\partial p}{\partial T} \right)_{V} \right]^{2}}{c_{v} \left( \frac{\partial p}{\partial V} \right)_{T}}$$
(10)

Speed of sound:

$$\mathbf{a} = \left[ \left( \frac{\partial \mathbf{p}}{\partial \rho} \right)_{\mathbf{S}} \right]^{1/2} = \left[ \gamma \left( \frac{\partial \mathbf{p}}{\partial \rho} \right)_{\mathbf{T}} \right]^{1/2} = \left[ -\gamma \mathbf{V}^2 \left( \frac{\partial \mathbf{p}}{\partial \mathbf{V}} \right)_{\mathbf{T}} \right]^{1/2} = \left[ \frac{\mathbf{V}^2 \mathbf{T}}{\mathbf{c}_{\mathbf{V}}} \left[ \left( \frac{\partial \mathbf{p}}{\partial \mathbf{T}} \right)_{\mathbf{V}} \right]^2 - \mathbf{V}^2 \left( \frac{\partial \mathbf{p}}{\partial \mathbf{V}} \right)_{\mathbf{T}} \right]^{1/2}$$
(11)

Isentropic exponent:

$$\gamma_{e} = \left(\frac{d \log p}{d \log \rho}\right)_{S} = \frac{\rho}{p} \left(\frac{dp}{d\rho}\right)_{S} = \frac{a^{2}}{pV}$$
(12)

Compressibility factor:

$$Z = \frac{pV}{RT}$$
 (13)

where the partial derivatives in  $c_p$ ,  $\gamma$ , and a are

$$\left(\frac{\partial p}{\partial T}\right)_{V} = \frac{R}{V - b} + \frac{\left(B_{2} - KC_{2}e^{-KT}\right)}{(V - b)^{2}} + \frac{\left(B_{3} - KC_{3}e^{-KT}\right)}{(V - b)^{3}} + \frac{B_{4}}{(V - b)^{4}}$$

$$\left(B_{5} - KC_{5}e^{-KT}\right) + B_{5}\alpha V$$
(1)

$$+\frac{\left(B_{5} - KC_{5}e^{-KT}\right)}{(V - b)^{5}} + B_{6}e^{\alpha V}$$
 (14)

$$\left(\frac{\partial p}{\partial V}\right)_{T} = -\frac{RT}{(V-b)^{2}} - 2\frac{\left(A_{2} + B_{2}T + C_{2}e^{-KT}\right)}{(V-b)^{3}} - \frac{3\left(A_{3} + B_{3}T + C_{3}e^{-KT}\right)}{(V-b)^{4}}$$

$$-\frac{4(A_4 + B_4T)}{(V - b)^5} - \frac{5(A_5 + B_5T + C_5e^{-KT})}{(V - b)^6} + \alpha(A_6 + B_6T)e^{\alpha V}$$
 (15)

These equations are limited to temperatures above the saturated vapor line. The saturation pressure in  $N m^{-2}$  as a function of saturation temperature in kelvins is (ref. 2):

$$\log p = A + \frac{B}{T} + C \log T + DT + E\left(\frac{F - T}{T}\right) \log (F - T) + G$$
 (16)

where

A = 20.71545389

B = -2467.505285

C = -4.69017025

 $D = 6.4798076 \times 10^{-4}$ 

E = 0.770707795

F = 424

G = 3.83852

The critical temperature  $T_c$  is 227.48 K. Equations (1) to (15) are also limited to temperatures below those at which dissociation occurs (T < 1600 K).

#### Transport Properties of Gaseous CF<sub>4</sub>

Viscosity. Five sources of experimental data for the viscosity of  $CF_4$  at a pressure of 1 atmosphere were fitted to a quadratic equation in 1/T by P. E. Liley of Purdue University. The data covered a temperature range from 230 K to 460 K. The agreement of the data of the various sets was stated to be generally good and the accuracy was thought to be  $\pm 2$  percent over the aforementioned temperature range. The empirical equation is

$$\mu^* = \frac{\sqrt{T}}{0.64625 + \frac{103.00}{T} - \frac{3.42714}{T^2}} \times 10^{-6}$$
 (17)

where  $\mu^*$  is in Nsm<sup>-2</sup>. The viscosity of CF<sub>4</sub> at a pressure of 1 atmosphere determined from this equation is plotted over a temperature range of 150 K to 800 K in figure 1. Even though the curve fit was only made for a temperature interval of 230 K to 460 K, equation (1) behaves well over the extended range. To obtain the viscosity of CF<sub>4</sub> at pressures other than 1 atmosphere, the residual viscosity is expressed as a function of the density, molecular weight, and critical constants of the substance (ref. 8) through a dimensional

analysis treatment, and the correct dependencies are established by the use of experimental data. The dimensional analysis treatment (ref. 8) resulted in the following expression:

$$(\mu - \mu^*)\xi = \frac{\beta}{R^{1/6}} Z_c^m \rho_R^n$$
 (18)

Experimental high-pressure viscosities for the gaseous and liquid phases available in the literature for 14 polar substances including 5 Freons (CCl<sub>3</sub>F, CCl<sub>2</sub>F<sub>2</sub>, CHCl<sub>2</sub>F, CHClF<sub>2</sub>, and C<sub>2</sub>Cl<sub>3</sub>F<sub>3</sub>) were used (ref. 9) in conjunction with pressure-volume-temperature data to establish the constant  $\beta$  and the exponents m and n of equation (18). Plots of  $(\mu - \mu^*)\xi$  against  $\rho_{\mathbf{R}}$  (ref. 9) were found to be essentially the same for all 14 substances; therefore, it was concluded that the exponent m of  $\mathbf{Z}_{\mathbf{C}}$  in equation (18) was zero. The analytical representation of the residual viscosity correlation for the 14 polar substances (ref. 9) which should apply to CF<sub>4</sub> as well are

$$(\mu - \mu^*)\xi = 16.56 \times 10^{-8} \rho_{\mathbf{R}}^{1.111} \qquad (\rho_{\mathbf{R}} \le 0.10)$$

$$(\mu - \mu^*)\xi = 0.607 \times 10^{-8} (9.045\rho_{\mathbf{R}} + 0.63)^{1.739} \qquad (0.10 < \rho_{\mathbf{R}} \le 0.90)$$

$$-\log[(\mu - \mu^*)\xi] = 10^{0.6439 - 0.1005\rho_{\mathbf{R}} - \Delta} + 3 \qquad (0.9 < \rho_{\mathbf{R}} < 2.6)$$

where  $\Delta = 0$  for  $0.9 < \rho_{\rm R} < 2.2$  and  $\Delta = 4.75 \times 10^{-4} \left( \rho_{\rm R}^{-3} - 10.65 \right)^2$  for  $2.2 < \rho_{\rm R} < 2.6$  and  $\xi = {\rm T}^{1/6} / {\rm M}^{1/2} \, {\rm p_c}^{2/3} = 0.023735$  for CF<sub>4</sub> with  $\mu$  in N s m<sup>-2</sup>.

Thermal conductivity. The thermal conductivity of  $CF_4$  gas at a pressure of 1 atmosphere was obtained from P. E. Liley of Purdue University as

$$k^* = 1.73073 \left[ 7.2910 \times 10^{-3} + \left( 2.377 \times 10^{-5} \right) \left( \frac{9}{5} \text{T} - 459.67 \right) \right]$$
 (20)

where  $k^*$  is in W m<sup>-1</sup>K<sup>-1</sup>. This is a curve fit of experimental data over a temperature range from 230 K to 460 K. An uncertainty of 5 percent in value obtained from this equation appears to be a reasonable estimate. The thermal conductivity at 1 atmosphere of pressure is plotted over a temperature range of 100 K to 800 K in figure 2. Again, equation (20) is well behaved over the extended temperature range. The thermal conductivity relationship is extended to pressures other than 1 atmosphere in the same manner as was the viscosity. Residual thermal conductivities  $k - k^*$  for  $CF_4$  were obtained from experimental data and correlated with the corresponding reduced densities

(ref. 10) to produce the following expression:

$$k - k^* = 7.18 \times 10^{-3} \left[ \exp(\rho_R) - 1 \right]$$
 (21)

where  $k - k^*$  is in  $W m^{-1} K^{-1}$ . Equation (21) represents the thermal conductivity of  $CF_4$  in the dense gaseous region. Deviations have been observed (ref. 10) at lower densities; these deviations may be attributed to difficulties encountered in obtaining precise thermal conductivity values in the less dense region.

#### CALCULATION PROCEDURE

In generating the thermodynamic and transport properties of  $CF_4$  by using the computer code given in the appendix, the boundaries of the thermodynamic regime of interest were first designated in terms of temperature and volume. These boundaries were taken as

- (a) The saturation pressure line (eq. (16))  $p_S = f(T_S)$ . The saturation volume was determined from the equation of state (eq. (1))  $p_S = f(T_S, V_S)$ .
  - (b) The critical volume line  $V_c = 0.0016 \text{ m}^3\text{kg}^{-1}$ ,  $T = T_c$  to 844.7 K.
  - (c) The constant temperature line T = 844.7 K,  $V_c = 0.0016 \text{ to } V = 81.16 \text{ m}^3\text{kg}^{-1}$ .
- (d) The constant volume line  $V=81.16~\mathrm{m^3kg^{-1}}$ ,  $T=844.7~\mathrm{K}$  to saturation temperature (procured from the simultaneous solution of the saturation pressure equation (eq. (16)) and the equation of state (eq. (1)), that is,  $p_S=f(T_S)$  and  $p_S=f(T_S,V)$  where  $V=81.16~\mathrm{m^3kg^{-1}}$ ).

Other thermodynamic and the transport properties along the boundary are now easily calculated since they are expressed as a function of T and V.

To present the thermodynamic and transport property data in a convenient form, it is advantageous to calculate the properties at specified values of a given variable. A good example is the entropy which remains constant during a frequently occurring class of expansions in gas dynamic analysis. (Equations and computer codes for isentropic expansions and flow across normal and oblique shocks in CF4 are given in the appendixes of ref. 1.) First, S is determined at the critical point which gives a lower limit for the thermodynamic regime specified herein. The upper limit on S is determined by inserting the highest temperature and volume occurring on the boundaries of the specified regime (T = 844.7 K) and  $V = 81.16 \text{ m}^3\text{kg}^{-1}$  into equation (6) (S = f(T,V)). The entropy is then divided into equal intervals between the upper and lower limits and set at the partition nearest the lower limit, S = Constant = f(T,V). The volume is set slightly above the critical value at  $V = 0.0026 \text{ m}^3\text{kg}^{-1}$  in order to avoid the large gradients and consequent convergence difficulties that occur along the critical volume line and the

corresponding temperature calculated. This procedure gives an upper limit on the temperature for the specified value of the entropy. With the entropy held constant, the temperature is reduced at even intervals and the volume calculated at each temperature point until the saturated volume or the upper limit ( $V = 81.16 \, \mathrm{m^3 kg^{-1}}$ ) is exceeded. The transport properties and remaining thermodynamic variables which are given herein as a function of T and V are then calculated for the specified value of the entropy. This procedure is repeated at each entropy interval until the limits have been spanned. A similar procedure is used in calculating the thermodynamic and transport properties at constant values of any of the other thermodynamic variables.

#### RESULTS

Pressure-enthalpy diagrams are presented in figures 3 to 6. Each of these diagrams contain lines of constant entropy and volume. In addition to these lines in common, figure 3 contains lines of constant temperature, figure 4 contains lines of constant speed of sound, figure 5 contains lines of constant isentropic expansion exponent, and figure 6 contains lines of constant compressibility factor. These diagrams were generated from the computer code of the appendix with subroutines added to calculate the constant speed of sound, isentropic expansion exponent, and compressibility factor.

Equilibrium thermodynamic data and transport property data (calculated from the computer code presented in the appendix) are presented in table I for  $CF_4$  from a dimensionless entropy S/R of approximately 24.0 to 46.0 and from a temperature of 89.45 K to 845 K. These data are listed at constant entropy in increments of 0.25 with temperature increments of 10 K.

Transport property data along with the specific heats are tabulated in table II for CF<sub>4</sub> over a specific volume range from 0.002 to 80  $\rm m^3kg^{-1}$  for five values of temperature from 100 K to 800 K. These properties show little effect of the specific volume except near the critical value 0.0016  $\rm m^3kg^{-1}$ .

#### CONCLUDING REMARKS

Equations for the thermodynamic properties of gaseous, undissociated tetrafluoromethane  $(CF_4)$  in chemical equilibrium have been generated by using as accurate an equation of state and the curve fits of specific heat available. These equations along with those for the transport properties of  $CF_4$  have been incorporated into a computer code. Thermodynamic and transport property data generated by the computer code are presented in a form which lends itself to a convenient gas dynamic analysis over a thermodynamic regime heretofore not penetrated.

Langley Research Center,
National Aeronautics and Space Administration,
Hampton, Va., April 18, 1973.

#### APPENDIX

# DIGITAL COMPUTER CODE FOR CALCULATING THERMODYNAMIC PROPERTIES OF CF4

A FORTRAN IV Control Data Series 6000 computer code was developed for evaluating the thermodynamic properties of gaseous, dissociated tetrafluoromethane  $(CF_4)$  in chemical equilibrium. The computer code calculates the thermodynamic properties of  $CF_4$  when given any two of five thermodynamic variables (entropy, temperature, volume, pressure, and enthalpy). Besides the five aforementioned variables, the computer code also calculates specific heat at constant pressure, specific heat ratio, speed of sound, isentropic expansion exponent, compressibility factor, viscosity, and thermal conductivity.

#### Subroutine CF4

Language:

FORTRAN IV

Purpose:

Evaluates the thermodynamic and transport properties of gaseous, undissociated tetrafluoromethane (CF4) in chemical equilibrium when given any two of five thermodynamic variables (entropy, temperature, volume, pressure, and enthalpy). Besides the five aforementioned variables, the subroutine calculates specific heat at constant pressure, specific heat ratio gamma, speed of sound, isentropic expansion exponent, compressibility factor, viscosity, and thermal conductivity.

Use:

CALL CF4 (N, UNIN, UNIØ, ERR, TG, VG, SD, HD, PD, TI, VI, P, H, A, CP, GAM, G, Z, S, EMU, EK1)

Code inputs:

N Option indicating thermodynamic variables required on input

N = 1 Input SD, VI, and TG (estimate), Set HD, PD, TI, and VG at zero

N = 2 Input HD, VI, and TG (estimate), Set SD, PD, TI, and VG at zero

N = 3 Input PD, VI, and TG (estimate), Set SD, HD, TI, and VG at zero

N = 4 Input SD, TI, and VG (estimate), Set HD, PD, VI, and TG at zero

N = 5 Input HD, TI, and VG (estimate), Set SD, PD, VI, and TG at zero

N = 6 Input PD, TI, and VG (estimate), Set SD, HD, VI, and TG at zero

N = 7 Input VI and TI, Set HD, PD, SD, VG, and TG at zero

N = 8 Input SD, HD, TG (estimate), and VG (estimate), Set PD, VI, and TI at zero

N = 9	Input PD, HD, TG (estimate), and VG (estimate), Set SD, VI, and
	TI at zero
N = 10	Input PD, SD, TG (estimate), and VG (estimate), Set HD, VI, and

TI at zero

UNIN = 1. if input is in SI units

= 2. if input is in U.S. units

UNIØ = 1. if output is in SI units

= 2. if output is in U.S. units

ERR Allowable error in  $\frac{S-SD}{SD}$ ,  $\frac{H-HD}{HD}$ ,  $\frac{P-PD}{PD}$ 

		SI units	U.S. units
TG	temperature (estimate)	K	OR
VG	volume (estimate)	${ m m}^3{ m kg}^{-1}$	$ft^3lb^{-1}$
SD	entropy desired	nondimensional S/R	$Btulb^{-1}oR^{-1}$
HD	enthalpy desired	nondimensional $H/RT_O$	Btu lb <sup>-1</sup>
PD	pressure desired	nondimensional atm	$lbin^{-2}$
TI	temperature	K	$^{\mathrm{o}}\mathrm{R}$
VI	volume	$m^3$ kg-1	$_{ m ft}$ 3 $_{ m lb}$ -1

#### Code outputs:

		SI units	U.S. Units
TI	temperature	K	OR
VI	volume	$\mathrm{m}^{3}\mathrm{kg}^{-1}$	$_{ m ft}$ $^3{ m lb}$ -1
P	pressure	nondimensional atm	$lbin^{-2}$
H	enthalpy	nondimensional H/RT <sub>o</sub>	Btu lb <sup>-1</sup>
A	a, speed of sound	${ m m\ s}^{-1}$	$\rm fts^{-1}$
CP	c <sub>p</sub> , specific heat at constant pressure	nondimensional $c_p/R$	Btulb-10R-1
GAM	$\gamma$ , specific heat ratio, $c_{ m p}/c_{ m v}$	nondimensional	nondimensional
G	$\gamma_{\rm e}$ , isentropic expansion exponent	nondimensional	nondimensional
Z	compressibility factor	nondimensional	non dimension al

		SI units	U.S. units
S	entropy	nondimensional S/R	$_{ m Btulb}$ -1 $_{ m R}$ -1
EMU	$\mu$ , viscosity	${ m Nsm^{-2}}$	$_{ m lbft}$ -1 $_{ m s}$ -1
EK1	k, thermal	$_{\mathrm{W}\mathrm{m}^{-1}\mathrm{K}^{-1}}$	$_{\mathrm{Btus}^{-1}\mathrm{ft}^{-1}\mathrm{o_R}^{-1}}$

conductivity

Accuracy:

A function of ERR input.

Error condition:

STOP 1000 indicates nonconvergence in subroutine ITT

Storage:

13618 locations

Subprograms used: ITT

1778 locations

PØTV 278 locations

SØTV 268 locations

HØTV 638 locations

TVAR 3778 locations

VVAR 1578 locations

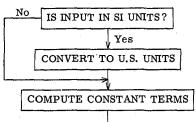
SQRT 438 locations

EXP 578 locations

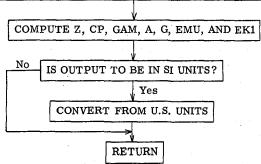
ALNLØG 678 locations

#### Flow Chart for Subroutine CF4

Computes thermodynamic properties of CF<sub>4</sub> when given any two of five thermodynamic variables



#### TEST N FOR INPUT OPTIONS HOLD V, VARY T UNTIL S IS FOUND, COMPUTE H AND P N = 1N = 2HOLD V, VARY T UNTIL H IS FOUND, COMPUTE S AND P HOLD V, VARY T UNTIL P IS FOUND, COMPUTE S AND H N = 3HOLD T, VARY V UNTIL S IS FOUND, COMPUTE H AND P N = 4N = 5HOLD T, VARY V UNTIL H IS FOUND, COMPUTE S AND P N = 6HOLD T, VARY V UNTIL P IS FOUND, COMPUTE S AND H HOLD T, HOLD V, COMPUTE S, H, AND P N = 7N = 8 (1) HOLD V, VARY T UNTIL H IS FOUND COMPUTE S IF S IS NOT THE DESIRED S, HOLD T, VARY V UNTIL S IS FOUND IF H IS NOT THE DESIRED H, REPEAT FROM (1) WHEN S AND H ARE FOUND, COMPUTE P N = 9 (2) HOLD V, VARY T UNTIL H IS FOUND COMPUTE P IF P IS NOT THE DESIRED P, HOLD T, VARY V UNTIL P IS FOUND COMPUTE H IF H IS NOT THE DESIRED H, REPEAT FROM (2) WHEN P AND H ARE FOUND, COMPUTE S N = 10 (3) HOLD V, VARY T UNTIL S IS FOUND COMPUTE P IF P IS NOT THE DESIRED P, HOLD T, VARY V UNTIL P IS FOUND IF S IS NOT THE DESIRED S, REPEAT FROM (3) WHEN P AND S ARE FOUND, COMPUTE H



#### Other Subroutines

### SUBROUTINE ITT (XVAR, XI, YVAR, YGG, YI, ZVAR, ZI, ZD, ERR, K)

(Iterative procedure to calculate ZI = f(XI,YI))

Given XI, YGG, and ZD

Compute XI terms

Estimate YI = YGG

(1) Compute YI terms, compute ZI = f(XI, YI)

If ZI is not the desired ZD, second estimate of YI = 0.95 \* first estimate. Other estimates after first two are by linear interpolation or extrapolation. Repeat from (1).

If ZI is not ZD after 1000 iterations, stop.

#### SUBROUTINE POTV (P, VI, TI)

p = f(T, V)

SUBROUTINE SOTV (S, VI, TI)

S = f(T, V)

SUBROUTINE HOTV (H, VI, TI)

H = f(T, V)

SUBROUTINE TVAR (TI)

Computes T terms

#### SUBROUTINE VVAR (VI)

Computes V terms

#### Program Listing

	SUBR	OUTINE	CF4 (	N.UN	EN JUN	110.E	RR,	TG, VG	, SD . F	ID . PD	.TI.	VI.P.I	H,A,C	P.GAM.	A	1
		S.EMU.E													Α	2
С		THIS	SUBRO	UŤIN	CAL	CULA	TES	THER	MODYN	IAMIC	PROF	PERTI	ES OF	CF4	A	3
C		WHEN	GIVEN	ANY	TWO	OF F	IVE	THER	MODYN	IAMIC	VAR	IABLES	S		Α	4
C		(ENTR	BPY,T	EMPE	RATUR	E,VO	LUM	E,PRE	SSURE	AND	ENT	HALPY	<b>)</b>		A	5
С	N	OPTIO	N IND	ICAT:	ING 1	HERM	ODY	NAMIC	PROP	ERTI	ES RI	EQUIRE	ED ON	INPUT	Α	6
С		<b>= 1</b>	SD.V	I.TG	EST	MATE									A	7
С		=2	HD . V	I.TG	EST	MATE				**					A	8
С		=3	PD.V	I.TG	ESTI	MATE									Α	9
С		= 4	SD.T	I.VG	EST 1	MATE									A	10
С		= 5	HD, T	I,VG	EST	MATE	,								À	11
С		=6	PD. T	I.VG	EST	MATE									A	12
C		= 7	VI.T	I											Ā	13
C		= 8	SD.H	D.TG	EST	MATE	• VG	ESTI	MATE						Δ	14
С		=9	PD.H	D.TG	EST	MATE	• VG	ESTI	MATE						Δ	15
С		= 10		D. TG					_						A	16

```
C
                                                                                      17
             =1.INPUT IN SI UNITS
                                                                           INPUT
                                                                                      18
C
C
              =2.INPUT IN US UNITS
                                                                                      19
             =1.OUTPUT IN SI UNITS
=2.OUTPUT IN US UNITS
C
                                                                           INPUT
                                                                                   A
                                                                                      20
С
                                                                                      21
C
       FRR
             RELATIVE ERROR IN SD. HD. PD
                                                                           INPUT
                                                                                      22
             TEMPERATURE ESTIMATE (DEGK)
                                                                           INPUT
C
       TG
                                               (DEGR)
                                                                                   A
                                                                                      23
C
       VG
              VOLUME ESTIMATE
                                     [M3/KGM]
                                               (FT3/LB)
                                                                            INPUT
                                                                                   A
                                                                                      24
                  ENTROPY
C
                                  (S/R)
                                               (BTU/LBDEGR)
                                                                           INPUT
                                                                                      25
       Sn
C
       HD
                  ENTHALPY
                                  (H/RTO)
                                               (BTU/LB)
                                                                            INPUT
                                                                                      26
Č
       ΡD
                  PRESSURE
                                  (ATM)
                                               (LBF/IN2)
                                                                           INPUT
                                                                                      27
                                                                                   A
                                                                INPUT OR OUTPUT
C
       T I
                  TEMPERATURE
                                  (DEGK)
                                               (DEGR)
                                                                                   A
                                                                                      28
                                                                INPUT OR OUTPUT
C
       ٧I
                  VOLUME
                                  (M3/KGM)
                                               (FT3/LB)
                                                                                      29
                                                                          OUTPUT
C
       Р
                  PRESSURE
                                  (ATM)
                                               (LBF/IN2)
                                                                                      30
C
       н
                  ENTHALPY
                                  (H/RTO)
                                               (BTU/LB)
                                                                          OUTPUT
                                                                                   A
                                                                                      31
                  SPEED OF SOUNDIM/SECT
С
       Α
                                                         (FT/SEC)
                                                                          OUTPUT
                                                                                   A
                                                                                      32
            SPECIFIC HEAT AT CONSTANT PRESSURE (CP/R) (BTU/LBDEGR) OUTPUT
C
       CP
                                                                                      33
                  RATIO OF SPECIFIC HEATS GAMMA=CP/CV
                                                                          OUTPUT
C
       GAM
                                                                                      34
C
                  (A**2)/(P*V)
                                  ISENTROPIC EXPANSION GAMMA
                                                                          DUTPUT
                                                                                      35
       G
                                                                                   Δ
                  (V*P)/(R*T)
C
                                COMPRESSIBILITY FACTOR
                                                                          OUTPUT
                                                                                      36
       Z
                                                                                   Δ
C
                  ENTROPY
                                  (S/R)
                                               (BTU/LBDEGR)
                                                                          OUTPUT
                                                                                      37
       S
                                              (LB/FT SEC)
С
                  VISCOSITY
                                 (N/M2)
                                                                          OUTPUT
       EMU
                                                                                   Δ
                                                                                      38
С
                  THERMAL CONDUCTIVITY (W/M DEGK) (BTU/SEC FT DEGR) DUTPUT
                                                                                   A
                                                                                      39
       EK 1
       STOP 1000 INDICATES MAXIMUM ITERATIONS IN SUBROUTINE ITT
С
                                                                                      40
                                                                                   Δ
                                                                                      41
      REAL K,KTI,KTR,J,JVI,JVI22,J8403,J860A,J2,J4,JK,JR,JVR,JVR22,JVI2
COMMON /BLOCK/ J,R,A2,82,C2,A3,B3,C3,A4,B4,A5,B5,C5,A6,B6,S8,K,ALP
                                                                                      42
                                                                                   Α
                                                                                      43
     1 HA, SA4, SB4, SC4, SD4, SR, TR, VR, HR, TR2, TR3, TR4, KTR, EMKTR, VRMB, VRMB2, VR
                                                                                      44
     2MB3,VRMB4,VRMB5,VRMB22,VRMB33,VRMB44,VRMB55,QVRB,QVRB2,QVRB3,QVRB4
                                                                                   Α
                                                                                      45
     3,0VRB5,AVR,EAVR,SUM1,JB403,JB60A,SUM18,SB42,SC43,SD44,SC42,SD43,J2
                                                                                   A
                                                                                      46
      4.J4.JK.JR.JVR.SUM21.SUM22.SUM23.SUM24.SUM25.JVR22.AER.RTI.OVIB.SUM
                                                                                   Δ
                                                                                       47
     52,0VIB2, SUM3,0VIB3, SUM4, OVIB4, SUM5, OVIB5, SUM6, EAVI, SUM14, SUM9, SUMI
                                                                                      48
     60, SUM11, SUM12, SUM8, SUM32, SUM26, SUM33, SUM28, SUM34, SUM29, SUM30, SUM35
                                                                                   Α
                                                                                      49
     7,SUM31,JVI22,B4T4,AEI,JVI,B4T,SUM36,SUM37,SUM38,SUM39,SUM40,SUM43,
                                                                                      50
     8SUM41,SUM42,OVIB6,JVI2,VI2,DEC1,DEC2,DEC3,DEC4,DEC5,KTI
                                                                                      51
       EXTERNAL TVAR, VVAR, SOTV, HOTV, POTV
                                                                                      52
       DATA J/1.850505E-1/,R/1.219336E-1/,A2/-2.162959/.B2/2.135114E-3/,C
                                                                                      53
     12/-1.8941131E1/.A3/4.404057E-3/.B3/1.282818E-5/.C3/5.39776E-1/.A4/
                                                                                      54
     21.921072E-4/.84/-3.918263E-7/.A5/-4.481049E-6/.B5/9.062318E-9/.C5/
                                                                                       55
     3-4.836678E-5/.A6/5.838823E7/.B6/-9.263923E4/.SB/1.5E-3/.K/9.76798E
                                                                                   Δ
                                                                                      56
     4-3/.ALPHA/-6.61199997E2/.SR/.848/,TR/820./,VR/1U0./,HR/200./,CONV/
                                                                                   A
                                                                                      57
     5.06242796200/.CONT/.55555555555556/.CONP/.06804596299/.CONS/44.289
                                                                                      58
                                                                                   Δ
     6180/.CONH/.090075418/.CONA/.3048/.DEC1/1./.DEC2/2./.DEC3/3./.DEC4/
                                                                                      59
     74./.DEC5/5./
                                                                                   Δ
                                                                                      60
       DATA TC/227.48/, EM/88.01/, PC/36.96/, VC/1.597444089E-3/
                                                                                   Δ
                                                                                      61
       IF (UNIN-1.) 11,11,12
                                                                                      62
       VI=VI/CONV
1.1
                                                                                      63
       VG=VG/CONV
                                                                                   A
                                                                                      64
       TI=TI/CONT
                                                                                   A
                                                                                      65
       TG=TG/CONT
                                                                                   Α
                                                                                      66
       SD=SD/CONS
                                                                                   Δ
                                                                                      67
       HD=HD/CONH
                                                                                   Δ
                                                                                      68
       PD=PD/CONP
                                                                                   A
                                                                                      69
12
       CONTINUE
                                                                                   A
                                                                                      70
       TR2=TR*TR
                                                                                   Δ
                                                                                      71
       TR3=TR2*TR
                                                                                   Δ
                                                                                      72
       TR4=TR2*TR2
                                                                                      73
                                                                                   Α
       KTR=K*TR
                                                                                      74
       FMKTR=FXP(-KTR)
                                                                                      75
                                                                                   Δ
       VRMB=VR-SB
                                                                                   Δ
                                                                                      76
       VRMB2=VRMB*VRMB
                                                                                      77
                                                                                   Α
       VRMB3=VRMB2*VRMB
                                                                                      78
       VRMB4=VRMB2*VRMB2
                                                                                   ۸
                                                                                      79
       VRM85=VRM82*VRMB3
                                                                                   Α
                                                                                      80
       VRMB22=VRMB2*DEC2
                                                                                      81
                                                                                   Δ
       VRMB33=VRMB3*DEC3
                                                                                   Α
                                                                                      82
       VRMB44=VRMB4*DEC4
                                                                                   Δ
                                                                                      83
       VRMB55=VRMB5*DEC5
                                                                                   Α
                                                                                      84
       OVRB=DEC1/VRMB
                                                                                      85
```

	OVRB2=DEC1/VRMB2	A	86
	OVRB3=DEC1/VRMB3	A	87
	OVRB4=DEC1/VRMB4	Á	88
	OVRB5=DEC1/VRMB5	Ā	89
	AVR=ALPHA*VR		
		A	90
	EAVR=EXP(AVR)	A	91
	SUM1=C2/VRMB+C3/VRMB22+C5/VRMB44	A	92
	JB 403=J* B4/DEC3	A	93
	JB6OA=J*B6/ALPHA	A	94
	SUM18=EMKTR*(KTR+DEC1)	A	95
	J2=J/DEC2	A	
	J4= J/DEC4	A	
	JK=J*K	Ā	
	JR=J*R		_
		A	
	JVR = J*VR		100
	SUM21=SB*OVRB		101
	SUM22=OVRB+SB/VRMB22	A	102
	SUM23=DEC1/VRMB22+SB/VRMB33	A	103
	SUM24=DEC4*A4*(DEC1/VRMB33+SB/VRMB44)	Α	104
	SUM25=DEC1/VRMB44+SB/VRMB55		105
	JVR22=JVR*VR/DEC2		106
	AER=ALPHA*EAVR		
			107
	GO TO ( 1, 2, 3, 4, 5, 6, 7, 8, 9,10), N		108
1	CALL ITT (VVAR.VI.TVAR.TG.TI.SOTV.S.SD.ERR.1)	A	109
	CALL HOTV (H,VI,TI)	A	110
	CALL POTV (P,VI,TI)	Α	111
	GO TO 35	Δ	112
2	CALL ITT (VVAR.VI.TVAR.TG.TI.HOTV.H.HD.ERR.1)		113
_	CALL SOTY (S.VI.TI)	-	114
	CALL POTV (P.VI.TI)		
	·		115
_	GO TO 35		116
3	CALL ITT (VVAR, VI, TVAR, TG, TI, POTV, P, PD, ERR, 1)		117
	CALL SOTV (S,VI,TI)	A	118
	CALL HOTV (H,VI,TI)	Α	119
	GO TO 35	A	120
4	CALL ITT (TVAR, TI, VVAR, VG, VI, SOTV, S, SD, ERR, 2)	Δ	121
	CALL HOTV (H,VI,TI)		122
	CALL POTV (P.VI.TI)		123
	GO TO 35		124
5	CALL ITT (TVAR,TI,VVAR,VG,VI,HOTV,H,HD,ERR,2)		-
•			125
	CALL SOTV (S.VI.TI)		126
	CALL POTV (P,VI,TI)		127
	GO TO 35	A	128
6	CALL ITT (TVAR,TI,VVAR,VG,VI,POTV,P,PD,ERR,2)	A	129
	CALL SOTV (S.VI.TI)	A	130
	CALL HOTV (H,VI,TI)	Δ	131
	GO TO 35		132
7	CALL TVAR (TI)		133
'			_
	CALL VVAR (VI)		134
	CALL SOTV (S,VI,TI)		135
	CALL HOTV (H,VI,TI)	A	136
	CALL POTV (P,VI,TI)	Α	137
	GO TO 35	A	138
8	VI = VG	Α	139
	CALL ITT (VVAR, VI, TVAR, TG, TI, HOTV, H, HD, ERR, 1)	Δ	140
	CALL SOTY (S.VI.TI)		141
	IF (ABS(S-SD)=ERR*SD) 24.22.22		142
	VG=VI		143
	CALL ITT (TVAR,TI,VVAR,VG,VI,SOTV,S,SD,ERR,2)		144
	CALL HOTV (H,VI,TI)		145
	IF (ABS(H-HD)-ERR*HD) 24,23,23		146
	TG=TI		147
	GO TO 21	Α	148
	CALL POTV (P.VI.TI)	A	149
	GO TO 35	Α	150
9	VI = VG		151
,	CALL ITT (VVAR, VI, TVAR, TG, TI, HOTV, H, HD, ERR, 1)		152
	CALL POTV (P,VI,TI)		153
	IF (ABS(P-PD)-ERR*PD) 29,27,27		154
	The state of the s	-	177

```
VG=VI
                                                                                A 155
27
                                                                                A 156
      CALL ITT (TVAR, TI, VVAR, VG, VI, POTV, P, PD, ERR, 2)
      CALL HOTY (H.VI.TI)
                                                                                A 157
      IF (ABS(H-HD)-ERR*HD) 29,28,29
                                                                                A 158
                                                                                  159
      TC=TT
28
                                                                                  160
      GO TO 26
                                                                                Δ
      CALL SOTV (S.VI.TI)
                                                                                A 161
29
                                                                                A 162
      GO TO 35
                                                                                Δ
                                                                                  163
   10 VI=VG
      CALL ITT (VVAR, VI, TVAR, TG, TI, SOTV, S, SD, ERR, 1)
                                                                                A 164
31
      CALL POTV (P.VI.TI)
                                                                                A 165
      IF (ABS(P-PD)-ERR*PD) 34,32,32
                                                                               A 166
32
      VG=VI
                                                                                Δ
                                                                                  167
      CALL ITT (TVAR, TI, VVAR, VG, VI, POTV, P, PD, ERR, 2)
                                                                                4 168
      CALL SOTV (S.VI.TI)
                                                                                A.169
      IF (ABS(S-SD)-ERR*SD) 34,33,33
                                                                                A 170
      TG=TI
                                                                                A 171
33
      GO TO 31
                                                                                Δ 172
                                                                                 173
34
      CALL HOTV (H.VI.TI)
                                                                                Δ
35
      Z=(VI*P)/(RTI)
                                                                                  174
                                                                                Δ 175
      CV=(SUM37-SUM38*SUM36)
      PPT=(R*OVIB+SUM39*OVIB2+SUM40*OVIB3+SUM43+SUM41*OVIB5)
                                                                                A 176
      PPV=(RTI*0VIB2+SUM33*0VIB3+SUM34*0VIB4+SUM42*0VIB5+SUM35*0VIB6-AEI
                                                                               A 177
     1*SUM6)
                                                                                  178
                                                                                A 179
      CP = CV - TI * J * PPT * * 2/(-PPV)
      GAM=CP/CV
                                                                                Δ 180
      A= JV I2*T [*PPT**2/CV+VI2*PPV
                                                                                A 181
                                                                                A 182
      ASQ=A*4633.056
      G=A/(P*VI)
                                                                                Δ 183
      TK=TI*CONT
                                                                                A 184
      EMU=(SQRT(TK)/(.64625+103./TK-3.42714/(TK*TK)))*1.E-6
                                                                                A 185
      EK1=1.73073*(7.291E-3+2.377E-5*((9./5.)*TK-459.67))
                                                                                A 186
                                                                                A 187
      IF (ASO) 37,36,36
36
      A=SQRT(ASQ)
                                                                                A 188
      VK = VI *CONV
                                                                                A 189
37
      XI=TC**.16666667/(SORT(EM)*PC**.66666667)
                                                                                A 190
      RHOR=VC/VK
                                                                                A 191
      EK1=EK1+7.18E-3*(EXP(RHOR)-1.)
                                                                                4 192
      IF (RHOR-.10) 41,41,38
                                                                                A 193
      IF (RHOR-.90) 42,42,39
                                                                                A 194
38
39
      IF (RHOR-2.2) 43,43,40
                                                                                A 195
      X=.6439-.1005*RHOR-4.75E-4*(RHOR**3-10.65)**2
                                                                                A 196
40
                                                                                A 197
      ALG1=10.**X+3.
      ALG2=10.**(-ALG1)
                                                                                A 198
      EMU=(ALG2+XI*EMU)/XI
                                                                                A 199
      GO TO 44
                                                                                A 200
41
      EMU=(16.56E-8*RHOR**1.111+XI *EMU)/XI
                                                                                  201
                                                                                A 202
      GO TO 44
      EMU=(.607E-8*(9.045*RHOR+.63)**1.739+XI*EMU)/XI
                                                                                A 203
42
      GO TO 44
                                                                                A 204
      X=.6439-.1005*RHOR
                                                                                Α
                                                                                  205
43
      ALG1=10.**X+3.
                                                                                A 206
      ALG2=10.**(-ALG1)
                                                                                A. 207
                                                                                A 208
      EMU=(ALG2+XI*EMU)/XI
44
      IF (UNIO-1.) 45,45,46
                                                                                A 209
      TI=TK
                                                                                A 210
45
      V [ = VK
                                                                                A 211
      S=S*CONS
                                                                                A 212
      H=H*CONH
                                                                                Δ
                                                                                  213
      P=P*CONP
                                                                                A 214
      CP=CP*CONS
                                                                                4 215
      A=A*CONA
                                                                                Δ 216
      VG=VG*CONV
                                                                                A
                                                                                  217
      TG=TG*CONT
                                                                                A 218
      SD=SD*CONS
                                                                                Δ
                                                                                 219
      HD=HD*CONH
                                                                                A 220
      PD=PD*CONP
                                                                                A 221
      GO TO 47
                                                                                A 222
46
      EMU=EMU/1.4881639
                                                                                A 223
      EK1=EK1/6226.47794
                                                                                A 224
47
      RETURN
                                                                                A 225
      END
                                                                                A 226-
```

```
SUBROUTINE ITT (XVAR, XI, YVAR, YGG, YI, ZVAR, ZI, ZD, ERR, K)
C
             THIS SUBROUTINE ITERATES TO FIND Z=F(X,Y)
                                                                                   P
                                                                                       2
       DIMENSION YG(2), ZG(2)
                                                                                   В
                                                                                       3
       K \cap U \cap T = 0
                                                                                   В
                                                                                        4
1
       CALL XVAR (XI)
       YG(1) = YGG
                                                                                   B
                                                                                       6
       J J = 1
                                                                                   В
                                                                                       7
2
       YI = YG\{11\}
                                                                                   В
                                                                                       8
       IF (K-2) 5,3,3
                                                                                   В
                                                                                       q
       IF (YI-.0015) 4,4,5
3
                                                                                   R
                                                                                      10
       XI = XI * 1.05
                                                                                   B
                                                                                      11
       GO TO 1
                                                                                   R
                                                                                      12
5
       CALL YVAR (YI)
                                                                                   B
                                                                                      13
       GO TO (6.7) . K
                                                                                   R
                                                                                      14
6
       CALL ZVAR (ZI.XI.YI)
                                                                                   В
                                                                                      15
       GO TO 8
                                                                                   B
                                                                                      16
       CALL ZVAR (ZI,YI,XI)
7
                                                                                   В
                                                                                      17
8
       7G(JJ)=ZI
                                                                                   В
                                                                                      18
       IF (ABS(ZG(JJ)-ZD)-ERR*ZD) 13.9.9
                                                                                   В
                                                                                      19
       IF (JJ-1) 10.10.11
                                                                                      20
10
       JJ=2
                                                                                   R
                                                                                      21
       YG(2)=YG(1)*.95
                                                                                   R
                                                                                      22
       GO TO 2
                                                                                   B
                                                                                      23
       YGN=((YG(2)-YG(1))/(ZG(2)-ZG(1)))*(ZD-ZG(1))+YG(1)
11
                                                                                      24
       ZG(1) = ZG(2)
                                                                                   R
                                                                                      25
       YG(1)=YG(2)
                                                                                   B
                                                                                      26
       YG (2) = YGN
                                                                                   B
                                                                                      27
       KOUNT=KOUNT+1
                                                                                   B
                                                                                      28
       IF (KOUNT-1000) 2,2,12
                                                                                   R
                                                                                      29
12
       STOP 1000
                                                                                   В
                                                                                      30
13
       RETURN
                                                                                   В
                                                                                      31
       FND
                                                                                   В
                                                                                      32-
       SUBROUTINE POTV (P, VI, TI)
                                                                                   C
                                                                                       1
             THIS SUBROUTINE CALCULATES P=F(T,V)
C.
                                                                                   C
                                                                                        2
            K, KTI, KTR, J, JVI, JVI, 22, J8403, J860A, J2, J4, JK, JK, JVR, JVR, JVR, 22, JVI, 2
                                                                                   С
                                                                                       3
       COMMON /BLOCK/ J.R.A2.B2.C2.A3.B3.C3.A4.B4.A5.B5.C5.A6.B6.SB.K.ALP
                                                                                        4
     1HA,SA4,SB4,SC4,SD4,SR,TR,VR,HR,TR2,TR3,TR4,KTR,EMKTR,VKMB,VRMB2,VR
                                                                                        5
     2MB3, VRMB4, VRMB5, VRMB22, VRMB33, VRMB44, VRMB55, OVRB4, OVRB2, UVRB3, OVRB4
                                                                                   C.
                                                                                        6
     3.0VRB5.AVR.EAVR.SUM1.JB403.JB60A.SUM18.SB42.SC43.SD44.SC42.SD43.J2
                                                                                        7
     4.14.1K.JR.JVR.SUM21.SUM22.SUM23.SUM24.SUM25.JVR22.AER.RTI.OVIB.SUM
                                                                                        8
     52.0VIB2.SUM3.0VIB3.SUM4.0VIB4.SUM5.0VIB5.SUM6.EAVI.SUM14.SUM9.SUM1
                                                                                       9
     60.SUM11.SUM12.SUM8.SUM32.SUM26.SUM33.SUM28.SUM34.SUM29.SUM30.SUM35
                                                                                      10
     7.SUM31.JVI22.B4T4.AEI.JVI.B4T.SUM36.SUM37.SUM38.SUM39.SUM40.SUM43.
                                                                                      11
     8SUM41.SUM42.OVIB6.JVI2.VI2.DEC1, DEC2.DEC3.DEC4.DEC5.KTI
                                                                                   С
                                                                                      12
       P=RTI*OVIB+SUM2*OVIB2+SUM3*OVIB3+SUM4*OVIB4+SUM5*OVIB5+SUM6*EAVI
                                                                                   C
                                                                                      13
       RETURN
                                                                                   C
                                                                                       14
       FND
                                                                                   C
                                                                                      15-
                                                                                   D
       SUBROUTINE SOTY (S.VI.TI)
                                                                                        1
C
             THIS SUBROUTINE CALCULATES S=F(T.V)
                                                                                   Ð
                                                                                        2
       REAL K,KTI,KTR, J, JVI, JVI22, JB403, JB60A, J2, J4, JK, JK, JVK, JVR22, JVI2
      COMMON /BLOCK/ J.R. A2, B2, C2, A3, B3, C3, A4, B4, A5, B5, C5, A6, B6, SB, K, ALP
                                                                                   n
                                                                                        4
      1HA, SA4, SB4, SC4, SD4, SR, TR, VR, HR, TR2, TR3, TR4, KTR, EMKTR, VRMB, VRMB2, VR
                                                                                   D
                                                                                        5
      2MB3.VRMB4.VRMB5.VRMB22.VRMB33.VRMB44.VRMB55.QVRB.QVRB2.QVRB3.QVRB4
                                                                                   D
                                                                                        6
     3, OV R R 5, AV R, E AV R, SUM 1, JB 403, JB 60A, SUM 18, SB 42, SC 43, SD 44, SC 42, SD 43, J2
     4.J4.JK.JR.JVR.SUM21.SUM22.SUM23.SUM24.SUM25.JVR22.AEK.RTI.OVIB.SUM
                                                                                   n
                                                                                        Я
     52.0VIB2.SUM3.0VIB3.SUM4.0VIB4.SUM5.0VIB5.SUM6.EAVI.SUM14.SUM9.SUM1
                                                                                   Ð
                                                                                        9
     60.SUM11.SUM12.SUM8.SUM32.SUM26.SUM33.SUM28.SUM34.SUM29.SUM30.SUM35
                                                                                       10
                                                                                   D
      7.SUM31.JVI22.B4T4.AEI.JVI.B4T,SUM36.SUM37.SUM38.SUM39.SUM40.SUM43.
                                                                                   D
                                                                                       11
      8SUM41,SUM42,OVIB6,JVI2,VI2,DEC1,DEC2,DEC3,DEC4,DEC5,KTI
                                                                                   n
                                                                                      12
       SUM 15=SUM 14-SUM9*OV 1B-SUM 10*OV IB 2-SUM 11*OV IB 4+SUM 12
                                                                                   D
                                                                                       13
       S=SUM15+SUM8
                                                                                      14
                                                                                   n
       RETURN
                                                                                   D
                                                                                      15
       END
                                                                                   0
                                                                                      16-
```

```
SUBROUTINE HOTY (H.VI.TI)
C
             THIS SUBROUTINE CALCULATES H=F(T.V)
                                                                                Ε
                                                                                    2
      REAL K,KTI;KTR,J,JVI,JVI22,JB403,JB60A,J2,J4,JK,JR,JVK,JVR22,JVI2
                                                                                E
                                                                                    3
      COMMON /BLOCK/ J.R. A2.B2.C2.A3.B3.C3.A4.B4.A5.B5.C5.A6.B6.SB.K.ALP
     1HA·SA4·SB4·SC4·SD4·SR·TR·VR·HR·TR2·TR3·TR4·KTK·EMKTK·VRMB·VRMB2·VR
                                                                                    5
     2MB3+VRMB4,VRMB5+VRMB22+VRMB33+VRMB44,VRMB55,UVRB,UVRB2+UVRB3+OVRB4
                                                                                    6
     3, GVRB5, AVR, EAVR, SUM1, JB403, JB60A, SUM18, SB42, SC43, SD44, SC42, SD43, J2
                                                                                    7
     4.J4.JK.JR.JVR.SUM21.SUM22.SUM23.SUM24.SUM25.JVR22.AER.RTI.QVIB.SUM
                                                                                    8
     52.0VIB2.SUM3.0VIB3.SUM4.0VIB4.SUM5.0VIB5.SUM6.EAVI.SUM14.SUM9.SUM1
                                                                                    Q
                                                                                E
     60, SUM11, SUM12, SUM8, SUM32, SUM26, SUM33, SUM28, SUM34, SUM29, SUM30, SUM35
                                                                                   10
     7,SUM31,JVI22,B4T4,AEI,JVI,B4T,SUM36,SUM37,SUM38,SUM39,SUM40,SUM43,
                                                                                E
                                                                                   11
     8SUM41.SUM42.OVIB6.JVI2.VI2.DEC1.DEC2.DEC3.DEC4.DEC5.KTI
                                                                                   12
      SUM15=SUM14-SUM9*OVIB-SUM10*OVIB2-SUM11*OVIB4+SUM12
                                                                                   13
      H=SUM32+HR-J*(RTI*SUM26-SUM33*SUM28-SUM34*SUM29-SUM30-SUM35*SUM31)
                                                                                   14
     1+JVI22*(-B4T4*OVIB5+AEI*SUM6)+JVI*(B4T*QVIB4+SUM6*EAVIJ+TI*SUM15
                                                                                   15
                                                                                ۶
      RETURN
                                                                                E
                                                                                   16
      END
                                                                                E
                                                                                   17-
      SUBROUTINE TVAR (TI)
                                                                                F
C
             THIS SUBROUTINE CALCULATES T TERMS
                                                                                F
                                                                                    2
                                                                                F.
      REAL K, KTI, KTR, J, JVI, JVI 22, JB403, JB60A, J2, J4, JK, JK, JVR, JVR22, JVI2
                                                                                    3
      COMMON /BLOCK/ J.R.A2,B2,C2,A3,B3,C3,A4,B4,A5,B5,C5,A6,B6,SB,K,ALP
                                                                                F
                                                                                    4
     1HA,SA4,SB4,SC4,SD4,SP,TR,VR,HR,TR2,TR3,TR4,KTR,EMKTR,VRMB,VRMB2,VR
                                                                                    5
     2MB3,VRMB4,VRMB5,VRMB22,VRMB33,VRMB44,VRMB55,QVRB,QVRB2,UVRB3,QVRB4
                                                                                    6
     3,0VRB5,AVR,EAVR,SUM1,JB403,JB60A,SUM18,SB42,SC43,SD44,SC42,SD43,J2
                                                                                    7
     4.J4.JK.JR.JVR.SUM21.SUM22.SUM23.SUM24.SUM25.JVR22.AER.RTI.OVIB.SUM
                                                                                    8
     52.0VIB2.SUM3.0VIB3.SUM4.0VIB4.SUM5.0VIB5.SUM6.EAVI.SUM14.SUM9.SUM1
     60.SUM11.SUM12.SUM8.SUM32.SUM26.SUM33.SUM28.SUM34.SUM29.SUM30.SUM35
                                                                                   10
     7.SUM31.JVI22.B4T4.AEI.JVI.B4T.SUM36.SUM37.SUM38.SUM39.SUM40.SUM43.
                                                                                   11
     8SUM41.SUM42, OVIB6.JVI2.VI2.DEC1, DEC2.DEC3.DEC4, DEC5.KTI
                                                                                   12
       IF(TI-1107.)2.1.1
                                                                                   13
                                                                                F
1
       SA4=.07069551
                                                                                   14
                                                                                F
                                                                                   15
       SB4=2.0415605E-4
                                                                                F
       SC4=-7.9130080E-8
                                                                                   16
                                                                                F
      SD4=1.0826239E-11
                                                                                   17
                                                                                F
      GO TO 3
                                                                                   18
      SA4=.03425143
                                                                                F
                                                                                   19
2
       S84=2.0072233E-4
                                                                                   20
                                                                                F
                                                                                   21
       SC4=3.8046689E-8
                                                                                F
                                                                                   22
       SD4=-6.5317171E-11
                                                                                F
       SB42=SB4/DEC2
                                                                                   23
3
                                                                                F
                                                                                   24
       SC43=SC4/DEC3
                                                                                F
      SD44=SD4/DEC4
                                                                                   25
      SC42=SC4/DEC2
                                                                                F
                                                                                   26
      SD43=SD4/DEC3
                                                                                F
                                                                                   27
      TI2=TI*TI
                                                                                   28
                                                                                ¢
      T13=T12*T1
                                                                                   29
                                                                                F
      TI4=TI2*TI2
                                                                                   30
                                                                                F
                                                                                   31
      KTI=K*TI
                                                                                F
                                                                                   32
      EMKTI=EXP(-KTI)
                                                                                F
      SUM38=JK*KTI*EMKTI
                                                                                   33
      SUM37=SA4+SB4*TI+SC4*TI2+SD4*TI3
                                                                                F
                                                                                   34
                                                                                F
                                                                                   35
      C2E=C2*EMKTI
      C3E=C3*EMKTI
                                                                                F
                                                                                   36
                                                                                F
                                                                                   37
      C5E=C5*EMKTI
                                                                                F
                                                                                   3.8
      RTI=R*TI
                                                                                F
      B2T=B2*T [
                                                                                   39
                                                                                F
      B3T=R3*T1
                                                                                   40
                                                                                F
                                                                                   41
      84T=84*T I
                                                                               F
      B5T=B5*T1
                                                                                   42
                                                                                F
                                                                                   43
      B6T=B6*TI
                                                                                F
                                                                                   44
      SUM 2= A2 + B2T + C2E
                                                                                F
                                                                                   45
       SUM3=A3+B3T+C3E
                                                                                F
                                                                                   46
       SUM 4= A4+B4T
                                                                                F
                                                                                   47
       SUM42=DEC4*SUM4
                                                                                F
       SUM5=A5+B5T+C5E
                                                                                   48
       SUM6=A6+B6T
                                                                                F
                                                                                   49
                                                                                   50
       SUM33=DEC2*SUM2
                                                                                   51
      SUM34=DEC3*SUM3
                                                                                F
                                                                                   52
       SUM35=DEC5*SUM5
                                                                                F
                                                                                   53
      B4T4=DEC4*B4T
                                                                                   54
      TIR=TI-TR
```

#### APPENDIX - Concluded

```
TIR2=TI2-TR2
                                                                                    55
      TIR3=TI3-TR3
                                                                                    56
      TIR4=TI4-TR4
                                                                                 F
                                                                                    57
      TIOR=TI/TR
                                                                                 F
                                                                                    58
      SUM7=SA4*ALOG(TIOR)+SB4*TIR+SC42*TIR2+SD43*TIR3+SR
                                                                                    59
      EMKIR=EMKTI-EMKTR
                                                                                    60
      SUM8=JK*EMKIR*SUM1+SUM7.
                                                                                 F
                                                                                    61
      SUM39=B2-K*C2E
                                                                                 F
                                                                                    62
      SUM 9= J*SUM39
                                                                                 F
                                                                                    63
      SUM40=83-K*C3E
                                                                                 F
                                                                                    64
      SUM10=J2*SUM40
                                                                                F
                                                                                    65
      SUM41=85-K*C5E
                                                                                 F
                                                                                    66
      SUM11=J4*SUM41
                                                                                 F
                                                                                    67
      SUM12=SUM9*OVRB+SUM10*OVRB2+SUM11*OVRB4
                                                                                 F
                                                                                    68
      SUM16=SA4*TIR+SB42*TIR2+SC43*TIR3+SD44*TIR4
                                                                                 F
                                                                                    69
      SUM17=J*(EMKTI*(KTI+1.)-SUM18)*SUM1
                                                                                 F
                                                                                    70
      SUM19=JVR*(R*OVRB*TIR+OVRB2*(B2*TIR+C2*EMKIR)+OVxB3*(B3*TIR+C3*EMK
                                                                                    71
     11R)+OVRB4*(B4*TIR)+OVRB5*(B5*TIR+C5*EMKIR)+B6*EAVR*TIR)
                                                                                    72
      SUM20=-J*(RTI*SUM21+SUM33*SUM22+SUM34*SUM23+SUM24+SUM35*SUM25)-JVR
                                                                                 F
                                                                                    73
     122*(-B4T4*OVRB5+AER*SUM6)-JVR*(B4T*OVRB4+SUM6*EAVR)
                                                                                 F
                                                                                    74
      SUM32=SUM16+SUM17+SUM19+SUM20
                                                                                 F
                                                                                    75
      RETURN
                                                                                F
                                                                                    76
      END
                                                                                F
                                                                                    77-
      SUBROUTINE VVAR (VI)
                                                                                 G
C
             THIS SUBROUTINE CALCULATES V TERMS
                                                                                     2
                                                                                G
      REAL K.KTI.KTR. J. JVI. JVI22. J8403. J860A. J2. J4. JK. JK. JVR. JVR. JVR. 22. JVI2
                                                                                 G
                                                                                     3
      COMMON /BLOCK/ J.R.A2.B2.C2.A3.B3.C3.A4.B4.A5.B5.C5.A6.B6.SB.K.ALP
                                                                                G
                                                                                     4
     1HA.SA4,SB4,SC4,SD4,SR,TR,VR,HR,TR2,TR3,TR4,KTR,EMKTR,VRMB,VRMB2,VR
                                                                                G
                                                                                     5
     2MB3.VRMB4.VRMB5.VRMB22.VRMB33.VRMB44.VRMB55.UVRB.OVRB2.UVRB3.OVRB4
                                                                                     6
     3, OVRB5, AVR, EAVR, SUM1, JB403, JB60A, SUM18, SB42, SC43, SD44, SC42, SD43, J2
                                                                                G
                                                                                     7
     4.J4.JK.JR.JVR.SUM21.SUM22.SUM23.SUM24.SUM25.JVR22.AER.RTI.OVIB.SUM
                                                                                 G
                                                                                     8
     52+0VIB2+SUM3+0VIB3+SUM4+0VIB4+SUM5+0VIB5+SUM6+EAVI+SUM14+SUM9+SUM1
                                                                                     9
                                                                                 G
     60, SUM11, SUM12, SUM8, SUM32, SUM26, SUM33, SUM28, SUM34, SUM29, SUM30, SUM35
                                                                                    10
     7.SUM31, JVI22, B4T4, AEI, JVI, B4T, SUM36, SUM37, SUM38, SUM39, SUM40, SUM43,
                                                                                 G
                                                                                    11
     8SUM41.SUM42.DVIB6.JVI2.VI2.DEC1.DEC2.DEC3.DEC4.DEC5.KTI
                                                                                 G
                                                                                    12
      VIMB=VI-SB
                                                                                G
                                                                                    13
      VIMB2=VIMB*VIMB
                                                                                 G
                                                                                    14
      VIMB3=VIMB2*VIMB
                                                                                G
                                                                                    15
      VIMB4=VIMB2*VIMB2
                                                                                G
                                                                                    16
      VIMB5=VIMB2*VIMB3
                                                                                G
                                                                                    17
      VIMB6=VIMB3*VIMB3
                                                                                G
                                                                                    18
      VIMB22=VIMB2*DEC2
                                                                                G
                                                                                    19
      VIMB33=VIMB3*DEC3
                                                                                G
                                                                                    20
      VIMB44=VIMB4*DEC4
                                                                                 G
                                                                                    21
      VIMB55=VIMB5*DEC5
                                                                                G
                                                                                    22
      OV I B= DEC 1/V I MB
                                                                                 G
                                                                                    23
      OVIB2=DEC1/VIMB2
                                                                                G
                                                                                    24
      OVIB3=DEC1/VIMB3
                                                                                    25
                                                                                G
      OVIB4=DEC1/VIMB4
                                                                                G
                                                                                    26
      OVIB5=DEC1/VIMB5
                                                                                 G
                                                                                    27
      OVIB6=DEC1/VIMB6
                                                                                G
                                                                                    28
      SUM36=C2/VIMB+C3/VIMB22+C5/VIMB44
                                                                                 G
                                                                                    29
      AVI=ALPHA*VI
                                                                                G
                                                                                    30
      EAVI=EXP(AVI)
                                                                                G
                                                                                    31
      SUM43=B6*EAVI+B4*OVIB4
                                                                                G
                                                                                    32
      SUM27=ALOG(VIMB/VRMB)
                                                                                 G
                                                                                    33
      SUM13=JR*SUM27
                                                                                G
                                                                                    34
      SUM14=SUM13-JB403*(OVIB3-DVRB3)+JB60A*(EAVI-EAVR)
                                                                                 G
                                                                                    35
       JV[=J*V[
                                                                                 G
                                                                                    36
      VI2=VI*VI
                                                                                 G
                                                                                    37
       JV I 2 = J*V I 2
                                                                                G
                                                                                    38
       JVI22=JVI2/DEC2
                                                                                 G
                                                                                    39
      AEI=ALPHA*EAVI
                                                                                G
                                                                                    40
      SUM26=SUM27-SB*OVIB
                                                                                G
                                                                                    41
      SUM28=OVIB+SB/VIMB22
                                                                                G
                                                                                    42
      SUM29=DEC1/VIMB22+SB/VIMB33
                                                                                 G
                                                                                    43
      SUM30=DEC4*A4*(DEC1/VIMB33+SB/VIMB44)
                                                                                    44
                                                                                G
                                                                                    45
      SUM31=DEC1/VIMB44+SB/VIMB55
                                                                                 G
                                                                                G
                                                                                    46
      RETURN
      END
                                                                                G
                                                                                    47-
```

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# Table 1.- Thermodynamic properties of $\mathtt{CF}_4$ at $\mathtt{Constant\ entropy}$

#### [Temperatures are in kelvins]

T	v	p	H/RT <sub>O</sub>	Á	$c_{p/R}$	γ	G	Z	$\mu$	k	$N_{\mathbf{Pr}}$
	S/R=24.25										
223.473 230.039	•0029 •0026	32.763 37.471			42.3294 37.4263				.00001857		
				S/F	R=24.50						
220.190 230.190 238.321	.0036 .0030 .0026	29.622 36.165 42.623		111.695	24.9064 25.2464 24.0046	3.661	1.133	.506	.00001702 .00001874 .00002037	.01579	2.829
				. \$/1	R=24.75						
215.139 225.139 235.139 245.139 247.075	.0046 .0038 .0032 .0027	37.822 46.165	9.9643 10.0717 10.1903 10.3297 10.3603	114.283 117.523 123.093	18.9522 18.7916	2.731 2.782 2.714	1.086 1.127 1.203	.565 .552 .544	.00001560 .00001696 .00001856 .00002044 .00002084	.01410 .01577 .01767	2.070 2.107 2.053
				\$7	R=25.00						
208.260 218.260 228.260 238.260 248.260 256.166	.0062 .0051 .0042 .0035 .0030	25.095 30.775 37.556 45.742	1C.0426 10.1537 10.2677 1C.3891 10.5253 1C.6509	118.423 119.821 122.430 126.894	13.6799 14.6772 15.4773 15.8746	2.144 2.238 2.305 2.320	1.079 1.088 1.115 1.170	.630 .612 .597 .587	.00001433 .00001542 .00001667 .00001811 .00001980	.01251 .01390 .01546 .01721	1.594 1.663 1.713 1.726
				\$/	R=25.25						
199.751 209.751 219.751 229.751 239.751 249.751 259.751 265.566	.0088 .0072 .0059 .0049 .0040 .0034 .0029	19.032 23.627 29.092 35.589 43.347 52.712	10.0767 10.1980 10.3184 10.4397 10.5648 10.6990 10.8503 10.9509	123.059 123.755 124.887 126.856 130.181 135.486	10.8563 11.6275 12.4171 13.1574 13.7410 14.0497	1.798 1.863 1.931 1.995 2.039 2.048	1.097 1.089 1.091 1.105 1.140 1.200	.697 .677 .659 .643 .630	.00001323 .00001413 .00001512 .00001623 .00001751 .00001898 .00002069	.01104 .01223 .01352 .01495 .01653	1.313 1.358 1.408 1.456 1.490 1.500
S/R=25.50											
190.295 200.295 210.295 220.295 230.295 240.265 250.295 260.295 270.295	.0129 .0104 .0085 .0069 .0057 .0047 .0039 .0033 .0026	13.611 17.164 21.440 26.546 32.615 39.825 48.426 58.787	10.0660 10.1994 10.3315 10.4619 10.5918 10.7229 10.8586 11.0044 11.1643 11.2607	127.118 127.889 128.663 129.655 131.164 133.586 137.422 143.265	9.0601 9.6224 10.2256 10.8592 11.4979 12.0931 12.5727 12.8613	1.596 1.633 1.677 1.726 1.778 1.826 1.860 1.870	1.097 1.102 1.121 1.158 1.221	.759 .741 .723 .704 .688 .673 .663	.00001229 .00001306 .00001389 .00001478 .00001690 .00001818 .00001965 .00002136	.00 973 .01 077 .01 189 .01 309 .01 439 .01 583 .01 741	1.149 1.172 1.201 1.237 1.275 1.312 1.340 1.352

### TABLE I.- THERMODYNAMIC PROPERTIES OF CF<sub>4</sub> AT CONSTANT ENTROPY — Continued

T	v	p	H/RTo	A	$c_p/R$	γ	G	Z	μ	k	$N_{\mathbf{Pr}}$
	S/R=25.75										
180.752 190.752 200.752 210.752 220.752 230.752 240.752 250.752 260.752 270.752 280.752 285.400	.0194 .0155 .0125 .0101 .0082 .0068 .0056 .0046 .0039 .0033	9.335 11.972 15.195 19.101 23.793 29.390 36.039 43.930 53.337 64.628	10.5925	130.016 131.211 132.231 133.165 134.165 135.448 137.309 140.136 144.402 150.672	11.3474 11.7654 12.0429	1.476 1.496 1.521 1.551 1.586 1.626 1.667 1.704 1.732	1.153 1.138 1.124 1.113 1.106 1.105 1.113 1.134 1.174 1.237	.813 .798 .781 .764 .747 .730 .715 .703 .694	.00001149 .00001220 .00001293 .00001369 .00001541 .00001640 .00001752 .00001880 .00002027 .00002282	.00861 .00956 .01054 .01159 .01271 .01392 .01523 .01666 .01825	1.053 1.060 1.074 1.094 1.118 1.147 1.179 1.209 1.234 1.248
				S/F	R=26.00						
171.715 181.715 191.715 201.715 211.715 221.715 231.715 241.715 251.715 261.715 271.715 281.715 291.715	.0293 .0232 .0185 .0149 .0120 .0098 .0080 .0066 .0054 .0038 .0032 .0029	8.146 10.502 13.405 16.549 21.234 26.373 32.495 35.761 48.377 58.635 70.916	10.1075 10.2612 10.4145 10.5669 10.7181	133.391 134.868 136.142 137.282 138.393 139.632 141.218 143.448 146.695 151.413 158.136	10.8318 11.2035 11.4686 11.5400	1.404 1.413 1.426 1.442 1.463 1.518 1.550 1.614 1.638 1.649	1.178 1.163 1.149 1.136 1.124 1.115 1.111 1.113 1.113 1.148 1.190 1.254	.858 .845 .831 .816 .800 .785 .769 .754 .741 .730 .724	.00001079 .00001147 .00001216 .00001286 .00001386 .00001516 .00001606 .00001706 .00001818 .00001945 .00002259 .00002335	.00768 .00855 .00946 .01041 .01140 .01246 .01358 .01480 .01611 .01755 .01914	.994 .993 .997 1.005 1.017 1.035 1.056 1.081 1.134 1.137 1.171
				*	l=26•25						
163.453 173.453 183.453 193.453 203.453 223.453 223.453 243.453 243.453 263.453 273.453 273.453 273.453 273.453 273.453 273.453 273.453	.0442 .0348 .0275 .0219 .0176 .0142 .0115 .0094 .0077 .0063 .0053 .0044 .0037 .0032 .0027	5.477 7.161 9.271 11.888 15.104 19.016 23.735 29.383 36.102 44.066 53.501 64.723 78.131	\$.8764 10.0362 10.1574 10.3594 10.5217 10.6835 10.8444 11.0041 11.1626 11.3202 11.4783 11.6393 11.8071 11.9874 12.1892 12.2576	134.523 136.477 138.197 139.711 141.065 142.336 143.639 145.138 147.060 149.697 153.418 153.659 165.924	11.0681	1.358 1.361 1.366 1.375 1.386 1.400 1.418 1.440 1.465 1.492 1.526 1.5566 1.576	1.198 1.184 1.170 1.157 1.145 1.124 1.118 1.116 1.121 1.136 1.121 1.136 1.208 1.274	.892 .882 .871 .859 .846 .832 .817 .803 .775 .764 .755 .752	.0001019 .00001085 .00001151 .00001218 .00001356 .00001428 .00001596 .00001576 .00001776 .0000188 .0000188 .0000188 .0000188	.006 89 .00772 .00858 .00946 .01037 .01133 .01233 .01340 .01453 .01576 .01708 .01853 .02013 .02189	1.031 1.055 1.078 1.099 1.114

# TABLE I.- THERMODYNAMIC PROPERTIES OF $CF_4$ AT CONSTANT ENTROPY — Continued

. <b>T</b>	v	p	H/RTo	A	$c_p/R$	γ	G	$\mathbf{z}$	μ	k	$N_{\mathbf{Pr}}$
S/R=26.50											
156.012 166.012 176.012 196.012 206.012 216.012 236.012 246.012 256.012 256.012 266.012 276.012 286.012 296.012 306.012 317.540	.0664 .0519 .0408 .0322 .0256 .0205 .0165 .0133 .0108 .0089 .0073 .0061 .0051 .0043 .0036 .0031	4.855 6.365 8.264 10.633 13.559 17.140 21.483 26.707 32.944 40.351 49.121 55.508 71.830 86.541	9.9590 10.1254 10.2938	137.224 139.370 141.295 143.018 144.574 146.019 147.438 148.556 150.748 153.047 156.147 160.407 166.253 174.166	10.5626 10.7953	1.329 1.328 1.329 1.331 1.336 1.344 1.354 1.383 1.402 1.424 1.448 1.471 1.493 1.518	1.213 1.200 1.188 1.175 1.163 1.152 1.141 1.132 1.124 1.122 1.131 1.149 1.181 1.229 1.297	.919 .911 .902 .892 .870 .858 .845 .832 .818 .806 .794 .785 .779 .778	.00001578 .00001661 .00001752 .00001854 .00001968	.00623 .00703 .00708 .00868 .00955 .01043 .01136 .01232 .01334 .01442 .01557 .01681 .01815 .01962 .02123	1.036 1.056 1.070
S/R=26.75											
149.361 159.361 179.361 189.361 199.361 209.361 229.361 239.361 259.361 259.361 259.361 279.361 289.361 299.361 309.361 309.361 319.361 328.805	.0989 .0767 .0599 .0471 .0372 .0296 .0236 .0193 .0125 .0102 .0084 .0069 .0058 .0048 .0041 .0035 .0035	3.291 4.361 7.24 7.447 9.603 12.279 15.570 19.580 24.426 30.236 37.157 45.360 55.059 66.538		137.331 139.642 142.141 144.233 146.136 147.671 149.483 151.036 152.628 154.395 156.523 159.249 162.872 167.746		1.310 1.306 1.304 1.303 1.304 1.307 1.311 1.318 1.328 1.340 1.354 1.372 1.391 1.412 1.433 1.443 1.4451	1.226 1.214 1.202 1.190 1.178 1.167 1.157 1.147 1.138 1.130 1.125 1.130 1.125 1.130	.939 .933 .926 .919 .901 .891 .880 .869 .857 .845 .833 .822 .812 .804	.00000922 .0000986 .00001050 .00001117 .00001242 .03001306 .0001372 .00001508 .00001508 .00001657 .00001834 .0000193 .0000193 .0000193 .0000193 .0000193 .0000193 .0000193 .00002053 .00002495	.00566 .00644 .00726 .00805 .00807 .00971 .01058 .01148 .01242 .01339 .01452 .01669 .01795 .01931 .02080 .02243	1.023
				\$/1	R=27.00						
143.410 153.410 163.410 183.410 193.410 203.410 213.410 223.410 243.410 253.410 263.410 273.410 293.410 303.410 303.410 303.410 303.410 303.410 303.410 303.410 303.410 303.410 303.410 303.410	.1459 .1125 .0873 .0683 .0537 .0424 .0337 .0269 .0216 .0174 .0142 .0115 .0095 .0074 .0046 .0033 .0029 .0026	2.991 3.563 5.2C5 6.778 8.752 11.211 14.246 17.961 22.469 27.896 34.382 42.C87 51.203 61.976 85.764	9.8[46	139.802 142.415 144.833 147.061 151.002 152.766 154.454 156.142 157.940 159.997 162.508 165.718 169.926 175.483 182.792	10.3134	1.298 1.293 1.285 1.285 1.283 1.286 1.291 1.296 1.316 1.306 1.347 1.365 1.383 1.401 1.412	1.237 1.225 1.213 1.202 1.191 1.180 1.160 1.151 1.142 1.135 1.135 1.130 1.128 1.139 1.155 1.182 1.278	.954 .950 .944 .939 .925 .917 .908 .899 .878 .867 .856 .837 .830 .825 .833	.00000882 .00000946 .00001010 .00001073 .00001135 .00001261 .00001324 .00001324 .00001454 .00001520 .00001520 .00001740 .00001826 .00001740 .00001920 .00002145 .00002279 .00002432 .00002549	.00517 .00594 .00672 .00751 .00831 .00912 .00995 .01080 .01168 .01259 .01354 .01453 .01558 .01669 .01789 .01789 .01917 .02056 .02208	.989 .941 .909 .887 .873 .864 .859 .863 .868 .875 .885 .910 .926 .944 .963 .982 .998 1.008

# TABLE I.- THERMODYNAMIC PROPERTIES OF $CF_4$ AT CONSTANT ENTROPY — Continued

<b>T</b>	v	p p	H/RTo	A	$c_{f p}/\!\!\!/{f R}$	γ	G	z	$\mu$	k	$N_{\mathbf{Pr}}$	
S/R=27.25												
138.054	.2135	• 584		126.058	5.0432				.00000847			
148.054	.1637	.814		129.684	5.2442 5.4482				.00000911		•952 •911	
158.054 168.054	.1265	1.121 1.526	9.9039 10.0807		5.6555				.00001037		.883	
178.054	.0769		10.2614		5.8664				.00001099		.865	
188.054	.0605		10.4456		6.0812				.00001161		.852	
198.054	.0479		10.6330	144.959	6.3004				.00001223	.00862	-844	
208.054	.0381		10.8231		6.5247				.00001284		•840	
218.054 228.054	.0304. .0244		11.0153		6.7546 6.9908				.00001347	.01024	.839 .840	
238.054	.0197		11.4040		7.2343				.00001473		.843	
248.054	.0160		11.5992		7.4860				.00001538		.847	
258.054	.0130		11.7943		7.7468	1.280	1.139	.896	.00001604	.01376	.853	
268.054	.0107		11.9889		8.0175				.00001673		.861	
278.054	.0088			161.360	8.2985				.00001747		.871	
288.054	.0073		12.3761		8.5893 8.8881				.00001827		.882 .896	
298.054 308.054	.0061		12.7649		9.1911				.00002011		•912	
318.054	.0043		12.9643		9.4918				.00002119		.929	
328.054	.0037		13.1719		9.7814			.845	.00002241	.02188	.946	
338.054	•0032		13.3936		10.0475				.00002379		•964	
348.054	.0028		13.6372		10.2781				.00002535		•980	
352.090	.0026	108.392	13.7440	195./10	10.3586	1.399	1.330	.862	.00002604	.02584	•98 <del>6</del>	
•				S/F	R=27.50							
•												
133.222	.3097	. 392	9.4944	124.699	4.8936	1.297	1.265	.976	.00000815	.00361	1.044	
143.222	.2364	.550		128.494	5.0857				.00000879		•968	
153.222	.1818	.763		132.098	5.2800				.00000943		.919	
163.222	.1408		10.0122		5.4768				.00001005		.885	
173.222	.1097		10.1940		5.6761				.00001067		-862	
183.222 193.222	.0859		10.3799	141.838	5.8782 6.0835				.00001129		.846 .835	
203.222	.0536			147.488	6.2923				.00001250		.828	
213.222	.0426		10.9592		6.5051				.00001311		.825	
223.222	.0341		11.1579		6.7225				.00001372		•823	
233.222	.0273		11.3586		6.9449				.00001434		.824	
243.222	.0221		11.5608		7.1733				.00001496		•827	
253,222 263,222	.0179		11.7638		7.4084 7.6511				.00001559		•831 •836	
273.222	.0119		12.1702	162.723	7.9022				.00001629		.843	
283.222	.0098		12.3728	164.652	8.1622				.00001759		•851	
293.222	.0081		12.5749	166.717	8.4312				.00001834		.861	
303.222	.0068		12.7769		8.7084				.00001916		.872	
313.222	.0057		12.9797		8.9917				.00002005		•886	
3.23.222	.0048		13.1854		9.2769				.00002105		.901	
333.222 343.222	.0041		13.3967	179.604	9.5583 9.8264				.00002217		•917 •934	
353.222	.0035		13.8570						.00002342		•954	
363.222	.0026		14.1210		10.2834				.00002464		.966	
364.087		115.060							.00002658		.968	

TABLE I.- THERMODYNAMIC PROPERTIES OF  $CF_4$  AT CONSTANT ENTROPY — Continued

T	v	р	H/RT <sub>o</sub>	A	c <sub>p</sub> /R	γ	G	z	μ	k	$N_{\mathbf{Pr}}$	
S/R=27.75												
3117-21912												
128.849	• 4458	. 26 5	9.4304	123.322	4.7709	1.295	1.272	.982	.00000787	.00328	1.082	
138.849	.3388	.375		127.259	4.9564				.00000851		• 990	
148.849	•2594	•523		131.006	5.1437				.00000914	•00477	.930	
158.849 168.849	•2001 •1553	•723 •987	10.1292	134.574	5.3326 5.5234				.00000977	.00553	.890 .862	
178.849	.1213		10.3159		5.7162				.00001100		.843	
188.849	•0952			144.298	5.9112				.00001161		.830	
198.849	•0751		10.7022		6.1087				.00001221		.821	
208.849 218.849	•0595 •0474		10.9C11 11.1032		6.3089 6.5124				.00001281		.815 .812	
228.849	.0379		11.3082		6.7194				.00001341		.811	
238.849	.0304		11.5156		6.9306					.01178	.812	
248.849	0246		11.7247		7.1466				.00001522		.814	
258.849	.0199		11.9351		7.3681				.00001583		.818	
268.849 278.849	.0162 .0133	17.561	12.1462 12.3575	165.820	7.5960 7.8308				.00001646		.823 .828	
288.849	.0109			167.823	8.0734				.00001777	.01623	.835	
298.849	.0090		12.7792		8.3240				.00001848	.01723	.843	
308.849	.0075		12.9897		8.5824				.00001924	.01828	.854	
318.849	.0063			174.915	8.8475		1.144		.00002008		.865	
328.849 338.849	.0053 .0045		13.4133		9.1167 9.3860				.00002100		.879 .893	
348.849	•0039		13.8544		9.6494				.00002202		909	
358.849	•0033		14.0916		9.8984			.886	.00002447	.02472	.926	
368.849		106.746							.00002593		.942	
376.306	•0026	121.834	14.5589	208.625	10.2732	1.346	1.351	• 906	.00002713	• 02764	.953	
				5.44	-20.00							
				5/1	₹=28.00							
124.865	-6371	.180		121.955	4.6685			. 987	.00000761	.00297	1.128	
134.865	4821	• 257		126.C13	4.8491				.00000825			
144.865	•3678 •2827	•361 •502		129.879 133.570	5.0310 5.2142				.00000889		•945 •898	
154.865 164.865	.2188		10.0674		5.3987				.00001013		.866	
174.865	.1703		10.2543		5.5846				.00001074		.843	
184.865	•1333		10.4460		5.7720				.00001135	.00748	.827	
194.865	.1048		10.6422		5.9610				.00001195		.816	
204.865 214.865	.0828 .0657		10.8427		6.1520 6.3452				.00001254		.808 .804	
224.865	.0524		11.2550		6.5408				.00001372		.801	
234.865	-0419		11.4660		6.7392			.958	.00001431		.801	
244.865	•0337		11.6797		6.9411				.00001490		.802	
254.865	• 02 72		11.8956		7.1468				.00001550		.804	
264.865 274.865	.0221 .0180		12.1131		7.3571 7.5725				.00001610		.807 .812	
284.865	-0147		12.5507		7.7939				.00001734	.01563	.817	
294.865	.0121	20.573	12.7699	170.880	8.0218	1.236	1.137	• 922	.00001798	.01656	.823	
304.865	.0100		12.9889		8.2568				.00001865	.01753	.830	
314.865	-0083		13.2078 13.4268		8.4988 8.7476				.00001938		.839	
324.865 334.865	.0069 .0058		13.6470		9.0014				.00002016		.849 .861	
344.865	.0050		13.8701		9.2577				.00002197		.874	
354.865	.0042	70.173	14.0588	189.277	9.5123	1.294	1.193	.896	.00002303	.02329	.889	
364.865	.0036		14.3373		9.7588				.00002422		•904	
374.865 384.865	.0031	100.790	14.5915		9.9903				.00002556		.920 .935	
388.737		128.710							.00002769		•941	
								,				

# TABLE I.- THERMODYNAMIC PROPERTIES OF CF<sub>4</sub> AT CONSTANT ENTROPY - Continued

т	v	р	H/RT <sub>O</sub>	· A	c <sub>p</sub> /R	γ	G	$\mathbf{z}$	μ	k	$Np_{\mathbf{r}}$
S/R=28.25											
121.203 131.203 141.203 151.203 161.203 171.203 201.203 201.203 221.203 221.203 241.203 251.203 261.203 271.203 271.203	.9048 .6819 .5186 .3973 .3065 .2379 .1857 .1457 .1148 .0722 .0576 .0462 .0462 .0372 .0300 .0243 .0198	.660 .893 1.199 1.597 2.111 2.773 3.620 4.693 6.C49 7.749 9.867 12.489	9.4808 9.6513 9.8272 10.0086 10.1952 10.3869 10.7848 1C.9904 11.2002 11.4137 11.6307 11.8505 12.0728 12.52971 12.5227	139.648 142.987 146.190 149.261 152.204 155.021 157.714 160.290 162.750 165.104 167.363 169.549 171.690	4.5812 4.7582 4.9362 5.1150 5.2948 5.4755 5.6572 5.8401 6.0242 6.2097 6.3969 6.5860 6.7772 7.1683 7.3690 7.5740	1.285 1.274 1.264 1.255 1.247 1.240 1.228 1.224 1.220 1.217 1.213 1.213 1.213 1.213 1.215	1.270 1.258 1.247 1.236 1.226 1.217 1.200 1.192 1.184 1.170 1.163 1.157 1.157 1.154 1.146	.989 .988 .986 .985 .983 .982 .979 .974 .974 .968 .964 .960 .955 .950 .944 .939	.00001464 .00001522 .00001580 .00001639 .00001699	.00344 .00419 .00493 .00568 .00643 .00719 .00791 .00948 .01025 .01103 .01182 .01263 .01344 .01428 .01513 .01513	1.047 .963 .909 .871 .845 .827 .814 .798 .795 .793 .794 .796 .796 .796 .803 .808
301.203 311.203 321.203 331.203 341.203 351.203 361.203 391.203 401.203 401.203	.0026	24.418 30.160 37.026 45.189 54.841 66.209 79.581	15.4182	176.025 178.359 180.935 183.887 187.379 191.607 196.801 203.222 211.174 221.006 221.189	10.2885	1.227 1.234 1.242 1.251 1.261 1.271 1.282 1.292 1.300 1.306	1.137 1.138 1.142 1.150 1.163 1.183 1.211 1.249 1.299	.927 .921 .916 .912 .910 .909 .912 .918 .929	.0001822 .0001886 .00001955 .00002029 .00002109 .00002198 .00002296 .00002405 .00002528 .00002667 .00002821 .00002824	.01787 .01886 .01990 .02100 .02217 .02342 .02476 .02620 .02776	.813 .820 .827 .836 .847 .858 .871 .886 .901 .916
117.848 127.848 137.848 147.848 167.848 177.848 197.848 207.848 217.848 227.848 227.848 227.848 247.848 247.848 257.848 277.848 307.848 317.848 327.848 327.848 327.848 347.848 347.848 347.848 347.848 347.848	•0028	.635 .855 1.144 1.518 2.002 2.622 3.415 4.420 5.689 7.280 9.263 11.720 14.744 18.441 22.931 28.346 42.565 51.721 62.515	9.4285 9.5579 9.7729 9.9535 10.1395 10.5273 10.7288 10.9350 11.1459 11.3610 11.8026 12.0284 12.2570 12.4878 12.4878 12.9541 13.1886 13.4235 13.6586 13.8938 14.1296 14.6073 14.8534 15.1092 15.3800 15.6729	145.526 148.702 151.756 154.693 157.515 160.225 162.826 165.323 167.724 170.039 172.286 174.490 176.687 178.928 181.283 183.842 186.719 190.056 194.026 198.830 204.697 211.894 220.727	10.2114	1.286 1.274 1.264 1.255 1.246 1.232 1.220 1.212 1.208 1.204 1.209 1.204 1.209 1.204 1.209 1.214 1.219 1.226 1.226 1.225 1.226 1.226 1.234 1.219 1.226 1.234 1.219 1.226 1.234 1.219 1.226 1.234 1.219 1.226 1.234 1.219 1.226 1.234 1.219 1.226 1.234 1.219 1.226 1.234 1.219 1.226 1.234 1.219 1.226 1.234 1.219 1.226 1.234 1.219 1.226 1.234 1.219 1.226 1.234 1.219 1.226 1.234 1.219 1.226 1.234 1.226 1.234 1.234 1.234 1.246 1.247	1.275 1.262 1.210 1.230 1.221 1.204 1.196 1.182 1.175 1.168 1.156 1.151 1.142 1.139 1.138 1.141 1.148 1.159 1.138 1.151 1.148 1.159 1.138 1.151 1.148 1.159 1.138 1.151 1.148 1.151	.992 .991 .989 .987 .988 .981 .978 .973 .969 .962 .957 .952 .937 .924 .922 .924 .923 .924 .923 .923 .924	.00000715 .00000779 .00000843 .0000997 .00000969 .0001030 .00001151 .00001210 .00001384 .00001384 .00001441 .00001498 .00001555 .0001612 .00001670 .00001788 .00001788 .00001976 .0000204 .0000204 .000020510 .00002510 .0000258	.00319 .00393 .00468 .00542 .00617 .00692 .00768 .00843 .00919 .01073 .01150 .01229 .01309 .01472 .01557 .01644 .01733 .01826 .01922 .02023 .02130 .02242 .02362 .02490 .02627 .02775 .02935	

т	v	p	H/RT <sub>o</sub>	A	c <sub>p</sub> /R	γ	G	z	μ	k	$N_{\mathbf{p_r}}$
				S/1	R=28.75						
114.727	1.7934	. C59		118.044	4.4400				•00000694		
124.727 134.727	1.3417	.086 .123		122.383 126.519	4.6123 4.7851				.00000759		1.120
144.727	.7725	.173		130.476	4.9583				.00000887		•935
154.727	•5929	. 241		134.271	5.1319				.00000.949		.888
164.727 174.727	•4580 •3558		10.0864		5.3060 5.4803				.00001011 .00001071		.854 .831
184.727	.2779		10.4731		5.6551				.00001131	.00743	.814
194.727	.2181		10.6744		5.8303					.00818	.802
204.727 214.727	.1719 .1361		10.8807		6.0060 6.1822				.00001249	.00894	•793 •787
224.727	.1081		11.3079	157.172	6.3590			.981	.00001364	.01046	.783
234.727	.0862	2.485	11.5283		6.5367			.979		.01122	.781
244.727 254.727	.0690		11.7527		6.7153 6.8952				.00001477	.01200	.781 .781
264.727	-0447		12.2125		7.0766				.00001589		.783
274.727	.0362		12.4471		7.2599				.00001645		.785
284.727 294.727	• 02 94 • 02 3 9		12.6842		7.4455 7.6339				.00001702 .00001759		.788 .791
304.727	•0196		13.1640		7.8255				.00001817		.795
314.727	.0161		13.4058		8.0210					.01776	.800
324.727 334.727	.0133		13.6482 13.8910		8.2208 8.4254				.00001936	.01867	•805 •811
344.727	.0092		14.1341		8.6351				.00002066		.818
354.727	•0077		14.3777		8.8496				.00002137		.826
364 • 727 374 • 727	•0065 •0055		14.6224		9.0684 9.2902				.00002215		•835 •846
384.727	.0047		15.1209		9.5128				.00002394		.857
394.727	.0041		15.3800		9.7328				.00002499		.870
404 •727 414 • 72 <b>7</b>	.0035		15.6510 15.9400		9.9459				.00002617	.02781	.884 .898
424.727	.0027		16.2550						.00002895		.912
427.242	•0026	149.942	16.3394	233.452	10.3751	1.275	1.374	.982	.00002934	.03141	.916
				5.41	3-30 00						
				,3/1	R=29.00						
111.848	2.5045	.041		116.835	4.3817				.00000675		
121.848	1.8676	.061 .087		121.249	4.5525				.00000740		
131.848 141.848	1.0695	.123		125.456	4.7236 4.8950				.00000805		.951
151.848	•8189	.172		133.339	5.0667	1.256	1.247	. 994	.00000.931	.00497	.897
161.848	.6313	• 237 • 325	10.0366		5.2385				.00000993		.860
171.848 181.848	.4895 .3816	• 440	10.2265		5.4106 5.5828				.00001054 .00001114		.834 .815
191.848	.2990	• 592	10.6227	147.402	5.7552	1.223	1.211		.00001173		.802
201.848 211.848	.2352 .1859		10.8288		5.9277				.00001231		•792
221.848	.1474		11.2563		6.1004 6.2734				.00001289	.00946	.785 .781
231.848	.1174	1.813	11.4773	159.650	6.4468	1.202	1.182	.984	.00001402	.01098	.778
241.848 251.848	.0938		11.7028		6.6206 6.7950				.00001458		•777
261 .848	.0605		12.1662		6.9703				.00001514		•777 •777
271.848	.0488	5.062	12.4035	170.357	7.1466	1.189	1.159		.00001624		.779
281 -848	•0395		12.6439 12.8872		7.3243				.00001679		.781
291.848 301.848	.0321 .0262		13.1327		7.5037 7.6853				.00001735		.784 .787
311.848	.0215	13.027	13.3800	179.855	7.8695	1.188	1.142	.961	.00001847	.01736	.791
321.848 331.848	.0176 .0146		13.6288 13.8785		8.0568				.00001905		•796
341.848	.0121		14.1288		8.2478 8.4427				.00001964		.800 .806
351.848	.0101	30.849	14.3795	189.416	8.6420	1.201	1.140	. 947	.00002088	.02100	.812
361.848 371.848	.0084 .0071		14.6308		8, 8458				.00002156		.819
381.848	•0060		15.1369		9.0536 9.2646				.00002229		.827 .836
391.848	.0051	67.095	15.3944	203.155	9.4774	1.228	1.182	.943	.00002397	. 02534	.847
401.848	.0044		15.6577		9.6896	1.236	1.205	.947	.00002495	.02660	-858
411.848 421.848	.0038	114.497	15.9307 16.2182		9.8976				.00002603		.871 .884
431.848	.0029	135.891	16.5270	230.400	10.2850	1.258	1.326		.00002125		898
440.468	.0026	157.219	16.8169	239.482	10.4329	1.262	1.379		.00002990		.910

T	. <b>v</b>	р	H/RT <sub>O</sub>	A	c <sub>p</sub> /R	γ	G	$\mathbf{z}$	μ	k	$N_{\mathbf{Pr}}$
				SZ	R=29.25						
109.164	3.4826 2.5886	.029 .043		115.671 120.155	4.3294				.00000657		
119.164	1.9448	.062		124.426	4.6688				.00000788		1.059
139.164	1.4748	.088		128.510	4.8389				.00000851		.968
149.164	1.1267	.123		132.426	5.0091 5.1794				.00000914		.908 .867
159.164 169.164	.8669	.170 .234	10.1786		5.3497				.00001037		.838
179.164	.5222	.318	10.3732	143.328	5.5200	1.230	1.222	. 993	.00001097	.00700	.818
189.164	4085		10.5733		5.6902				.00001157	.00774 .00849	.803
199.164	.3209		10.7789	153.169	5.8605 6.0306				.00001215		.785
209.164 219.164	.2005		11.2061		6.2007				.00001213		.779
229.164	.1594	1.324	11.4272	159.227	6.3709	1.200	1.185	.988	.00001386	.01075	.776
239.164	.1271		11.6533	162.117	6.5411				.00001442		.774 .773
249.164 259.164	.1017 .0817		11.8839		6.7115 6.8821				.00001497		.773
269.164	.0658		12.3580		7.0533				.00001606		.774
279.164	.0532		12.6008		7.2251				.00001660		.776
289.164 299.164	.0431		12.8469		7.3978 7.5718				.00001714		.778 .781
309.164	.0286		13.3478		7.7474			.970	.00001824	.01701	.784
319.164	.0235		13.6016		7.9250				.00001879		.788
329.164 339.164	.0193		13.8570 14.1137		8.1051 8.2881				.00001935	.01870	•792 •797
349.164	.0132		14.3712		8.4744				.00002051		802
359.164	.0110		14.6294	192.091	8.6644				.00002112		.807
369.164	.0092		14.8881		8 8 8 5 8 3					.02240	.813
379.164 389.164	.0078		15.1477		9.0560 9.2568				.00002247		.820 .829
399.164	.0056		15.6726		9.4598				.00002404		.838
409.164	.0048		15.9409		9.6635					•02685	.848
419.164	.0041		16.2171		9.8649				.00002596	.02813	.860 .872
439.164	.0031		16.8103					.985	.00002834	.03099	.885
449.164	.0028				10.4214				.00002974		.898
453.888	.0026	164.594	17.3076	245.453	10.4977	1.251	1.384	1.015	.00003045	.03338	.905
				\$/1	R=29.50						
	* *										
106.650	4.8235	. C21		114.552	4.2818				.00000641		
116.650 126.650	3.5740 2.6780	.030 .C44		119.102 123.432	4.4506				.00000707		1.264
136.650	2.0262	.063		127.570	4.7885				.00000835	.00383	986
146.650	1.5449	.088	9.7634		4.9576					.00458	.920
156.650 166.650	1.1864 .9168	•123 •169		135.355	5.1267 5.2957		1.243		.00000961		.875 .843
176.650	.7124		10.3270		5.4646				.00001082		.821
186.650	.5564		10.5263		5.6333				.00001141		.805
196.650	.4366	.417	10.7313		5.8018 5.9701				.00001200		.793 .784
206.650 216.650	.3440		11.1575		6.1381				.00001258		.778
226.650	.2160	.970	11.3785	158.751	6.3058	1.199	1.188	•991	.00001371	.01055	•774
236.650	.1720		11.6047		6.4734				.00001426		.772
246.650 256.650	.1375		11.8357 12.0714		6.6408 6.8080				.00001481	.01206	•771 •771
266.650	.0887	2.763	12.3116	170.069	6.9753	1.183	1.165		.00001590		.771
276.650	.0715		12.5559		7.1427				.00001643		.772
286.650	.0579	4.533	12.8041	113.261	7.3105	1.178	1.156	• 982	.00001697	.01514	.774

T	v	p	H/RT <sub>O</sub>	A	c <sub>p</sub> /R	γ	G	z	μ	k	$N_{Pr}$		
S/R=29.50													
296.650 306.650 316.650 326.650 336.650 356.650 366.650 386.650 396.650 406.650 426.650 436.650	.0470 .0382 .0312 .0256 .0211 .0174 .0144 .0120 .0101 .0085 .0072 .0061 .0052 .0045 .0039	7.302 9.205 11.552 14.429 17.937 22.191 27.320 33.467 40.793 49.477 59.720 71.749 85.847 102.280	13.0559 13.3108 13.5685 14.0904 14.3538 14.6183 14.8837 15.1497 15.4166 15.6847 15.9551 16.2291 16.7989 17.1029	180.208 182.604 184.569 187.326 189.704 192.142 194.693 197.422 200.414 203.769 207.610 212.077 217.336 223.567	7.4788 7.6479 7.8181 7.9898 8.3392 8.5178 8.6994 8.8843 9.0725 9.2637 9.4573 9.4573 9.8459 10.0365	1.175 1.174 1.175 1.176 1.176 1.182 1.186 1.190 1.196 1.202 1.209 1.209	1.148 1.144 1.141 1.137 1.137 1.137 1.139 1.142 1.148 1.157 1.169 1.187	.977 .974 .972 .969 .966 .963 .959 .958 .958 .958 .958	.00002023 .00002080 .00002139 .00002201 .00002266 .00002338 .00002415	.01672 .01753 .01836 .01920 .02007 .02096 .02188 .02283 .02383 .02488 .02597 .02714 .02837 .02969	.776 .779 .782 .786 .790 .794 .798 .809 .815 .822 .831 .840 .850 .862 .874		
456 - 650	.0030	143.711	17.4273	239.825	10.3944	1.235	1.325	1.006	.00002943	.03261	.886		
466.650 467.503									.00003087		•899 •900		
				S/F	k=29 <b>.</b> 75								
104.290 114.290 124.290 134.290 144.290 154.290 164.290 174.290 184.290 204.290 204.290	6.6560 4.9170 3.6749 2.7743 2.1111 1.6185 1.2487 .9690 .7558 .5922 .4660 .3682	.167 .226 .304 .406	9.2154 9.3785 9.5477 9.7227 9.9037 10.0906 10.2832 10.6858 10.6858 11.1108	141.855 145.333 148.705 151.976 155.154	4.2384 4.4064 4.5746 4.7429 4.9112 5.0794 5.2474 5.4153 5.5828 5.7501 5.9169 6.0833	1.297 1.284 1.271 1.260 1.250 1.240 1.232 1.224 1.217 1.210	1.294 1.281 1.268 1.256 1.246 1.236 1.227 1.219 1.211 1.203 1.196	.998 .998 .997 .997 .996 .996 .996 .995 .995	.0000,625 .0000691 .00000820 .00000884 .00001946 .00001007 .00011068 .00001127 .0001186 .00001244	.00217 .00292 .00366 .00440 .00514 .00588 .00663 .00737 .00811 .00886	1.323 1.121 1.005 .932 .883 .849 .824 .807 .794 .785		
224.290 234.290 244.290 254.290 264.290 274.290 284.290 304.290 314.290	.2919 .2323 .1854 .1485 .1192 .0961 .0776 .0629 .0511	.933 1.218 1.581 2.043 2.629 3.367 4.295 5.454 6.896	11.3315 11.5574 11.7884 12.0244 12.2652 12.5105 12.7600 13.0136 13.2708 13.5313	161.247 164.169 167.015 169.785 172.484 175.114 177.680 180.187 182.643	6.2494 6.4149 6.5801 6.7449 6.9093 7.0735 7.2375 7.4016 7.5658 7.7304	1.193 1.189 1.185 1.181 1.178 1.175 1.173	1.184 1.178 1.173 1.168 1.163 1.158 1.154 1.150	.992 .991 .990 .989 .987 .986 .984 .982	.0001357 .0001412 .00001467 .00001521 .00001575 .00001628 .00001734 .00001736	.01111 .01186 .01262 .01338 .01414 .01491 .01569 .01647	.774 .771 .769 .768 .769 .770 .771 .773 .775		
324.290 334.290 344.290 354.290 364.290 384.290 394.290 404.290 414.290	.0341 .0279 .0230 .0190 .0158 .0131 .0110 .0092 .0078	10.884 13.584 16.878 20.875 25.698 31.484 38.389 46.585 56.262	13.7948 14.0608 14.3290 14.5989 14.8701 15.1424 15.4156 15.6896 15.9647 16.2417	187.445 189.825 192.224 194.676 197.227 199.937 202.877 206.138 209.828	7.8958 8.0621 8.2298 8.3992 8.5707 8.7446 8.9212 9.1007 9.2829	1.168 1.169 1.170 1.172 1.174 1.177 1.181 1.186	1.140 1.138 1.137 1.137 1.138 1.141 1.146 1.153	.976 .973 .971 .969 .967 .965 .965	.0001892 .0001945 .00001999 .00002109 .00002166 .0000226 .00002288 .00002429	.01889 .01972 .02057 .02145 .02235 .02329 .02426 .02528 .02634	.781 .784 .788 .792 .796 .800 .805 .811 .817		
424.290 434.290 444.290 454.290 464.290 474.290 481.316	.0057 .0049 .0042 .0037 .0032	67.637 80.975 96.523 114.626 135.671 160.125	16.5216 16.8064 17.0990 17.4032 17.7243 18.0689	214.672 219.017 224.822 231.677 239.793 249.420	9.6531 9.8392 10.0230 10.2024 10.3743 10.5353	1.197 1.204 1.210 1.217 1.223 1.228	1.180 1.200 1.226 1.259 1.300 1.351	.969 .974 .982 .993 1.008 1.028	.00002508 .00002596 .00002693 .00002800 .00002920 .00003053 .00003155	.02747 .02865 .02992 .03126 .03271 .03426	.833 .842 .852 .863 .875 .887		

T	v	p	H/RT <sub>o</sub>	A	c <sub>p</sub> /R	γ	G	z	μ	k	$N_{\mathbf{Pr}}$
				5/1	R=30.00			٠			
102.070 112.070 122.070 132.070	9.1537 6.7423 5.0267 3.7857	.010 .015 .023	9.1806 9.3426	112.444 117.115 121.553 125.789	4.1983 4.3659 4.5335 4.7012	1.300 1.286	1.298 1.284	•998 •998	.00000610 .00000676 .00000742	.00201 .00275	
142.070 152.070 162.070 172.070 182.070	2.8765 2.2013 1.6960 1.3143 1.0238	.C46 .C64 .C89 .122	9.6845 9.8643	129.847 133.748	4.8689 5.0364 5.2038 5.3708 5.5375	1.262 1.251 1.242 1.233	1.259 1.248 1.238 1.229	•998 •997 •997	.00000870 .00000932 .00000994 .00001054 .00001114	.00497 .00572 .00646	.945 .891 .854 .828
192.070 202.070 212.070 222.070 232.070	.8013 .6299 .4971 .3938 .3130	.223 .298 .396 .523	10.6426 10.8515 11.0661 11.2862 11.5117	148.063 151.372 154.588 157.717	5.7038 5.8696 6.0349 6.1997 6.3638	1.217 1.210 1.204 1.198	1.213 1.205 1.198 1.192	•996 •996 •995	.00001173 .00001231 .00001288	.00795 .00869 .00944 .01018	.795 .785 .778 .773
242.070 252.070 262.070 272.070 282.070	.2496 .1996 .1602 .1288 .1040	1.513 1.950	11.7425 11.9785 12.2194 12.4652 12.7155	169.443 172.194	6.5274 6.6903 6.8526 7.0144 7.1757	1.184 1.180 1.176	1.175 1.170 1.165	•992 •992 •990	.00001454 .00001508 .00001562 .00001615	.01243 .01319 .01394	.768 .767 .767 .767
292.070 302.070 312.070 322.070 332.070	.0841 .0682 .0555 .0453	4.071 5.160 6.515 8.192	13.2290 13.4915 13.7576 14.0267	182.577 185.042 187.470	7.3366 7.4972 7.6577 7.8182 7.9791	1.168 1.166 1.165 1.164	1.152 1.148 1.145 1.142	.986 .985 .983	.00001719 .00001771 .00001823 .00001875	.01625 .01703 .01782 .01861	.770 .772 .775 .777
342.070 352.070 362.070 372.070 382.070	.0304 .0251 .0207 .0172 .0143	12.790 15.881 19.632 24.162	14.8489 15.1267 15.4056	192.271 194.686 197.148 199.699	8.1405 8.3027 8.4662 8.6312 8.7981	1.163 1.164 1.165 1.167	1.137 1.136 1.136 1.137	•977 •975 •974 •972	.00002085 .00002139 .00002195	.02025 .02109 .02196 .02285	.783 .787 .790 .794 .798
392.070 402.070 412.070 422.070 432.070 442.070	.01 20 .01 01 .0085 .0072 .0062	36.100 43.821 52.948 63.687	15.6856 15.9666 16.2486 16.5322 16.8183	205.286 208.466 212.026 216.077	8.9671 9.1384 9.3121 9.4878 9.6650 9.8428	1.173 1.177 1.182 1.187	1.144 1.150 1.160 1.174	.970 .970 .972 .975	.00002445	.02472 .02571 .02674 .02783	.803 .808 .813 .820 .827
452.070 462.070 472.070 482.070 492.070	.0046 .0040 .0035 .0031	90.979 108.080 127.944 150.988	18.3689	226.190 232.559 240.C48 248.872	10.0194 10.1930 10.3611 10.5207	1.199 1.205 1.211 1.216	1.214 1.243 1.279 1.323	.987 .997 1.010 1.028	.00002602 .00002692 .00002792 .00002903 .00003026	.03019 .03148 .03286 .03433	.835 .844 .854 .865 .876
495.330				263.071					.00003210		.891
99.974 109.974 119.974 129.974 139.974 149.974	12.5502 9.2175 6.8555 5.1524 3.9080 2.9861 2.2973	.007 .011 .016 .023 .033 .C47	9.1479 9.3087 9.4755 9.6483	111.451 116.179 120.667 124.947 129.046 132.984 136.778	4.1611 4.3283 4.4955 4.6628 4.8300 4.9971 5.1639	1.302 1.288 1.275 1.264 1.253	1.301 1.286 1.273 1.261 1.251	•999 •998 •998 •998	.00000597 .00000663 .00000728 .00000793 .00000919 .00000981	.00185 .00259 .00334 .00408 .00482	1.462
169.974 179.974 189.974 199.974 209.974 219.974 229.974	1.7780 1.3834 1.0816 .8494 .6697 .5299 .4208	.089 .121 .163 .219 .291	10.2025 10.3991 10.6014 10.8095 11.0234 11.2428 11.4677	140.444 143.991 147.432 150.773 154.621 157.184	5.3304 5.4964 5.6621 5.8271 5.9916	1.234 1.226 1.218 1.211 1.204 1.198	1.231 1.223 1.215 1.207 1.200 1.194	.998 .997 .997 .997 .996	.00001042 .00001101 .00001160	.00630 .00704 .00779 .00853 .00927 .01002	.832 .812 .797 .786 .779 .773

T	v	p	H/RT <sub>O</sub>	A	$c_p \! / \! R$	γ	G	z	μ	k	$Np_{\mathbf{r}}$
				5/,	₹=30.25						
239.974	.3353	.664	11.6981	163.269	6.4809	1.188	1.182	.995	.00001442	.01151	.767
249.974	.2679		11.9338		6.6424	1.183	1.176		.00001496		.766
259.974	•2147		12.1747		6.8032				.00001550		.765
269.974 279.974	.1726 .1391		12.4205	171.855	6.9633 7.1226				.00001603		.766
289.974	.1124		12.9266		7.2811				.00001655	.01452 .01528	•767 •768
299.974	.0911		13.1863		7.4391				.00001758	.01605	.770
309.974	.0740		13.4502		7.5965				.00001809	.01682	.772
319.974	.0603		13.7180		7.7534				.00001860		.774
329.974 339.974	•0492 •0404		13.9894		7.9101				.00001911		.777
349.974	.0332		14.2641		8.0668 8.2236				.00001962		.780 .783
359.974	•0273		14.8216		8.3809		1.136		.00002013		.786
369.974	.0226	14.939	15.1038	197.095	8.5389			.979			.789
379.974	.0188		15.3878		8.6979				.00002170		.793
389.974	.0156		15.6732		8.8582				.00002224		.797
399.974 409.974	.0131 .0110		15.9598		9.0202			-975	.00002280	• 02426	.801
419.974	.0093		16.5363		9.1839 9.3496			•975 •975	.00002337	.02519	.805 .810
429.974	.0079		16.8264		9.5170				.000023464		.815
439.974	•0067	59.893	17.1187	218.C80	9.6858				.00002534		.822
449.974	.0053		17.4142		9.8552				.00002611		.829
459.974 469.974	.0050	85.634	17.7147	227.636	10.0244	1.189	1.204		.00002695		.837
479.974	.0043	120.500	18.0229 18.3425	240 527	10.1913	1.195	1.229		•00002788		.846
489.974	.0033	142.206	18.6781	248.653	10.5545	1.206	1.300	1.028	.00002891	- 03446	.856 .866
499.974	•0029	167.332	19.0361	258.182	10.6581	1.211	1.347	1.048	.00003132	. 03596	.877
509.551	•0026	195.094	19.4072	269.863	10.7881	1.214	1.401	1.072	.00003265	.03750	.887
				\$/1	₹=30.50						
97.989	17.1592	. 005	9 0434	110 (05	4 12//	1 221		000	00000500		
107.989	12.5675	.009		110.495 115.278	4.1264 4.2932				.00000583		
117.989	9.3252	.012		119.813	4.4602				.00000715		1.232
127.989	6.9945	.C17		124.136	4.6271				.00000780		
137.989	5.2962	•024		128.272	4.7940				.00000844		.973
147.939	4.0406	• 034		132.245	4.9607				.00000907		•910
157.989 167.989	3.1044 2.3998	.047 .065	10.1653	136.071	5.1271 5.2932				.00000968		.867
177.989	1.8652		10.3608		5.4588		1.233	998	.00001029	-00615	.837 .815
187.989	1.4568			146.813	5.6239				.00001149		.799
197.989	1.1429		10.7695	150.182	5.7885				.00001207		.788
207.989	•9003			153.459	5.9523				.00001264		.779
217.989 227.989	.7118		11.2012		6.1155				.00001321		.773
237.989	•5648 •4496		11.4255		6.2778				.00001376		•769
247.989	.3589		11.8905		6.6000		1.183		.00001431		.767 .765
257.939	.2874	.833			6.7597				.00001539		.764
267.989	.2308		12.3768	171.484	6.9184	1.175	1.168	.994	.00001591		.765
277.989	.1859		12.6276		7.C762			• 994	.00001643	.01436	.765
287.989 297.989	.1501 .1215			175.961	7.2331				.00001695	.01511	.766
307.989	.0986		13.1435 13.4082	179.614	7.3891 7.5442				.00001746	.01587	•768
317.989	.0802			184.765	7.6985				.00001797	.01740	.770 .772
327.989	.0654		13.9501		7.8522					.01817	.774
337.989	.0535	5.817	14.2268	189.743	8.0053	1.156	1.142		.00001947	.01895	•777
347.989	.0439		14.5067		8.1580				.00001997		.780
357.989	.0361	9.1C8	14.7898	174.605	8.3105	1.154	1.137	•985	.00002048	•02054	.783

T	v	р	H/RT <sub>o</sub>	A	$c_{\mathbf{p}}/\mathbf{R}$	γ	G	$\mathbf{z}$	μ	k	$N_{\mathbf{Pr}}$
				\$/1	R=30.50			÷			
367.989 377.989 387.989 397.989 417.989 427.989 437.989 457.989 457.989 457.989 457.989 507.989 507.989	.0028	14.048 17.343 21.325 26.112 31.840 38.657 46.732 56.249 67.415 60.483 95.681 113.320 133.745 157.357	19.7252	197.023 199.455 201.928 204.471 207.127 209.946 212.661 216.337 220.072 224.300 229.139 234.716 241.180 248.696 257.455 267.680	8.4631 8.6159 8.7693 8.9236 9.0790 9.2356 9.3533 9.7139 9.8753 10.0366 10.1965 10.3533 10.65500 10.7850	1.154 1.155 1.156 1.160 1.163 1.166 1.171 1.175 1.180 1.185 1.191 1.190 1.201	1.134 1.135 1.136 1.140 1.145 1.153 1.163 1.177 1.195 1.217 1.245 1.279 1.320 1.370	.982 .981 .980 .979 .989 .984 .984 .988 .994 1.002 1.013 1.028 1.046	.00002308 .00002364 .00002422	.02218 .02302 .02388 .02477 .02568 .02663 .02761 .02864 .02971 .03084 .03203 .03464 .03607 .03760	.786 .789 .792 .796 .799 .803 .807 .812 .831 .839 .847 .867 .867
:				S/F	R=3C.75	•					
96.100 106.100 116.100 126.100 126.100 156.100 156.100 156.100 156.100 206.100 216.100 226.100 236.100 256.100		.065 .C88 .119 .159 .211 .278 .365 .476 .619 .801 1.033 1.326 1.696 2.161 2.743 3.470 4.374 5.495 6.878 8.580	9.0878 9.2464 9.4111 9.5817 9.7584	142.714 146.208 149.603 152.904 156.120 159.256 162.317 165.307 168.230 171.090 173.889 176.630 179.316 181.951 184.537 187.079 189.580 192.047 194.488 196.913 199.335	4.0937 4.2603 4.4270 4.5937 4.7603 4.9267 5.0929 5.2587 5.4240 5.5888 5.7529 6.0790 6.2408 6.4018 6.7206 6.8785 7.1909 7.3454 7.4989 7.6913 7.8027 7.9532 8.1028 8.2518 8.4002	1.308 1.293 1.280 1.267 1.256 1.2237 1.228 1.220 1.199 1.194 1.183 1.179 1.170 1.167 1.167 1.161 1.158 1.158 1.159 1.151 1.150	1.307 1.292 1.278 1.266 1.255 1.244 1.235 1.226 1.218 1.203 1.197 1.191 1.179 1.179 1.165 1.161 1.153 1.149	.999 .999 .999 .999 .999 .998 .998 .998	.00000703 .0000768 .0000895 .0000957 .00001018 .00001137 .00001253 .00001366 .00001420 .00001475 .00001581 .00001638 .00001638 .00001786 .00001786 .00001885 .00001984 .00001983	.00157 .00231 .00305 .00379 .00453 .00527 .00601 .00675 .00749 .00898 .00972 .01047 .01121 .01196 .01270 .01345 .01495 .0	2.675 1.638 1.274 1.093 .987 .873 .841 .880 .789 .766 .765 .764 .765 .767 .777 .778 .777 .778 .775 .777 .778 .783 .789
386.100 396.100 406.100 416.100 426.100 436.100 446.100 456.100 476.100 486.100 506.100 516.100 536.100 536.100 538.692	.0223 .0186 .0156 .0131 .0110 .0094 .0080 .0068 .0059 .0051 .0044 .0039 .0034	16.286 20.012 24.494 25.858 36.246 43.819 52.751 63.238 75.500 89.806 106.389 125.583 147.750 173.311 202.764	15.9236 16.2212 16.5204 16.8208 17.1224 17.7299 18.0367 18.3470 18.6622 18.9850 19.3187 19.6675 20.0372	204.242 206.779 209.417 212.202 215.188 218.443 222.046 226.C89 230.676 235.928 241.969 248.949 257.032 266.411 277.314	8.8445 8.9931 9.1422 9.2922 9.4432 9.57481 9.9015 10.0549 10.2057 10.3577 10.5041 10.6448 10.7776	1.150 1.151 1.152 1.154 1.167 1.163 1.168 1.172 1.177 1.182 1.187 1.192 1.192	1.133 1.133 1.135 1.138 1.143 1.149 1.159 1.171 1.206 1.231 1.261 1.298 1.341	.984 .983 .983 .984 .985 .991 .997 1.005 1.015 1.028 1.045 1.065		.02357 .02442 .02530 .02619 .02712 .02808 .02908 .03012 .03121 .03236 .03358 .03486 .03623 .03769	.789 .792 .795 .798 .801 .809 .814 .819 .825 .840 .848 .857 .876

#### TABLE I.- THERMODYNAMIC PROPERTIES OF $CF_4$ AT

#### CONSTANT ENTROPY - Continued

· m	17		TT /D.D.		<b>5</b>		_	_			
T	v	p	H/RT <sub>O</sub>	A	$c_{\mathbf{p}}/\mathbf{R}$	γ	G	Z	μ	k	$N_{\mathbf{Pr}}$
				S/	R=31.00						
				•							
	3 31.8269			108.691	4.0632			.999	.00000559	.00069	3.094
	23 23.1841 23 17.1251			113.578 118.203	4.2296 4.3962				.00000625		
	3 12.7960			122.604	4.5627				.00000691		
134.32				126.811 130.847	4.7291			. 999	.00000820	.00366	1.002
154.32				134.732	4.8953 5.0613				.00000884		.929 .880
164.32			10.0964		5.2268			.999	.00001007	.00588	.846
174.32 184.32			10.2901		5.3919 5.5564				.00001067		.821 .804
194.32			10.6951		5.7203	1.213	1.212	.999	.00001185	.00810	.791
204.32			10.9064		5.8835 6.0458				.00001243		.781 .774
224.32		.206	11.3463	158.763	6.2073	1.194	1.192	.998	.00001356	.01033	.769
234.32			11.5748 11.8088		6.3678 6.5272				.00001411		•766 •764
254.32	.5127	.461	12.0484	167.806	6.6856	1.179	1.175	.997	.00001518	.01256	.763
264.32 274.32			12.2934		6.8428 6.9989				.00001571		•763 •763
284.32	2664	.991	12.7990	176.282	7.1536				.00001623		.764
294.32 304.32			13.0595 13.3248		7.3072 7.4595				.00001725		•766
314.32	3 .1416		13.5948		7.6104				.00001775		•767 •769
324.32 334.32			13.8694		7.7602			.993	.00001875	.01782	.771
344.32			14.4312		7.9087 8.0561				.00001924		•773 •775
354.32			14.7179		8.2025			.991	•00002021	.02013	•778
364.32 374.32			15.0082 15.3018		8.3478 8.4924				.00002069		•780 •783
384.32	.0353	10.031	15.5983	201.614	8.6363	1.146	1.133	.988	.00002167	.02250	.786
394.32 404.32			15.8974 16.1988		8.7797 8.9228				.00002216		.788 .791
414.32	.0203	18.774	16.5022	209.046	9.0660	1.147	1.132	• 986	.00002316	.02498	.794
424.32 434.32			16.8072 17.1137		9.2092 9.3529				.00002368		.797
444.32	.0120	33.960	17.4214		9.4971				.00002420 .00002474		.800 .803
454.32 464.32			17.7305 18.0410		9.6419 9.7873				.00002531		.807
474.32	.0074	59.251	18.3535	227.886	9.9330	1.161	1.165	.994	.00002591 .00002655	. 03 056	.811 .815
484.32		70.754	18.6689	232 • 252	10.0787	1.165	1.179	1.000	.00002725	.03162	.821
504.32	3 .0048	99.745	19.3140	242.881	10.3689	1.174	1.219	1.016	.00002800 .00002883	.03390	.826 .833
514.32 524.32	.0042 .3 .0037	117.757	19.6484	249.387	10.5070	1.179	1.245	1.028	-00002974	.03513	.840
534.32		162.490	20.3594	265.515	10.5426	1.183	1.316	1.043	.00003075	.03644	.848 .857
544.32	3 •0029	190.030	2C.7468	275.498	10.8926	1.192	1.362	1.084	.00003308	.03931	.866
553.61	.4 .0026	219.290	21.1339	286.178	10.9954	1.195	1.412	1.109	.00003432	.04077	.874
				371	R=31.25						
92.63	2 43.1889	.002	8.8840	107.841	4.0344	1 220	1 270	1 000	.00000548	00057	2 475
102.63	2 31.3751	.003		112.778	4.2007	1.313	1.312	1.000	.000000346	.00131	1.863
	2 23.1249 2 17.2474			117.446 121.884	4.3670 4.5334	1.29 8	1.297	1.000	.00000680	.00205	1.369
	2 12.9969			126.124	4.6997				.00000745		
142.63				130.189	4.8658			•999	.00000873	• 00427	.939
162.63			10.0647	134.100 137.875	5.0316 5.1970				.00000935		.887
172.63			10.2574		5.3619			.999	.00001057	.00649	•825
192.63			10.4561		5.5263 5.6900				.00001117		•806 •792
202.63	2 -1615	.C87	10.8711	151.845	5.8530	1.207	1.206	.999	.00001233	.00872	•782
212.63			11.0874		6.0151 6.1763				.00001290 .00001346		•775 •770
232.63	2 1.0725	• 20 2	11.5372	161.382	6.3365	1.189	1.187	• 998	.00001401	. 01 095	.766
242.63 252.63	-		11.7706		6.4957 6.6537				.00001455		•764 •763
262.63	2 .5474	.446	12.2539	170.285	6.8105	1.175	1.172	.998	.00001562	.01318	.763
272.63 282.63			12.5037 12.7588		6.9660 7.1202				.00001614		•763 •764
292.63			13.0190						.00001716		.765
							•				

т	. <b>v</b>	p	H/RTo	<b>A</b>	$c_p/R$	γ	G	Z	μ	k	$N_{\mathbf{Pr}}$		
S/R=31.25													
302.632 312.632	.2316 .1879		13.2843 13.5544		7.4244 7.5744				.00001766		.766 .768		
3 22 •6 32 3 32 •6 32	•1528 •1246		13.8292 14.1086		7.7230 7.8701				.00001865		.770 .772		
342.632 352.632	.1018 .0833		14.3923 14.6801		8.0159 8.1602				.00001962		.774 .776		
362.632 372.632	.0684 .0563		14.9718 15.2671		8.3033 8.4452				.00002058		.779 .781		
382.632 392.632	•0464 •0384		15.5657 15.8673		8.5860 8.7258				.00002153		.783 .786		
402.632 412.632	.0319 .0265		16.1717 16.4785		8.8648				.00002250		.788 .791		
422.632 432.632	.0221 .0185		16.7874 17.0981	_	9.1412	1.143	1.131	•989	.00002348	•02554	•794 •796		
442.632 452.632	.0156	26.197	17.4103 17.7240	216.590	9.4165 9.5543	1.145	1.135	.989	.00002449	.02726	.799 .802		
462.632	.0111	38.408	18.0389	222.571	9.6922	1.149	1.144	•991	.00002556	.02907	.805 .808		
472.632 482.632	.0095 .0081	55.432	18.3553	229.679	9.9687	1.155	1.160	•997	.00002674	.03101	.812		
492.632 502.632	.0070	78.771		238.546	10.2441	1.162	1.189	1.008	.00002740	.03312	.816 .821		
512.632 522.632		110.223	19.9830	249.964	10.5135	1.171	1.232	1.028	.00002888	.03544	.827 .833		
532.632 542.632	•0040 •0035		20.3293						.00003066		.840 .848		
552 • 632 562 • 632									.00003281		.856 .864		
568.781	•0026	227.588	21.7392	291.923	11.0553	1.190	1.416	1.120	.00003487	.04189	.870		
				.\$/1	₹=31.50								
91.008	58.5027	.001	8.8602	107.015	4.0069	1.333	1.332	1.000	.00000537	.00045	4.539		
	42.3891	.002		112.002 116.711					.00000603				
	23.2099 17.4579	.005 .007		121.186 125.456					.00000735		1.172		
141.008 151.008	13.2501 10.1296	.010	9.6687	129.550 133.487		1.261	1.261	1.000	.00000863	.00415	•950 •894		
161.008 171.008	7.7964 6.0360	.C19	10.0343	137.284	5.1688 5.3336	1.241	1.240	.999	.00000987	•00563	.856 .828		
181.008	4.6976 3.6734	.C36	10.4239	144.515	5.4979	1.223	1.222	.999	.00001107	.00711	.808 .794		
201.008	2.8848	.065	10.8372	151.333	5.8243	1.208	1.207	.999	.00001224	.00860	.783 .776		
211.008	2.2744	.114	11.0527	157.802	5.9863	1.195	1.194	•999	.00001337	.01008	.770		
231.008	1.4287	.197	11.5009	163.572	6.3074	1.184	1.183	•999	.00001392	.01157	•766 •764		
251.008 261.008	•9087 •7279	•334	11.9719 12.2157	169.878	6.6241 6.7806	1.175	1.173	•998	.00001500	.01305	•763 •762		
271.008 281.008	•5847 •4706	• 555	12.4650 12.7196	175.551	6.9358 7.0896	1.167	1.164	.998	.00001605	.01454	.762 .763		
291.008 301.008	•3798 •3073		12.9795 13.2445		7.2419 7.3927				.00001707		•764 •765		
311.008 321.008	•2491 •2025		13.5145 13.7893		7.5421 7.6898				.00001807		•767 •769		
331.008 341.008	•1649 •1346		14.0689		7.8359 7.9805				.00001904		•771 •773		
351.008 361.008	.1101	2.955	14.6414	193.902	8.1235 8.2649	1.146	1.140	•995	.00002000	.01981	•775 •777		
371.008 381.008		4.629	15.2305 15.5306	198.817	8.4048 8.5433	1.143	1.135	.993	.00002095	.02134	•779 •782		
391.008 401.008	.0505 .0418	7.160	15.8342	203.658	8.6804 8.8163	1.140	1.132	•992	.00002142	.02289	•784		
411.008	•0347	10.935	16.4503	208.497	8.9510	1.139	1.129	.991	.00002283	• 02448	•786 •789		
431.008	•0289 •0242	16.481	16.7623 17.0765 17.3926	213.456	9.0848	1.139	1.130	.991	.00002331	.02612	.791 .793		
441.008 451.008	•0202 •0170		17.7104		9.3502 9.4821				.00002428		•796 •798		

т	v	p	H/RT <sub>O</sub>	A	$c_p/R$	γ	G	${f z}$	μ	k	$N_{\mathbf{Pr}}$	
				S/R	R=31.50							
461.008 471.008 481.008 491.008 501.008 521.008 531.008 551.008 551.008 561.008 571.009 581.008	.0038 .0034 .0030 .0027	35.882 43.182 51.769 61.824 73.549 87.193 102.961 121.148 142.067 166.C71 153.562 225.010	19.6503 19.9828 20.3213 20.6680 21.0263 21.4002 21.7951 22.2174	224.584 227.663 231.458 235.445 239.907 244.943 250.649 257.141 264.546 273.004 282.683 293.777	10.1379 10.2677 10.3963 10.5227 10.6460 10.7648 10.8779 10.9835 11.0799	1.144 1.146 1.149 1.152 1.156 1.160 1.164 1.168 1.173 1.177 1.181	1.141 1.147 1.156 1.167 1.181 1.198 1.219 1.245 1.275 1.311 1.353 1.402	.994 .996 .999 1.004 1.010 1.017 1.027 1.040 1.055 1.073 1.095	.00002529 .00002582 .00002637 .00002695 .00002757 .00002896 .00002975 .00003156 .00003261 .000033501 .00003543	.02959 .03053 .03149 .03249 .03354 .03463 .03577 .03698 .03825 .03959 .04101	.801 .803 .806 .809 .813 .817 .821 .827 .833 .839 .846 .854	
S/R=31.75												
99.450 109.450 119.450 129.450 139.450 149.450 159.450 169.450 169.450 209.450 229.450 229.450 229.450 239.450 239.450 239.450 239.450 239.450 239.450 339.450 339.450 339.450 339.450 339.450 339.450 339.450 349.450 349.450 349.450 349.450	79.1021 57.1738 41.9598 31.1832 23.4200 17.7523 13.55560 10.4231 8.0624 6.2697 4.8990 3.8447 3.0293 2.3955 1.9008 1.5129 1.2076 9686 .7763 .6245 .5038 .4073 .3301 .2681 .2182 .1780 .1455 .1192 .0979 .0806 .0665 .0550 .0456	.020 .027 .036 .C48 .064 .085 .112 .147 .192 .250 .323 .416 .535 .684 .872 1.108 1.403 1.771 2.229 2.798 3.500 4.366 5.429 6.732 8.321	8.9862 9.1409 9.3016 9.4685 9.6414 9.8203 10.0052 10.1962 10.3931 10.5559 10.8047 11.0193 11.2398 11.4660 11.6980 11.9356 12.1787 12.4274 12.6815 12.9409 13.2056 13.4753 13.7500 14.0296 14.3139 14.6026 14.3139 14.6026 14.3139 14.6026 15.1930 16.1073 16.4188	106 · 214 111 · 248 115 · 999 120 · 508 124 · 810 128 · 931 132 · 892 140 · 404 143 · 982 147 · 456 150 · 834 154 · 125 157 · 336 160 · 471 163 · 536 169 · 473 177 · 951 183 · 353 185 · 986 188 · 578 191 · 131 193 · 649 193 · 649 194 · 134 195 · 134 196 · 134 197 · 136 198 · 137 199 · 137 191 · 131 193 · 649 196 · 134 198 · 591 201 · 024 203 · 440 205 · 267 208 · 253 210 · 670	3.9806 4.1467 4.3129 4.4791 4.6452 4.8111 4.9767 5.1420 5.3067 5.4709 5.6345 5.7973 5.9592 6.1202 6.2801 6.4389 6.5965 6.7529 7.0614 7.2134 7.36599 7.8053 7.9619 8.2313 8.3666 8.6417 8.7752 8.9077 9.0378	1.318 1.302 1.282 1.275 1.263 1.252 1.242 1.216 1.202 1.196 1.196 1.175 1.167 1.163 1.159 1.154 1.154 1.154 1.141 1.141 1.141 1.141 1.141 1.141 1.141 1.141	1.318 1.302 1.287 1.274 1.262 1.251 1.224 1.218 1.208 1.201 1.195 1.184 1.174 1.160 1.153 1.150 1.153 1.151 1.141 1.138 1.141 1.138 1.138 1.141 1.138 1.139 1.139 1.139 1.139 1.139	1.000 1.000	.00001749 .00001799 .00001848 .00001894 .00001991 .00002038 .00002035 .00002132 .00002178 .00002271	.00107 .00181 .00255 .00329 .00404 .00478 .00552 .00626 .00770 .00848 .00922 .00996 .01071 .01145 .01219 .01293 .01368 .01442 .01517 .01591 .01666 .01741 .01891 .01966 .02042 .02195 .02195 .02195 .02195 .02272 .02350 .02508	2.166 1.481 1.201 1.051 .961 .961 .832 .811 .795 .776 .767 .764 .763 .7662 .7662 .7668 .7766 .7766 .7766 .7766 .7766 .7772 .7774 .7776 .7778 .7778 .7778 .7789	
429.450 439.450 449.453 459.450 469.450 479.450 509.450 519.450 529.450 539.450 559.450 579.450 579.450 579.450 579.450	.0316 .0264 .0221 .0186 .0157 .0133 .0113 .0097 .0083 .0071 .0062 .0054 .0041 .0037 .0033 .0029 .0026	12.543 15.418 18.813 22.878 27.723 33.474 40.271 48.267 57.635 68.563 81.282 95.984 112.941 132.437 154.792 180.365 209.569 242.877	17.0502 17.3695 17.6909 18.0140 18.3387 18.6648 18.9523 19.3212 19.6520 21.0109 21.3682 21.7383 22.1255 22.5354 22.5745	213.114 215.603 218.161 220.816 223.604 226.567 229.755 233.226 237.048 241.298 246.062 251.427 257.496 264.380 272.203 281.105 291.250 302.833	9.1672 9.2954 9.4226 9.5489 9.6746 9.7997 9.9242 10.0482 10.1715 10.5343 10.6507 10.7634 10.9725 11.0661 11.1502	1.136 1.136 1.137 1.138 1.140 1.142 1.147 1.150 1.154 1.158 1.166 1.170 1.174 1.177	1.128 1.129 1.131 1.131 1.134 1.144 1.152 1.162 1.174 1.189 1.203 1.257 1.289 1.326 1.370 1.420	.993 .992 .993 .994 .996 .998 1.005 1.011 1.018 1.025 1.048 1.052 1.068 1.012	.00002364 .00002411 .00002459 .00002558 .0000258 .00002608 .00002717 .00002775 .00002838 .00002906 .00002906 .00003060 .00003148 .00003466 .00003593 .00003593	.02589 .02670 .02753 .02837 .02924 .03013 .03104 .03198 .03296 .03397 .03503 .03614 .03730 .03851 .03980 .04116 .04259	.791 .793 .795 .797 .799 .801 .806 .809 .812 .816 .821 .826 .831	

T	v	p	H/RT <sub>o</sub>	Α	$c_p/R$	γ	G	Z	$\mu_{}$ .	k	$N_{\mathbf{Pr}}$
				S/1	R=32.00						
96.342	81.0701	-C01	8.9394	109.720					.00000572		
106.342		.002		114.554					.00000639		
116.342	43.8589	.002		119.135					.00000704		1.268
	32.8379	• 004		123.499						.00306	1.089
	24.8256	• 005		127.674					.00000833	.00380	.984 .917
	18.9133	.007		131.684					.00000896	.00455	.872
156.342 166.342	14.5129	.010 .014		135.547					.00001019	.00603	840
176.342	8.6999		10.3315						.00001079	.00677	.817
186.342	6.7881		10.5326						.00001139		.800
196.342	5.32Cl		10.7396		5.7455				.00001197		.788
206.342	4.1867		10.9525		5.9075				.00001254		.779
216.342	3,3070		11.1712		6.0686	1.198	1.197	.999	.00001311	.00973	.772
226.342	2.6212	.080	11.3957	159.527	6.2287	1.192	1.191	. 999	.00001366	.01047	.768
2.36 . 342	2.0843	.106	11.6260	162.616	6.3876	1.186	1.185	.999	.00001421	.01122	.765
246.342	1.6619	.138	11.8620	165.640	6.5454	1.181	1.180	.999	.00001475	• 01 1 96	.763
256.342	1.3296		12.1036		6.7019				.00001528	.01270	.762
266.342	1.0663		12.3508		6.8569				.00001580		•762
276.342	. 85 73		12.6034		7.0106				.00001632		.762
286 • 3 42	.6909		12.8615		7.1627				.00001683		.763
296.342 306.342	.5582 .4519		13.1248		7.3132 7.4620				.00001733		•764 •765
316.342	•3668		13.6670		7.6091				.00001783		.767
326.342	.2983		13.9456		7.7544				.00001880		.769
336.342	.2431		14.2290		7.8979				.00001928		.771
346.342	.1985		14.5172		8.0395				.00001976		.773
356.342	.1625		14.8098		8.1792				.00002022		.775
366.342	.1333		15.1068		8.3170				.00002069	.02092	.777
376.342	.1096	3.189	15.4080	200.396	8.4528	1.139	1.134	.996	.00002115	.02168	.779
386.342	•0902		15.7132	202.820	8.5868				.00002161		.781
396.342	.0745		16.0221	205.227	8.7189				.00002207	.02321	.783
406.342	.0617		16.3345		8.8492				.00002253		.785
416.342	.0511		16.6502		8.9777					•02477	.787
426.342	•0425		16.9688		9.1045				.00002344		.789 .791
436.342	.0355 .0296		17.2902 17.6141		9.2298 9.3535				.00002390		.793
456.342	.0249		17.9401		9.4759				.00002483	.02798	.794
466.342	.0209		18.2680		9.5971				.00002531	.02881	.796
476.342	.0176		18.5976		9.7173				.00002579	.02966	798
486.342	.0149		18.9287		9.8364				.00002628	.03053	.800
496.342	.0127		19.2612		9.9546				.00002678	.03143	.802
506.342	.0108	43.649	19.5951	234.421	10.0719	1.140	1.147		.00002731	.03234	.803
516.342	.0093	52.139	19.9306	238.038	10.1883	1.142	1.155	1.006	.00002787	.03329	.806
526.342	.0080	62.052	20.2680	242.C26	10.3037	1.145	1.166	1.010	.00002845	.03427	.808
536.342	.0069			246.461					.00002908	.03529	.811
546.342	.0060								.00002977	.03635	.814
556.342									.00003050		.818
566 • 342	•0046			263.300					.00003131		.823
576.342	.0041			270.412					.00003219	.03985	.828
586.342 596.342									.00003315	.04113	.833 .839
606.342									.00003535		•845
616.058									.00003555		.851
,				_ ,							

${f T}$	v	p	H/RT <sub>O</sub>	A	$c_p/R$	γ	G	z	μ	k	$\mathtt{N}_{\mathbf{Pr}}$
				S/R	=32.25						
104.134	81.4244	.001	9.0580	113.513	4.2238	1.310	1.310	1.000	.00000624	.00142	1.754
114.134	60.1251	.002	9.2156	118.146	4.3899	1.295	1.295	1.000	.00000690	.00216	1.325
124.134	44.9132	.003		122.556					•00000755		1.120
134.134		•004		126.771					.00000819		1.003
144.134		• 005		130.817						.00438	•930
154.134		•007		134.711					.00000945	.00512	.880
164.134		.010	10.0943							.00586	.846
174.134	9.2036		10.2881						.00001126	.00660	.821 .803
194.134	7.2063		10.6936		5.7086					.00809	•790
204.134	5.6659		10.9053		5.8707				.00001242	.00883	.780
214.134	4.4718		11.1228		6.0319				.00001298	.00957	.773
224.134	3.5417	•059	11.3461	158.852	6.1920			.999	.00001354	.01031	.768
234.134	2.8142	.078	11.5752	161.559	6.3511	1.187	1.187	.999	.00001409	.01105	.765
244.134	2.2430		11.8100		6.5089				.00001463		•763
254.134	1.7927		12.0505		6.6655					.01253	.762
264.134	1.4370		12.2966		6.8206				.00001569		•761
274.134	1.1545		12.5482		6.9743				.00001621		•762
284 • 134 294 • 134	•9299 •7508		12.8C53 13.0677		7.1264 7.2770					.01476 .01550	•762 •764
304.134	.6075		13.3354		7.4257				.00001722	.01625	.765
314.134	.4927		13.6083		7.5728				.00001821	.01699	.766
324.134	•4004		13.8862		7.7179				.00001869	.01774	.768
334.134	•3261		14.1691		7.8612				.00001917		•770
344.134	.2662	1.203	14.4567		8.0025					.01923	.772
354.134	.2177	1.513	14.7491	195.013	8.1418			.997	.00002011	.01999	.774
364.134	.1784	1.897	15.0459	197.499	8.2791	1.141	1.137	• 997	.00002058	. 02 074	•776
374.134	.1465		15.3471		8.4143				.00002104		.778
384.134	.1206		15.6525		8.5475				.00002149		.780
394.134	.0994		15.9618		8.6785				.00002195		.782
404.134	.0822		16.2749		8.8075				.00002240	.02378	.784
414.134	.0681 .0565		16.5916		8.9345 9.0594				.00002285	.02455 .02532	•786 •787
424.134	.0471		17.2346		9.1825				.00002335		.789
444.134	.0393		17.5604		9.3036				.00002420	.02689	.791
454.134	.0328		17.8887		9.4230				.00002465	.02770	
464.134	.0276		18.2194		9.5408				.00002511	.02851	.794
474.134	.0232		18.5520		9.6570			.996	.00002557	.02933	.795
484.134	• 01 96	22.997	18.8863	226.952	9.7717	1.131	1.130	.997	.00002605	.03017	.797
494.134	.0166	27.754	19.2223		9.8851				.00002653		.798
504.134	.0141	33.380	19.5597						.00002701		•800
514.134	•0120	40.009	19.8984		10.1081					.03280	.801
524.134	.0103		20.2386						.00002804		.803
534.134	•0089		20.5805						.00002860		.804
544.134 554.134	•0076 •0066	67.443 79.717	20.9245	252.C19					.00002919	.03567	.807
564.134	.0058	93.866	21.6224						.00003051	.03777	
574.134	.0051	110.142							.00003126	.03888	
584.134	.0045		22.3432						.00003207	. 04 005	.820
594.134									.00003295	.04128	-824
604.134		174.445							.00003391		
614.134									.00003497	.04393	.834
624.134									.00003610		.841
632.441	.0026	262.433	24.3203	315.024	11.2533	1.173	1.430	1.162	.00003713	• 04660	.847

TABLE I.- THERMODYNAMIC PROPERTIES OF  $CF_4$  AT CONSTANT ENTROPY - Continued

Т	v	p	H/RT <sub>o</sub>	A	$c_p/R$	γ	G	Z	$\mu_{\cdot}$	k	$N_{\mathbf{Pr}}$
				\$/	°=32.50						
	81.1639 60.5181	.001		117.390 121.835					.00000679		
132.460	45.5937	.003	9.5202	126.082	4.6937	1.271	1.271	1.000	.000000808	.00352	1.019
	34.6296 26.5022	.004 .005		130.154					.000003872		.940 .887
	20.4147	.007							.30030996		.851
	15.8166	.010	10.2554						.00001056		-824
192.460	9.6373		10.4542						.00001116	.00722	.805 .792
202.460	7.5721		10.8697						.00001232	.00870	·782
212.460	5.9724	.033	11.0863	155.143	6.0040	1.200	1.200	1.000	.00001289	.00944	.774
222.460	4.7275		11.3087						.00001345		•769
232,460 242,460	3.7543 2.9907		11.5369	161.459	6.3233 6.4812				.00001400		•765 •763
252.460	2.3889	•098		167.503	6.6379				.00001404	.01241	.762
262.460	1.9140	.12d		170.435	6.7931				.00001560	.01315	.761
272 • 400	1.5371			173.312	6.9468				.30001612		.761
282.460	1.2375		12.7629		7.0990				.00001663		.762
292.460 302.460	.9987		13.0246		7.2495 7.3983				.00001713		.763 .764
312.460	.0548		13.5639		7.5452				.00001103		.766
322.460	.5319		13.8413		7.6903				.30001861		.768
332.460	• 4330		14.1237		7.8335				.00001909		•770
342 • 460 352 • 450	.3532 .2887		14.4110		7.9745 8.1136				.00001956		•771 •773
362.460	.2365		14.9597		3.2505				.00002049		.775
372.400	.1941	1.785		199.625	8.3852				.00002095		.777
382 -460	.1596		15.6064		3.5178				.00002140		•779
392 • 460	.1315		15.9161		3.6481					.02286	.781
402.460 412.460	.1086 .0899	4.264	16.2297		8.7761				.00002230	.02362	.783 .785
422.460	.C745		16.8680	211.633	9.0255				.00002319		786
432.460	0623		17.1923		9.1469				.00002363		.788
442.460	• 051 o		17.5197		9.2661				.00002408		.789
452.460 462.460	.0361		17.8499 18.1826		9.3832 9.4983				.00002452		.791 .792
472.460	.0303	14.487	18.5177	223.675	9.6114			997	.00002542		.793
482.460	.0255			226.215	9.7226			. 997	.00002587		. 795
492.460	.0215		19.1939		9.8321				.30002633		• 796
502.460 512.460	•0183		19.5345		9.9398				.00002690	.03157	.797 .798
522.460	.0132	36.533	20.2200	237.590	10.0460				.03002727	.03332	.799
532.460	.0113		20.5648						.00002826	.03422	.300
542.460	.0097		20.9111							.03516	.801
552.460	.0084								.00002936	.03612	.903
562.460 572.460	.0073 .0064								.00002995	.03712	.804 .807
582.460	.0056									.03923	.809
592.450	.0049									.04035	.812
602,460	. 0043								.00003285	.04153	.816
612.460	.0038								.00003373	. 04 2 7 6	.319
622.460	.0034	214.801	23.8349	301.988					.00003469	.04404	.825 .831
642.400									.00003689		.838
649.366									.06903770		.843

TABLE I.- THERMODYNAMIC PROPERTIES OF CF<sub>4</sub> AT

CONSTANT ENTROPY - Continued

T	v	p	H/RT <sub>O</sub>	A	$c_p/R$	γ	G	$\mathbf{z}$	μ	k	$N_{\mathbf{Pr}}$
				S/F	R=32.75						
120.889	81.3353	• CO 1		121.153					.00000734		
130.889		•002		125.429					.00000798		
140.889	46.4125 35.4768	.003		129.528 133.471					.00000862 .00000924		•950 •894
	27.3015		10.0329						.00000986	.00562	855
170.889	21.1338		10.2248	140.954					.00001047	.00636	.828
180.889	16.4456	.010	10.4227	144.521	5.4914	1.223	1.222	1.000	.00001106	.00710	.808
	12.8579		10.6266						.00001165		•793
200.889	10.0960	.019	10.8364						.00001223		.783
210.889 220.889	7.9584 6.2959		11.0521						.00001280	.00933	•775 •770
230.889	4.9973		11.5010						.00001330	.01081	.766
240.889	3.9789		11.7341						.00001446	.01155	.763
250.889	3.1767	.074	11.9729		6.6122				.00001499	.01229	.762
260.889	2.5439	• 096	12.2174		6.7675				.00001552		.761
270.889	2.0423			172.883	6.9213				.00001604		.761
280.889 290.889	1.6435		12.7230	178.504	7.0736 7.2241				.00001655	.01452 .01526	.762 .763
300.889	1.0719		13.2504		7.3730					.01600	.764
310.889	.8685		13.5220		7.5200				.00001804		.766
320.889	.7052		13.7988		7.6650				.00001853		.767
330.889	.5738		14.0807		7.8081				.00001901		.769
340.889	.4679		14.3676		7.9492					.01898	• 771
350.889 360.889	.3823 .3129	.855 1.073	14.6593		8.0881 8.2247				.00001995		.773 .775
370.889	.2567		15.2568		8.3592				.00002041		777
380.889	2110		15.5622	201.747	8.4913				.00002132		779
390.889	.1737		15.8720	204.169	8.6211				.00002177	.02272	.780
400.889	.1433	2.601	16.1859	206.569	8.7486	1.132	1.130	• 998	.00002222		.782
410.889	.1185	3.223	16.5037		8.8736				.00002266	.02423	.784
420.889	.0982		16.8253		8,9962				.00002310	.02499	.785
430.889 440.889	.0815 .0679		17.1504 17.4789	216.034	9.1164			•997	.00002354	.02576	.787 .788
450.889	.0566		17.8104		9.3496			.997	.00002441		.790
460.889	.0473		18.1448	220.776	9.4627				.00002485	.02808	.791
470.889	.0397	11.040	18.4818	223.182	9.5735	1.126	1.123	•997	.00002528	.02887	•792
480.889	.0333		18.8212		9.6820				.00002573	.02967	• 793
490.889	•0281		19.1627		9.7884				.00002617	.03048	•794 •795
500.889 510.889	.0237 .0201		19.5061 19.8512		9.8927 9.9951				.00002662	.03130	• 796
520.889	.0171	28.458	20.1977	236.258	10.0954				.00002754	.03298	.796
530.889	.0146		20.5456		10.1939				.00002801	.03385	.797
540.889	.0125								.00002850		.797
550.889	.0107	48.350		245.963					.00002900		.798
560.889	.0093									.03659	•799
570 .889	.0080	67.638							.00003010	.03756	.800
580.889 590.889	.0070 .0061								.00003070	.03857	.801 .803
600.889	.0054								.00003204		.805
610.889	.0047								.00003279	.04182	.808
620.889	.0042	147.736	23.7798	282.669	10.9858	1.153	1.266	1.076	.00003360	.04299	-811
630.889	.0038			290.533					.00003449	.04423	.816
640.889	.0034								.00003546	• 04552	•822
650.889 660.889	.0030 .0027								.00003651	.04689	.828 .835
665.981									.00003183		.838

T	V	р	H/RT <sub>O</sub>	A	$c_{\mathbf{p}}/\mathbf{R}$	γ	G	$\mathbf{z}$	μ	k	$N_{\mathbf{Pr}}$
				\$/1	R=33.00						
129.678	81.2760	.001	9.4727	124.923	4.6471	1.274	1-274	1.000	.00000791	-00331	1.048
139.678		•002		129.043					.00000854		.959
149.678	47-0505	.003		133.004					.00000917		•900
159.678	36.1778	•004	10.0102	136.824					.00000979		.859
169.678			10.2014						.00001039		.831
179.678	21.7643		10.3986						.00001099 .00001158		.810 .795
189.678 199.678	17.0069		10.6017						.00001216		•784
209.678	10.5162		11.0258						.00001273		.776
219.678	8.3158		11.2467						.00001329	.00998	.770
229.678	6.5980		11.4734	160.617					.00001385	.01072	.766
239.678	5.2513		11.7058	163.692						.01146	.763
249.678	4.1909		11.9440	166.704					.00001493		.762
259.678	3.3547		12.1879							.01294	.761
269.678	2.6932		12.4373						.00001597		.761
279.678	2.1662	•120	12.6923		7.0540				.00001649		.762 .763
289.678 299.678	1.7468		12.9528	178.189 180.936	7.2046 7.3535					.01591	.764
309.678	1.1436		13.4898		7.5005				.00001798		.765
319.678	•9283		13.7661		7.6456				.00001847		.767
329.678	.7551		14.0476		7.7886			.999	.00001895	.01814	.769
339.678	.6154		14.3341		7.9296			999		.01888	.771
349.678	.5026		14.6256		8.0684				.00001989		•772
359.678	•4113	. 814	14.9218		8.2049				.00002035		•774
369.678 379.678	.3372		15.2227 15.5281		8.3392 8.4710				.00002081		•776 •778
389.678	•2770 •2280		15.8380		8.6005				.00002120		.780
399.678	.1880		16.1520		8.7274					.02337	.782
409.678	.1554		16.4702		8.8518				.00002259		.783
419.678	-1287		16.7922		8.9737	1.129	1.126			.02488	.785
429.678	.1068		17.1180		9.0930					.02563	.786
439.678	.0888		17.4473		9.2098				.00002389		.788
449.678	•0740		17.7798		9.3239					.02716	789
459.678 469.678	.0618		18.1155 18.4541		9.4355 9.5445				.00002476 .00002519	.02794	.790 .791
479.678	•0434		18.7952		9.6510				.00002513	.02950	.792
489.678	.0365		19.1388		9.7550					.03029	.793
499.678	.0308		19.4845		9.8566				.00002649		.793
509.678	•0260		19.8321							.03191	•794
519.678	.0221								.00002737		•794
529 - 678	.0188								.00002783		•795 •795
539.678 549.678	.0160 .0137								.00002829 .00002876	.03442	• 795
559.678	.0118								.00002924		.795
569.678	.0102								.00002975	.03711	.795
579.678	•0088								.00003028		.796
589.678	.0077								.00003085		.797
599.678	•0067									• 04 005	.797
609.678	.0059									•04109	•799
619.678	•0052								.00003280		.801
629.678										.04331	.804
639.678 649.678	•0041								.00003437 .00003526	.04449	.808
659,678	•0037								.00003328		.819
669.678									.00003728		.825
679.678									.00003842		.831
683.167									.00003884		.834

TABLE I.- THERMODYNAMIC PROPERTIES OF  $CF_4$  AT CONSTANT ENTROPY — Continued

T	v	p	H/RT <sub>O</sub>	A	$c_p/R$	. <b>Y</b>	G	Z	μ	k	$N_{Pr}$
				\$ / 8	l=33 <b>.</b> 25						
				37	(-33.2)						
138.684	81.2882	•002	9.6284	128.642	4.7961	1.263	1.263	1.000	.00000848	-00398	•966
148.684		.002		132.619					.00000911		905
	47.6769	.003		136.452					.00000973	• 00546	.863
	36.8587		10.1822						.00001033	• 00620	.833
	28.6501		10.3788						.00001093		.812
	22.3772		10.5814						.00001152		• 796
	17.5543 13.8257		10.7899						.00001210	.00842	•785 •776
	10.9290		11.2246						.00001288	.00910	.771
228.684	8.6684		11.4508						.00001379	.01064	.766
238.684	6.8971		11.6827						.00001434	.01138	.764
248.684	5.5025	.042	11.9203	166.416	6.5762	1.179	1.179	1.000	.00001487	.01213	.762
258.684	4,4032		12.1637							.01287	•761
268.684	3.5339		12.4126						.00001592		.761
278.684	2.8418		12.6671						.00001644	.01435	.762
288.684	2.2910 1.8512		12.9271 13.1925		7.3375				.00001694	.01583	•762 •764
308.684	1.4991		13.4633		7.4846				.00001793	.01657	.765
318.684	1.2166		13.7393		7.6297				.00001842	.01732	.767
328.684	.9893	.310	14.0204	188.686	7.7727				.00001890	.01806	.768
338.684	.8061		14.3067		7.9137	1.145	1.144	• 999	.00001937	.01880	.770
348.684	.6582		14.5978		8.0524				.00001984		.772
358.684	.5384		14.8939		8.1889					. 02 029	•774
368 -684	.4413		15.1946 15.5000		8.3230				.00002076		•776
378.684 388.684	.3624 .2982		15.8098	201.298	8.4546 8.5838				.00002121	.02178	•778 •780
398.684	. 2458		16.1240		8.7104				.00002210		.781
408.684	.2030		16.4423		8.8344				.00002254		.783
418.684	•1680		16.7647		8.9558				.00002297		.784
428.684	.1393		17.0909		9.0744				.00002340	.02554	.786
438.684	-1157	3.527			9.1904					.02629	•787
448.684	.0964		17.7542		9.3036				.00002426		.788
458.684 468.684	.0804 .0672		18.0908 18.4306		9.4140 9.5216				.00002468	.02782	•789 •790
478.684	•0563		18.7731		9.6265					.02936	•791
488.684	.0473		19.1183		9.7287				.00002596		.791
498.684	.0398		19.4659		9.8282				.00002638		•792
508.684	.0336	14.098	19.8156	232.122	9.9249				.00002681		.792
518.684	.0285								.00002724		•793
528 • 584	.0242		20.5205						.00002768	.03335	•793
538.684 548.684	.0206								-00002812	.03418	• 793
558.684	.0176								.00002857	03502	•793 •793
568.684	.0130								.00002950		.792
578.684	.0112								.00002998		.792
588.684	.0097	57.826	22.6684	256.375	10.6072	1.130	1.158	1.020	.00003049	.03859	.792
598 • 684	•0084								.00003103		•792
608.684	.0074								.00003160	.04052	.792
618.684	.0065								.00003220	.04153	.793
628.684	•0057 •0050								.00003285	.04259	•795 •798
648.684									.00003333	.04482	.801
658.684									.00003513	.04601	.806
668.684	.0036								.00003602	.04725	.810
678.684	•0032	222.627	26.1380	313.518	11.3334	1.154	1.348	1.137	-00003699	.04855	.816
688.684	.0029								.00003804		.822
698.684	•0027								.00003918		.828
700.682	• 0026	299.832	21.1726	351.943	11.5018	1.159	1.440	1.198	.00003942	.05166	.829

T	v	p	H/RT <sub>o</sub>	A	$c_p/R$	γ	G	Z	μ	k	$Np_{\mathbf{r}}$
				S/1	R=33.50						
				_,							
147.877	81.3987	•002	9.7924	132.305	4.9480	1.253	1.253	1.000	.00000906	.00466	.909
	62.5386	.002		136.150					.00000968		.866
167.877			10.1666		5.2774				.00001029	.00614	.835 .813
177.877			10.3627						.00001089	.00762	.797
	22.9852		10.7729						.00001206		.786
	18.0974		10.9869						.00001263		.777
217.877		.014	11.2067						.00001319		•771
227.877			11.4324							-01058	.767 .764
237.877	9.0206 7.1947		11.6639	166.182					.00001429		.762
257.877	5.7559		12.1441	169.146						.01281	.761
267.877	4.6183	.054	12.3926		6.8726	1.170	1.170	1.000	.00001588	.01355	.761
277.877	3.7134		12.6467						.00001639	.01429	.761
287.877	2.9931		12.9063							.01503	.762
297.877 307.877	2.4180 1.9577		13.1714		7.4717				.00001740	.01577	.763 .765
317.877	1.5883		13.7175		7.6168				.00001133	.01725	.766
327.877	1.2914		13.9983		7.7599					.01800	.768
337.877	1.0520		14.2843		7.9008					.01874	•770
347.877	.8587		14.5753		8.0395				.00001980		•772
357.877 367.877	.7023 .5755		14.8711		8.1759 8.3099				.00002026	.02023	•774 •776
377.877	•4724		15.4770		8.4415				.00002117		.777
387.877	.3886		15.7868						.00002162		.779
397.877	.3202	1.157	16.1011	205.576	8.6968				.00002206		.781
407.877	•2644	1.437	16.4195		8.8205					.02396	.782
417.877 427.977	.2187 .1813	1.779 2.198	16.7422		8.9415 9.0597	1.128			.00002293	.02471	.784 .785
427.877	.1505		17.3991		9.1750				.00002378	.02621	.787
447.877	.1252		17.7330						.00002421		.788
457.877	.1044		18.0704		9.3970				.00002463		.789
467.877	.0872		18.4110		9.5037					. 02849	-789
477.877 487.877	.0730		18.7547 19.1011		9.6073 9.7081				.00002547 .00002588	.02925	.790 .791
497.877	.0515		19.4502		9.8059				.00002588	.03080	.791
507.877	.0434		19.8016		9.9007					.C3159	.791
517.877	.0367		20.1551						.00002714	.03238	.791
527.877	.0311		20.5106						.00002757		.791
537.877 547.877	.0264 .0225								.00002799	.03481	.791 .791
557.877	.0193	27.170							.00002887	.03564	.791
567.877	.0165								.00002931		.790
577.877	.0142								.00002977	.03736	.789
587.877	.0123	45.367			10.5573					.03824	•789
597.877 607.877	.0106	53.485	23.40375						.00003072	.04008	.788 .787
617.877	•0092									.04103	.787
627.877	.0071									.04202	.788
637.877	•0062	99.971							.00003294	.04304	.790
647.877	.0055		24.8900						.00003359	.04409	.792
657.877 667.877	.0049 .0044	134.396	25.2764		11.0897				.00003430	.04519	.795 .799
677.877	•0039								.00003588	.04753	.803
687.877	.0035								.00003678	.04877	.807
697.877		235.322	26.9409	320.543	11.4114	1.151	1.357	1.149	.00003774	.05008	.812
707.877									.00003879	.05145	.818
717.877 718.482									.00003992	.05288	.824 .825
	\$3020	24,4200		2.5.056		1-1/0					

T	v	<b>, p</b>	H/RT <sub>o</sub>	A	c <sub>p</sub> /R	γ	G	${f z}$	$\mu$	k	$N_{\mathbf{Pr}}$
				S/F	₹=33.75						
157.401		-002		135.571					.00000965		.867
167.401 177.401		• CO2	10.1575						.00001026		.836
187.401			10.5552						.00001086	.00685	.814 .798
	29.8582		10.7629						.00001203		.786
	23.5045		10.9766		5.9203	1.203	1.203	1.000	.00001260	.00907	.777
	18.5713		11.1962						.00001317		.771
227.401 237.401	14.7236		11.4217 11.6529							• 01 055	•767
247.401	9.3383		11.8899						.00001427	.01129	.764 .762
257.401	7.4696		12.1325							.01277	.761
267.401	5.9919		12.3809							.01351	.761
277.401	4.81.89		12.6348		7.0172	1.166	1.166	1.000	.00001637	.01425	.761
287.401 297.401	3.8819		12.8942							.01499	•762
307.401	3.1369 2.5389		13.1590 13.4292						.00001738		.763
317.401	2.0597		13.7047		7.6091	1.152	1.151	1.000	.00001787	. 01722	•765 •766
327.401	1.6743		13.9855		7.7521	1.148	1.148	1.000		.01796	.768
337.401	1.3638		14.2713		7.8930	1.145	1.145	1.000	.00001931	.01870	.770
347.401	1.1131		14.5621		8.0316				.00001978	.01944	•772
357.401 367.401	.9102 .7457		14.8579 15.1585		8.1679 8.3018				.00002024		•774
377.401	.6121		15.4638		8.4332				.00002069	.02093	•775 •777
387.401	.5033		15.7737		8.5620					.02242	.779
397.401	.4147		16.0880		8.6882			.999		.02316	.781
407.401	•3423		16.4067		8.8116				.00002247		•782
417.401	.2830 .2345		16.7295 17.0564		8.9323				.00002290	.02466	•784
437.401	.1947		17.3871		9.0500 9.1649				.00002333	.02541 .02616	.785 .786
447.401	1619		17.7216		9.2767					.02691	.787
457.401	.1349		18.0596		9.3856	1.122	1.121		.00002459		.788
467.401	-1126		18.4010		9.4914				.00002501		.789
477.401 487.401	•0942 •0790		18.7455 19.0930		9.5941					.02918	.790
497.401	.0664		19.4433		9.6936 9.7901					•02995 •03072	•790 •790
507.401	.0559		19.7961						.00002625	.03072	•790
517.401	.0472		20.1512		9.9736				.00002707	.03227	•790
527.401	.0399		20.5085		10.0607	1.118	1.119	1.001	.00002748	.03306	.790
537.401	.0339	14.813	20.8676	238.665	10.1446	1.118	1.120	1.002	.00002790	.03385	•790
547.401 557.401	•0288 •0246	21 230	21.2284	241.193	10.2255	1.118	1.122	1.003		.03465	•789
567.401	.0210	25.308	21.9541	246.547	10.3779	1.119	1.127	1.004	.00002874	.03547	•789 •788
577.401	.0180	30.080	22.3188	249.422	10.4496	1.120	1.131	1.008		.03713	.787
587.401	.0155	35.646	22.6845	252.468	10.5182	1.121	1.136	1.011	.00003005	.03798	.786
597.401	.0134									.03885	.785
607.401	.0116	49.599	23.4188	259.209	10.6461	1.124	1.149	1.019	.00003097	.03974	.784
627.401	.0089	68-068	24-1527	267.031	10.7852	1.128	1 168	1.024		.04065 .04159	•783 •783
637.401	.0078	79.453	24.5259	271.470	10.8636	1.130	1.180	1.037		• 04255	•784
647.401	.0068	92.491	24.9025	276.335	10.9425	1.132	1.194	1.046	.00003308	.04354	.785
657.401	.0060	107.345	25.2834	281.682	11.0219	1.134	1.210	1.056	.00003369	.04457	.787
667.401 677.401	.0053	124.257	25.6700	287.571	11.1013	1.136	1.228	1.068	.00003434	.04563	.789
687.401	.0048		26.4674	301.239	11.2502	1.142	1.272	1.000	.00003505 .00003581	.04673	•792
697.401		189.719	26.8835	309.163	11.3370	1.144	1.300	1.116	.00003581	.04788	• 796 • 800
707.401	.0034	217.386	27.3149	317,930	11.4133	1.147	1.331	1.136	.00003753	• 05032	.804
717.401	.0031	248.523	27.7659	327.641	11.4874	1.149	1.365	1.160	.00003850	.05163	.809
727-401	•0028	283.517	28.2413	338.419	11.5587	1.151	1.404	1.187	.00003954	.05300	.815
736.601	•0026	319.492	28.7U51	349.405	11.6212	1.153	1.445	1.214	.00004057	.05432	.820

T	<b>v</b>	p	H/RT <sub>o</sub>	A	$c_p/R$	Y	G	z	μ	k	$N_{\mathbf{Pr}}$
				\$/1	R=34.00						
167 •0 71	<b>E1.344</b> 6	•002	10.1511	139.574					.00001024		.837
177.071			10.3468						.00001084		.815
187.071	49.3048		10.5484						.00001143		•798 •786
197.071	38.6505 30.4220		10.9696						.00001258		.778
	24.0339		11.1890						.00001315	.00978	.771
227.071	19.0523		11.4142						.00001370	. 01 052	.767
237.071	15.1511		11.6453						.00001425	.01126	•764 •762
247.071 257.071	12.0810 9.6524		12.1246						.00001532		.761
267.071	7.7526		12.3727						.00001584	.01349	.761
277.071	6.2326		12.6265							.01423	.761
287.071	5.0208		12.8857						.00001686	.01497	•762 •763
297 •071 307 • 071	4.0565 3.2829		13.1505 13.4206						.00001735	.01645	.765
317.071	2.6629		13.6960						.00001834	.01719	.766
327.071	2.1645	.141	13.9766	188.311					.00001882		.768
337.071	1.7629	.178	14.2623						.00001929		•770
347.071 357.071	1.4386	• 225 • 283	14.5531 14.8489		8.1623				.00001976	.02016	.772 .773
367.071	.9635		15.1494		8.2961				.00002068		.775
377.071	.7908	.444	15.4547	200.976	8.4274	1.135	1.135	.999	.00002113	.02165	.777
387.071	•6502		15.7647		8.5560					.02239	.779
397.071 407.071	•5356 •4420		16.0791	208.216	8.6820				.00002201	.02313	.781 .782
417.071	.3654		16.7209		8.9256				.00002288		.784
427.071	.3027		17.0481		9.0430			.999	.00002331	.02537	.785
437.071	. 2512		17.3792		9.1574					.02612	•786
447.071 457.071	.2088 .1739	2.448	17.7140 18.0526		9.2688 9.3771				.00002415	.02762	•787 •788
467.071	.1452		18.3945		9.4823				.00002498	.02837	.789
477.071	.1214		18.7398		9.5842					.02913	.789
487.071 497.071	.1017		19.0881		9.6829 9.7782				.00002580	.02989	.790 .790
507.071	.0719	€.576	19.7933		9.8703				.00002661	.03142	.790
517.071	.0606		20.1497		9.9591				.00002702		.790
527.071	.0512		20.5084						.00002743	.03297	.789
537.071	•0434								.00002783		.789 .788
547.071 557.071	.0369 .0314								.00002824 .00002865	.03533	.788
567.071	.0268								.00002907		.787
577.071	.0230								.00002949	.03696	.786
587.071	.0197	27.584	22.6963						.00002992	.03779	.784 .783
597.071 607.071	.0170								.00003039	.03949	781
617.071	0128								.00003123		.780
627.071	.0111								.00003170	.04125	.780
637.071 647.071	.0097		24.5457						.00003219	.04217	.780 .780
657.071	•0075	85.509		276.985					.00003270	.04408	.781
667.071	.0066								.00003381		.782
677.071	•0058	114.812	26.0708	287.539	11.1154	1.133	1.216	1.063	.00003442	.04610	•784
687.071 697.071	•0052								.00003508	04717	.786 .789
707.071	•0046 •0042								.00003579	.04827 .04942	•789 •792
717.071									.00003738	.05062	.796
727.071	•0034	229.370	28.1432	324.718	11.4892	1.145	1.339	1.147	.00003827		. 801
737.071 747.071									.00003923	.05318	.806 .811
755.034									.00004027		.816

TABLE I.- THERMODYNAMIC PROPERTIES OF CF<sub>4</sub> AT

CONSTANT ENTROPY - Continued

T	v	p	H/RT <sub>O</sub>	A	$c_p/R$	γ	G	Z	$\mu$	k	$N_{Pr}$
				\$/1	₹=34•25						
176.940	81.3928	.002	10.3442	143.139	5.4255	1.226	1.226	1.000	.00001083	- 00681	.815
186.940	63,5319		10.5458						.00001142		.799
	49.7930		10.7533		5.7510	1.210	1.210	1.000	.00001200	.00829	.786
206.940			10.9668						.00001258		-778
216.940 226.940			11.1861						.00001314		•771
236.940	15.5149		11.6423							.01125	•767 •764
246.940	15.5598		11.8790							.01200	.762
256 •9 40	12.4442	.019	12.1215	168.885					.00001531		.761
266.940	9.9854		12.3696		6.8570	1.171	1.171	1.000	.00001583	.01348	.761
276.940	8.0264		12.6233						.00001635		.761
286.940 296.940	6.4659 5.2235		12.8825						.00001685		•762
306.940	4.2271		13.4172						.00001735	.01570	•763 •765
316.940	3.4287		13.6926						.000011833		•766
325.940	2.7868		13.9732						.00001881		.768
336.940	2.2696		14.2590							.01866	-770
346.940	1.8520		14.5498							.01941	•772
356.940	1.5142		14.8456							.02015	-773
366.940 376.940	1.2403	. 276	15.1462		8 4244	1 125	1 125	1.000	.00002067	• 02 089	•775
386.940	.8368		15.7616		8.5530	1.133	1.132			•02103	•777 •779
396.940	.6892		16.0762		8.6788				.00002201		780
406.940	.5687		16.3951		8.8018					.02386	•782
416.940	.4701		16.7184		8.9219				.00002287		•783
426.940	.3893		17.0458		9.0390			.999		.02535	.785
436.940 446.940	.3230 .2685		17.3772 17.7124		9.1531 9.2641				.00002372 .00002414		•786
456 • 940	.2236		18.0514		9.3719					.02685 .02760	•787 •788
466.940	.1865		18.3938		9.4765				.00002496		.788
476.940	.1559		18.7397	224.365	9.5778	1.119	1.118		.00002537	.02910	•789
486.940	.1306		19.0887	226.626	9.6757	1.118	1.117	.999	.00002578	.02985	• 789
496.940 506.940	.1096		19.4408		9.7702	1.117	1.116	1.000	.00002618	.03061	•789
516.940	.0922 .0777		19.7956 20.1531							.03137	•789
526.940	.0656	7.491	20.5130	235.713	10.0330	1.115	1.116	1.000		.03214	•789 •789
536.940	.0555	9.022	20.8751	238.029	10.1136	1.115	1.116	1.001		.03368	.788
546.940	.0471	1C.E38	21.2391	240.380	10.1907	1.115	1.117	1.002	.00002819	.03446	•787
556.940	.0401	12.986	21.6050	242.777	10.2642	1.115	1.118	1.002	.00002859		.787
566.940 576.940	.0342	15.518	21.9724	245.235	10.3342	1.115	1.119	1.003		.03603	•785
586.940	.0251	21.983	22.3412	250.308	10.4636	1 116	1 124	1.005	.00002940	.03764	• 784 • 783
596.940	.0215	26.055	23.0820	253.143	10.5227	1.116	1.127	1.008		.03846	•781
606.940	.0186		23.4538	256.026	10.5784	1.117	1.131	1.011		.03930	.779
616.940	.0161	36.223	23.8210	259.063	10.6316	1.118	1.136	1.014	.00003108	.04014	•778
626.940	.0140	42.569	24.1946	262 • 276	10.7019	1.119	1.141	1.017	.00003151	.04100	•777
636.940 646.940	.0122	49.893	24.5698	265.713	10.7726	1.120	1.148	1.022	.00003196	• 04188	•777
656.940	.0106	68.017	25.3256	273.422	10 0152	1 122	1.156	1.027	.00003243	.04278	•776
666.940	.0082	79.091	25.7071	277.774	10.9872	1.125	1.177	1.040		.04464	•777 •777
676.940	.0072	91.726	26.0919	282.522	11.0596	1.127	1.190	1.049		.04562	778
686.940	.0064	106.104	26.4806	287.714	11.1323	1.129	1.205	1.059	.00003454	.04662	•779
696.940	.0057	122.422	26.8746	293.403	11.2051	1.131	1.222	1.070		.04765	•781
706.940		140.894	27.2752	299.646	11.2779	1.133	1.241	1.083	.00003581	.04872	• 783
726.940	.0045	185, 264	28-1040	314,035	11-4220	1.120	1.200	1.116		•04983	•786
736.940	.0037	211.699	28.5372	322.320	11.4927	1.140	1.315	1.135		.05098	•789 •793
746.940	.0033	241.370	28.9872	331.440	11.5619	1.143	1.346	1.156		.05343	•797
756.940	.0030	274.622	29.4581	341.495	11.6290	1.145	1.381	1.181	•00003996	.05473	.802
766.940	•0028	311.839	29.9545	352.604	11.6934	1.147	1.420	1.209	.00004099	.05610	•807
773.794	•0026	334.838	30.3124	50U+899	11.7358	1.148	1.449	1.230	.00004174	•05707	•811

T	v	p	H/RT <sub>O</sub>	A	$c_p/R$	γ	G	Z	μ	k	Npr
				s/	R=34.50			٠			
	81.3384 63.7682		10.5483						.00001143		.798 .786
207.061	50.1834		10.9694						.00001258	.00904	.778
217.061			11.1889						.00001315	.00978	.771
227.061 237.061	31.4273 24.9920		11.4141						.00001370	.01052 .01126	.767 .764
247.061	19.9276		11.8820	165.952					.00001479	.01200	.762
257.061		•015	12.1245	168.524	6.7047	1.175	1.175	1.000	.00001532	.01274	.761
	12.7880		12.3727							.01349	.761
277.061 287.061	8.2814		12.6265						.00001635		.761 .762
297.061	6.6905		13.1506							.01571	.763
307.061	5-4143		13.4208						.00001785		.765
317.061	4.3918		13.6962							.01719	.766
327.061	3.5696		13,9769	188.325					.00001882		•768 •770
337.061 347.061	2.9072		14.2628						.00001929		.772
357.061	1.9394		14.8497		8.1605	1.140	1.140	1.000	.00002022	.02015	.773
367.061	1.5886		15.1504						.00002067	.02090	• 775
377.061 387.061	1.3036		15.4560	201.000					.00002112	.02164	•777 •779
397.061	.8827		16.0810							.02312	780
407.061	.7283		16.4002		8.8018	1.129	1.128	1.000	.00002244	.02387	.782
417.061	.6020		16.7237		8.9216				.00002287	.02461	.783
427.061 437.061	.4985 .4135		17.0513 17.3830		9.0385 9.1522				.00002330	.02536	• 785 • 786
447.061	.3437		17.7187		9.2629				.00002414	.02685	787
457.061	.2861	1.488	18.0580	219.852	9.3702	1.121	1120	.999	.00002455	•02759	¥788
467.061	-2387		18.4010		9.4743			.999	.00002496	.02834	.788
477.061 487.061	.1995 .1670		18.7474 19.0970		9.5750			.999	.00002537	.02909 .02984	•789 •789
497.061	.1401		19.4498		9.7660				.00002517	.03060	.789
507.061	.1178	4.C13	19.8054	231.115	948562	1.115	1.115	1.000	.00002657	.03135	•789
517.061	.0992		20.1638						.00002697	.03211	.789
527.061 537.061	.0838		20.5247		10.0258				.00002736	.03288 .03364	.788 .788
547.061	.0601		21.2532						.00002815	.03441	.787
557.061	.0510	10.194	21.6205	242.509	10.2527	1.113	1.116	1.002	.00002855	.03519	.786
567.061	.0435								.00002894		•785
577.061 587.061	.0371								.00002934		.783 .782
597.061	.0273	20.534	23.1043	252.382	10.5027	1.114	1.122		.00003014	.03835	.780
607.061	.0235				10.5557					.03917	•778
617.061	.0203 .0176								.00003096	.03999	•776 •775
627.061 637.061	.0153	39.546	24.5994	263.904	10.7408	1.117	1.138		.00003138		.774
647.061	.0133				10.8085					.04254	.774
657.061	.0116								.00003268	.04342	•773
667.061 677.061	.0102 .0089				11.0136				.00003315	.04432 .04525	•773 •773
. 687.061	•0079				11.0827				.00003304	.04620	.774
697.061	.0070	98.152	26.9013	288.098	11.1521	1.126	1.195	1.055	.00003469	.04717	.775
707.061									.00003527	.04818	•776
717.061 727.061									.00003588 .00003654	.04921	•778 •780
737.061									.00003725	.05140	.783
747.061	•0040	195.524	28.9484	320.415	11.4984	1.136	1.295	1.124	.00003801	.05255	.786
757.061	.0036								.00003883	.05375	•789
767.061 777.061	.0033				11.6316				.00003972	.05500	•794 •798
787.061									.00004170		-803
792.883									.00004233		.806

TABLE I.- THERMODYNAMIC PROPERTIES OF  $CF_4$  AT CONSTANT ENTROPY — Continued

T	v	p	H/RTo	A	$c_p/R$	γ	G	$\mathbf{z}$	μ	k	$N_{\mathbf{Pr}}$		
S/R=34.75													
	£1.3590 64.0484		10.7616						.00001203		.786 .777		
217.328	50.5966	.004	11.1948	156.745	6.0790	1.197	1.197	1.000	.00001316	.00980	.771		
227.328	40.1118		11.4202						.00001372	.01054	•767 •764		
247.328	25.4384	.009	11.8885	166.C34	6.5532	1.180	1.180	1.000	.00001480	.01202	.762		
257.328 267.328	20.3469	.012	12.1312	169.005 171.919					.00001533	.01276	.761		
277.328	13.1254	.020	12.6334						.00001585	.01350 .01425	.761 .761		
287.328	10.5732		12.8929		7.1654	1.162	1.162	1.000	.00001687	.01499	.762		
297.328 307.328	8.5431 6.9140		13.1579		7.3142 7.4611				.00001737	.01573	.763		
317.328	5.6084		13.7038							.01721	.766		
327.328	4.5587	.C67	13.9847		7.7487					.01795	.768		
337.328 347.328	3.7128 3.0297		14.2708	191.003					.00001930	.01869	•770 •772		
357.328	2.4770	.134	14.8580	196.103	8.1635	1.140	1.139	1.000	.00002023	.02017	•773		
367.328 377.328	2.0290 1.6650		15.1590						.00002069	•02091	•775 •777		
387.328	1.3688		15.7752		8.5559	1.133	1.132	1.000	.00002114	.02240	.779		
397.328	1.1274		16.0902		8.6813	1.131	1.130	1.000	.00002202	.02314	.780		
407.328	.9302 .7688		16.4096							.02388	.782 .783		
427.328	.6366	•626	17.0613	213.018	9.0400	1.125	1.124	1.000	.00002331	.02537	.785		
437.328 447.328	.5281		17.3934 17.7294						.00002373	.02611	.786		
457.328	.4388 .3653		18.0691						.00002414	.02761	•787 •787		
467.328	.3047	1.429	18.4125	222.179	9 • 4743	1.119	1.119	1.000	.00002496	.02835	.788		
477,328 487,328	.2546 .2131		18.7594						.00002537	.02910	•789 •789		
497.328	.1788		19.4630						.00002517	.03060	.789		
507.328	.1502		19.8193		9.8537	1.115	1.115	1.000	.00002657	.03135	.789		
517.328 527.328	.1265 .1067		20.1784						.00002696	.03211	.788 .788		
537.328	• 0902	5.554	20.9043	237.818	10.0998	1.113	1.114	1.001	.00002774	.03363	.787		
547.328 557.328	.0765								.00002813	.03439	•786		
567.328	.0649 .0553	9.591	22.0092	244.648	10.2446	1.112	1.114	1.002	.00002852	.03593	.785 .784		
577.328	-0471	11.449	22.3810	246.991	10.3741	1.112	1.115	1.003	.00002930	.03671	.782		
587.328 597.328	.0403 .0346	13.633	22.7542	249.385	10.4328	1.112	1.117	1.004	.00002969	.03749	.781 .779		
607.328	.0297	15.179	23.5040	254.379	10.5383	1.113	1.121	1.006	.00003048	.03908	.776		
617.328	•0257	22.615	23.8747	257.002	10.5870	1.113	1.123	1.008	.00003088	.03988	.774		
627.328 637.328	.0222 .0192								.00003128	.04153	•773 •773		
647.328	.0167	36.733							.00003211		.772		
657.328	.0145	42.969		268.750	10.8456	1.116	1.140	1.020	.00003252	.04322	.771		
667.328 677.328	.0127 .0111	58.365	26.1600	275.798	10.9106	1.117	1.155	1.024	.00003296	.04409 .04497	.770 .770		
687.328	.0098	67.795	26.5468	279.736	11.0416	1.120	1.164	1.035	.00003387	.04588	•770		
697.328 707.328	.0086 .0076									.04681 .04776	.770 .771		
717.328	•0068								.00003541	.04874	.771		
727.328	•0060	120.311	28.1257	299.143	11.3068	1.126	1.216	1.071	.00003598	.04974	.773		
737.328 747.328	•0054 •0048	138.035	28.5326	311.692	11.4398	1.130	1.254	1.098	.00003660	.05078	•774 •776		
757.328	.0044	180.454	29.3706	318.856	11.5057	1.133	1.276	1.114	.00003796	.05297	•779		
767.328	.0039	205.638	29.8059	326.694	11.5709	1.135	1.301	1.132	.00003872	.05412	.782		
777.328 787.328	.0036	265.354	30.7232	344.677	11.6976	1.137	1.360	1.175	.00003954	.05532 .05657	.786 .790		
797.328	.0030	300.531	31.2125	354.997	11.7583	1.141	1.394	1.200	.00004137	.05787	• 794		
807.328 812.321									.00004238		.799 .801		
014.321	•0020	,500 • 70 4	J1#7716	J1 C # 773	1110444	10143	** 473		.00007272	• 07772	• 001		

T	v	p	H/RT <sub>O</sub>	, <b>A</b>	$c_{\mathbf{p}}/\mathbf{R}$	γ	G	Z	μ	k	$N_{\mathbf{Pr}}$
				\$/1	R=35.00						
207.748			10.9844 11.2042						.00001262	.00909	.777 .771
217.748 227.748	64.3415 51.0156		11.4299						.00001318		.767
237.748	40.5776	•005	11.6614	163.134	6.4029	1.185	1.185	1.000	.00001428	.01131	• 764
247.748 257.748			11.8986 12.1415	166.162					.00001482	.01205	.762 .761
267.748			12.3901		6.8688	1.170	1.170	1.000	.00001587		.761
277.748	16.7026		12.6443	174.903					.00001639	.01428	.761
287.748 297.748	13.4543		12.9040						.00001689		•762 •763
307.748	8.8006	•033	13.4398	183.197	7.4670	1.155	1.154	1.000	.00001788	.01650	.765
317.748	7.1393		13.7157						.00001837	.01724	•766 •768
327.748 337.748	5.8035 4.7269		14.2831							.01872	.770
347.748	3.8576	•C84	14.5745	193.682	8.0330	1.142	1.142	1.000	.00001979	.01946	•772
357.748 367.748	3.1540 2.5836		14.8708 15.1721	196.215					.00002025	.02020	•773 •775
377.748	2.1203		15.4781						.00002115	.C2169	.777
387.748	1.7432		15.7888						.00002160	.02243	•779
397.748 407.748	1.4357		16.1041		•				.00002247		.780 .782
417.748	.9792		16.7479		8.9274	1.126	1.126	1.000	.00002290	. 02465	.783
427.748 437.748	.8108 .6726		17.0762 17.4086						.00002332		.785 .786
447.748	.5589		17.7449							.02688	.787
457.748	.4653			220.012					.00002457	.02763	.787
467.748 477.748	.3880 .3242		18.4289						.00002498	.02838	•788 •788
487.748	.2714		19.1269		9.6723	1.116	1.116	1.000	.00002578	.02987	.789
497.748	.2276		19.4808						.00002618	.03062	789
507.748 517.748	.1912		19.8378	231.184					.00002657	.03212	•789°
527.748	.1358				10.0199	1.113	1.113	1.000	.00002735	.03287	.788
537.748 547.748	.1148								.00002774	.03363	•787 •786
557.748	.0825									.03515	.785
567.748	.0702								.00002889		• 783
577.748 587.748	.0598 .0511								.00002928	.03669	•782 •780
597.748	.0438	12.780	23.1559	251 • 479	10.4766	1.111	1.116	1.004	.00003004	.03824	•778
607.748 617.748	.0376								.00003043	.03902	•775 •773
627.748	.0280								.00003121		.772
637.748	.0242								.00003160	.04142	• 771
647.748 657.748	.0210								.00003200		•770 •769
667.748	.0159	39.871	25.8133	270.332	10.8837	1.114	1.137	1.019	.00003282	.04391	•768
677.748 687.748	.0139								.00003324	.04477	•768 •767
697.748	.0107								.000033411	.04653	.767
707.748	.0094	72.627							.00003458	.04744	.767
717.748 727.748	.0084 .0074								.00003506	.04837	•767 •767
737.748									.00003611		.768
747.748									.00003669		. 769
757.748 767.748									.00003730		•771 •773
777.748	.0043	189.619	30.2340	324.904	11.5775	1.131	1.282	1.121	.00003866	.05454	•775
787.748 797.748									.00003942		.778 .782
807.748									.00004023		• 182 • 786
817.748	•0029	312.907	32.1073	361.481	11.8178	1.139	1.399	1.209	.00004204	. 05 943	.790
827.748 832.087									.00004305		•794 •797
											,,

	T	v	р	H/RT <sub>O</sub>	A	$c_{\mathbf{p}}/\mathbf{R}$	γ	G	$\mathbf{z}$	$\mu$	k	$N_{Pr}$	
S/R=35.25													
	218.409	81 - 36 84	-003	11.2190	157-092	6.0961	1,196	1.196	1.000	.00001322	.00988	.771	
		64.5312		11.4450						.00001378		.766	
	238.409	51.3335		11.6769		6.4132	1.185	1.185	1.000	.00001432	.01136	.764	
	248.409	40.9494		11.9145		6.5699	1.179	1.179	1.000	.00001486	.01210	.762	
	258.409	32.7638		12.1578		6.7251	1.175	1.175	1.000	.00001539	.01284	.761	
	268.409			12.4068						.00001591		.761	
		21.1398		12.6614						.00001642		.761	
	288.409 298.409			12.9215						.00001693		.762	
	308.409	13.7663		13.1870 13.4580						.00001743		.763	
	318.409	9.0429		13.7342						.00001792		.765 .766	
	328.409	7.3518		14.0157						.00001888		.768	
	338.409	5.9887		14.3024		7.9038	1.145	1.145	1.000	.00001935	.01877	.770	
	348.409	4.8878		14.5941		8.0417	1.142	1.142	1.000	.00001982	.01951	.772	
	358.409	3.9969	•084	14.8908	196.385					.00002028		.774	
	368.409	3.2744		15.1924		8.3103	1.137	1.137	1.000	.00002073	• 02 099	.775	
	378.409	2.6874		15.4988						.00002118		.777	
	388.409	2.2096		15.8099		8.5684	1.132	1.132	1.000	.00002163	.02248	•779	
	398.409 408.409	1.8201		16.1255						.00002206		.780	
	418.409	1.2415		16.7701						.00002250		•782 •783	
	428.409	1.0280		17.0988						.000022335	.02544	.785	
	438.409	.8528		17.4316		9.1631	1.123	1.123	1.000	.00002377		786	
	448.409	•7087		17.7683						.00002418		.787	
	458.409	•5900		18.1089		9.3788	1.120	1.120	1.000	.00002459	.02767	.787	
	+68.409	•4921		18.4532		9.4815	1.119	1.118	1.000	.00002500	•02842	.788	
	478.409	•4111		18.8010						.00002540		.788	
	488.409 498.409	•3441 •2885		19.1522						.00002580		.789	
	508.409	•2424		19.8641		9.1002	1 114	1 114	1 000	.00002620 .00002659	03140	•789 •788	
	518.409	2040		20.2245		9-0504	1.114	1.113	1.000	.00002698	03215	.788	
	528.409	.1721		20.5877						.00002737		.787	
	538.409	.1454				10.0976	1.112	1.112	1.000	.00002775	.03366	.787	
	548.409	.1231	4.155	21.3214	240.C74	10.1700	1.111	1.112	1.001	.00002813	.03441	.785	
	558.409	•1045	4.588	21.6916	242.275	10.2383	1.111	1.112	1.001	.00002851	.03517	.784	
	568.409 578.409	.0888 .0757	5.574	22.0637	244.490	10.3024	1.110	1.112	1.001	.00002889	.03593	.783	
	588.409	•0645	9 500	22 43 11	240 122	10.3624	1.110	1.112	1.002	.00002927	.03669	.781	
	598.409	•0553	10-116	23.1901	251.273	10.4695	1-110	1.113	1.002	.00002985	02922	•779 •777	
	608.409	.0475	11.999	23.5681	253.608	10.5165	1.110	1.115	1.004	.00003041	03901	774	
	618.409	-0409	14.169	23.9417	255.987	10.5634	1.110	1.116	1.005	.00003079	.03979	.772	
	628.409	•0353	16.724	24.3220	258.410	10.6240	1.110	1.118	L.006	.00003117	.04058	.771	
	638.409	•0305	19.696	24.7038	260.906	10.6843	1.110	1.120	1.008	.00003155	.04137	.770	
	648.409	.0264	23.144	25.0869	263,493	10.7442	1.111	1.122	1.010	.00003194	.04217	•769	
	658.409 668.409	•0229 •0199	21.134	25 9674	266.187	10.8040	1.111	1.120	1.012	.00003233	• 04298	.768	
	678.409	.0174	37-046	26.2448	271.980	10.0030	1.112	1.134	1.019	.00003273	04466	.767 .766	
	688.409	•0152	43.141	26.6336	275.127	10.9828	1.113	1.139	1.022	.00003353	.04548	.765	
	698.409	.0133	50.125	27.0240	278.476	11.0425	1.114	1.146	1.026	.00003395	04634	.764	
	708.409	. •0117	58.108	27.4162	282.059	11.1023	1.115	1.153	1.031	.00003438	.04722	.764	
	718.409	.0103	67.234	27.8105	285.913	11.1624	1.116	1.161	1.037	.00003482	.04811	.763	
	728.409	•0091	77.592	28.2072	290.064	11.2227	1.118	1.171	1.044	.00003528	• 04902	.763	
	738.409	.0081	89.344	28.6067	294.553	11.2831	1.119	1.182	1.052	.00003577	04995	.763	
	748.409 758.409	0064	117 665	29.0098	294.420	11.3437	1.120	1.195	1.061	.00003628	.05091	.764	
	768.409	.0050	134,585	25.8200	310 451	11 6452	1 12/	1.224	1.002	.00003682	.05189	.764	
	778.409	•0052	153.604	30. 2492	316, 703	11.5258	1.126	1.244	1.096	.00003739	. 05290	.766 .767	
	788.409	•0047	174.934	30.6766	323.507	11.5861	1.128	1.264	1.111	.00003866	. 05502	.769	
	798.409	.0042	198.809	31.1141	330.916	11.6460	1.130	1.287	1.128	.00003336	.05613	.771	
	808.409	•0038	225.479	31.5€39	338.586	11.7050	1.131	1.312	1.147	.00004011	.05728	.774	
	818.409	•0035	255.219	32.0288	347.782	11.7631	1.133	1.339	1.168	.00004092	.05848	.778	
	828.409	•0032	288.328	32.5121	357.379	11.8197	1.135	1.370	1.191	.00004179	. 05972	.781	
	838.409	•0029	325.136	33.0177	367.868	11.8745	1.137	1.404	1.217	.00004271	.06101	.785	
	844.814	•0028	550.821	23.3553	5/5.103	A1.9084	1.138	1.427	1.235	.00004334	.06186	.788	

T	v	р	H/RTo	A	$c_p/R$	γ	G	$\mathbf{z}$	μ	k	$N_{\mathbf{Pr}}$
				S/F	R=35.50						
229.208 239.208	81.3630 64.7427		11.4634 11.6957						.00001382 .00001436		.766 .763
249.208	51.6661	.004	11,9338	166.601	6.5823	1.179	1.179	1.000	.00001490	.01216	.762
259.208 269.208	41.3499			169.561 172.466					.00001543		.761 .761
279.208	26.6823			175.319						.01438	.761
289.208	21.5114		12.9425	178.123 180.881	7.1931 7.3414				.00001697 .00001746	.01512	•762 •763
299.208 309.208	17.3817 14.0752		13.2085 13.4799	183.596					.00001746	.01661	.765
319.208	11.4216	•026	13.7566	186.269	7.6323	1.151	1.151	1.000	.00001844	.01735	•.766
329.208 339.208	9.2870 7.5663		14.0385	188.903					.00001892	.01809	.768 .770
349.208	6.1763	•053	14.6178	194.062	8.0524	1.142	1.142	1.000	.00001986	.01957	.772
359.208	5.0511		14.9149						.00002032	.02031	•774
369.208 379.208	4.1386 3.3971		15.2169 15.5237						.00002077	.02105	•776 •777
389.208	2.7935	.130	15.8352	203.988	8.5781	1.132	1.132	1.000	.00002166	.02253	.779
399.208 409.208	2.3013 1.8992	. 162	16.1513 16.4718	206.397					.00002210 .00002253	•02327 •02402	.781 .782
419.208	1.5701	.249	16.7967	211.138						.02476	.783
429 - 208	1.3003	.308	17.1258	213.472					.00002338	.02550	.785
439.208 449.208	1.0787 .8965	.467	17.4590 17.7962						.00002380	.02624	.786 .787
459.208	•7464	.573	18.1372	220.344	9.3860	1.120	1.119	1.000	•00002462	.02773	.787
469 • 208 479 • 208	.6225 .5201		18.4820						.00002503 .00002543	•02847 •02922	.788 .788
489.208	.4354			227.052					.00002543	.02996	.789
499.208	.3651	1.275	19.5369						.00002622	.03071	.788
509.208 519.208	.3067 .2581	1.548 1.875	19.8950						.00002661	.03145 .03220	.788 .788
529.208	.2177	2.267	20.6197	235.819	10.0242	1.112	1.112	1.000	.00002739	•03295	.787
539 - 208	.1839 .1557								.00002777 .00002815	.03370	•786 •785
549.208 559.208	•1321								.00002853	.03521	.784
569.208	.1123	4.732	22.0986	244.528	10.3018	1.110	1.111	1.001	.00002890		.782
579.208 589.208	.0956								.00002928 .00002965	.03672	.780 .778
599.208	.0698	8.019	23.2277	251.173	10.4651	1.109	1.112	1.002	.00003003	.03825	.776
609 • 208	.0599 .0516								.00003040	.03901	•774 •771
619.208 629.208	.0444		24.3630						.00003114		.770
639.208	.0383								.00003152	.04135	.769
649.208 659.208	.0332 .0287								.00003190	.04214	.768 .766
669.208	.0250	25.268	25.9039	268.042	10.8487	1.110	1.123	1.012	.00003266	.04374	.765
679.208	.0218		26.2926						.00003305	.04455 .04537	.764 .763
689.208 699.208	.0190								.00003344	.04621	.762
709.208	.0146	46.463	27.4674	279.912	11.0774	1.112	1.141	1.024	.00003424	•04706	.761
719.208 729.208	.0128 .0113	53.813		283.341 287.016					.00003465 .00003508	.04792 .04880	•761 •760
739.208	.0100								.00003552	.04969	.760
749 - 208	•0089								.00003598	.05060	.759
759.208 769.208	.0079 .0070								.00003646 .00003697	.05154	.760 .760
779.208	.0063	124.155	30.2850	310.175	11.4805	1.121	1.214	1.077	.00003751	.05348	.761
789.208 799.208	.0057								.00003808	.05449 .05554	•762 •763
809.208	•0046	183.201		329.297					•00003934		.765
819.208	•0042	207.716	32.0062	336.802	11.7106	1.128	1.292	1.135	.00004004	.05772	.767
829.208 839.208	.0038	235.045	32.4627	344.560	11.8219	1.130	1.344	1.175	.00004079 .00004159	.06006	.770 .773
844.814									.00004206		.775

T	v	p	H/RT <sub>O</sub>	A	$c_{\mathbf{p}}/\mathbf{R}$	γ	G	$\mathbf{z}$	μ	k	$N_{\mathbf{Pr}}$
				S/8	R=35.75						
240-147			11.7178						.00001441		.763
250.147			11.9564						.00001495		.762 .761
270.147			12.4507						.00001540		.761
280.147		.008	12.7063	175.586					.00001651		.761
290.147			12.9673						.00001701		.762
300.147 310.147			13.2338 13.5057						.00001751		•764
320.147			13.7829						.00001800		•765 •767
330.147	11.6980		14.0654						.00001896		.768
340.147	9.5322	.033	14.3530	191.744	7.9275	1.144	1.144	1.000	.00001943	.01890	.770
350.147	7.7824		14.6456						.00001990		.772
360 • 1 47 370 • 1 47	6.3657 5.2165		14.9432						.00002036		.774
380.147	4.2826		15.2457 15.5530						.00002081		•776 •777
390 • 147	3.5222		15.8650						.00002170		.779
400.147	2.9020		16.1815		8.7139	1.130	1.130	1.000	.00002214	.02334	.781
410.147	2.3952		16.5025						.00002257		•782
420.147 430.147	1.9804 1.6403		16.8278 17.1574						.00002300		.784 .785
440.147	1.3610		17.4911						.00002342		.786
450.147	1.1313		17.8287						.00002425		.787
460.147	.9419		18.1702		9.3948	1.119	1.119	1.000	.00002466	.02779	.787
470.147	.7857		18.5154						.00002506		.788
480 .147	•6565 •5496		18.8642 19.2164						.00002547		•788 •788
500 .147	4609		19.5719						.00002386		.788
510.147	.3872	1.228	19.9304	231.641	9.8671	1.113	1.113	1.000	.00002665	.03151	.788
520.147	.3259		20.2919						.00002703		.788
530.147 540.147	.2748 .2322								.00002742		•787
550.147	.1965								.00002788		.786 .785
560.147	.1667	3.135	21.7641	242.464	10.2410	1.110	1.110	1.001	.00002855	. 03526	.783
570.147	.1417	3.755	22.1377	244.624	10.3031	1.109	1.110	1.001	.00002892	.03601	•782
580.147	.1207								.00002930		.780
590.147 600.147	.1030 .0881	6.366	23.2692	251.161	10.4142	1.109	1.111	1.001	.00002967	.03752	•778 •776
610.147	.0755	7.555	23.6491	253.376	10.5071	1.108	1.111	1.002	.00003040	.03904	.773
620.147	.0650	8.929	24.0248	255.6C7	10.5545	1.108	1.112	1.003	.00003077	.03981	•771
630.147	.0559	1C.548	24.4074	257.857	10.6124	1.108	1.113	1.004	.00003114		•769
640.147	.0482	14.630	24.7910	260 - 145	10.5697	1.108	1.114	1.005	.00003150	.04135	•768 •767
660.147	.0361								.00003224		.765
670.147	.0313	20.124	25.9531	267.355	10.8382	1.108	1.119	1.009	.00003262	.04371	.764
690.147	•0273	23.528	26.3431	269.915	10.8936	1.108	1.121	1.011	.00003299	.04451	•763
690.147	.0238									.04531	.762
700.147 710.147	.0208									.04613	.761 .760
720.147	.0160									.04779	.759
730.147	.0140	49.819	28.3147	284.683	11.1675	1.111	1.144	1.027	.00003494		.758
740.147	.0124								.00003535		•757
750.147 760.147	.0109 .0097	66.302	29.1149	291 - 945	11.2771	1.113	1.159	1.038	.00003577	.05039	•756
770.147	.0085								.00003621		.756
780-147	.0077	100.164	30.3339	305.011	11.4421	1.117	1.190	1.061	.00003715	.05313	.756
790.147	.0069	114.455	3C.7473	310.C83	11.4973	1.118	1.203	1.071	.00003766	• 05409	.756
800.147	•0062	130.516	31.1654	315.575	11.5525	1.120	1.218	1.082	.00003820	.05508	• 757
810.147 820.147	•0056 •0050								.00003876		•758 •759
830.147	.0045	191.193	32.4598	334.968	11.7173	1.125	1.273	1.124	.00003937	.05820	.761
843.147	-0041	216.284	32.9099	342.551	11.7714	1.127	1.296	1.141	.00004071	.05931	.763
844.814	.0040	228.945	33.1242	346.307	11.7964	1.127	1.307	1.150	.00004105	• 05 984	.764

Ť	<b>v</b>	, <b>p</b>	H/RT <sub>o</sub>	A	$c_p/R$	γ .	G	$\mathbf{z}$	μ	k	$N_{\mathbf{Pr}}$
				\$/5	R=36.00						
	81.4244		11.9830						.00001501	.01231 .01305	.762 .761
261 • 246	52.3258		12.2280						.00001553		.761
281.246			12.7347						.00001656		.762
291.246		.008	12.9964	178.691					.00001707		.762
	27.4545		13.2635						.00001757		.764
311.246			13.5360 13.8138						.00001806		.765 .767
321.246	14.6869		14.0968						.00001901		.769
341.246	11.9703		14.3850						.00001949	.01898	.770
351.246	9.7748		14.6782		8.0798	1.141	1.141	1.000	.00001995	.01972	.772
361.246	7.9970		14.9763						.00002041	. 02 046	.774
371.246 381.246	6,5546 5,3822		15.2794						.00002086	.02120	.776 .778
391.246	4.4273		15.8997						.00002131	.02268	.779
401.246	3.6484	.103	16.2168						.00002219	.02342	.781
411.246	3.0118		16.5383		8.8481	1.127	1.127	1.000	.00002262		.782
421.246	2.4907	.158	16.8642						.00002304		.784
431.246 441.246	2.0633		17.1943 17.5284						.00002347	.02565	.785 .786
451.246	1.7122		17.8666						.00002388	.02713	.787
461.246	1.1853		18.2086						.00002470	.02787	.787
471 - 246	.9889		18.5543		9.5068	1.118	1.118	1.000	.00002511		.788
481.246	.8264		18.9036						.00002551	.02936	.788
491.246 501.246	.6918 .5802		19.2563							.03010	.788 .788
511.246	.4875		19.9714						.00002669	.03159	.788
521.246	.4104		20.3334						.00002707	.03233	.788
531.246	.3461								.00002745	.03308	.787
541.246	.2924								.00002783	.03383	.786
551.246 561.246	•2475 •2099	2.077 2.494							.00002821	.03457	.785 .783
571.246	.1784	2.987							.00002895	.03607	.781
581.246	.1519								.00002932	.03683	.780
591.246	.1296									.03758	•777
601.246	.1108									.03834	.775
611.246 621.246	.0950		24.0728							.03909	•772 •770
631.246	.0703								.00003114		769
641.246	.0606								.00003151		.767
651.246	.0524								.00003187	.04216	.766
661.246	0453		25.6166						.00003223	.04293	•764 •763
671.246 681.246	.0393								.00003296	.04371	.762
691.246	.0297								.00003333	.04529	.760
701.246	.0259								.00003370	.04609	•759
711.246	.0227								.00003408	.04690	•758
721.246	.0199								.00003446	.04772	•757
731,.246 741.246	.0175 .0154								.00003485	.04855 .04938	•756 •755
751.246	.0136								.00003563	.05024	.754
761.246	.0120									.05110	.753
771.246	.0106								.00003646	.05198	-753
781.246	.0095								.00003690		•752
791.246 801.246	.0084 .0075								.00003735	.05380	•752 •752
811.246									.000031834		.752
821.246	.0061	136.737	32.0589	320.905	11.6205	1.119	1.222	1.086	.00003887	.05668	.753
831.246		155,230							.00003944		.754
841.246									.00004004		.755
844.814	•00+0	103.012	23.0022	222.419	11.1437	1.144	1.204	1.113	.00004026	• 03711	.756

TABLE I.- THERMODYNAMIC PROPERTIES OF  $CF_4$  AT CONSTANT ENTROPY — Continued

T	v	p	H/RT <sub>O</sub>	A	$c_p/R$	γ	G	$\mathbf{z}$	μ	k	$N_{\mathbf{Pr}}$
S/R=36.25											
262.527	01 3904	003	12.2598	170 522	4 7003	1 172	1 172		00001540	01215	741
272.527			12.5111						.00001560		•761 •761
282.527			12.7679						.00001663	.01463	.762
292.527			13.0303							.01537	.763
302.527	34.3152		13.2981						.00001763	.01611	• 764
312.527 322.527										.01685	.765
332.527	18.3713		13.8498	187.152						.01759	•767 •769
342.527	14.9768	.021	14.4223							.01907	•771
352.527		.027	14.7162						.00002001		.772
362.527	10.0103		15.0150						.00002047	.02055	.774
372.527	8.2066		15.3187						.00002092		.776
382.527	6.7402		15.6271							• 02204	•778
392.527 402.527	5.5456 4.5709		15.9402 16.2579							.02278	.779
412.527	3.7741		16.5800						.00002224	.02352	.781 .783
422.527	3.1217		16.9065							.02500	.784
432.527	2.5866		17.2371						.00002352		.785
442.527	2.1469		17.5719						.00002393	.02648	.786
452.527	1.7851		17.9106						.00002435	.02722	.787
462.527 472.527	1.4868	• 290	18.2532 18.5994							.02797	•788 700
482.527	1.2406		18.9493						.00002516	.02945	• 788 • 788
492.527	.8683		19,3025							.03019	.788
502.527	•7283		19.6590						.00002634	.03094	.788
512.527	.6120		20.0186							.03168	.788
522.527	•5152		20.3812						.00002712		.787
532.527	•4346		20.7466						.00002750	.03317	.787
542.527 552.527	•3672 •3109		21.1146						.00002788 .00002825	.03391	.786 .784
562.527	.2637	1.990							.00002862		.783
572.527	.2241	2.383	22.2327	244.980	10.3110	1.108	1.109	1.001	.00002899	.03616	.781
582.527	.1908	2.848	22.6095	247.104	10.3667	1.108	1.109	1.001	.00002936		.779
592.527	.1628								.00002972	•03766	•777
602.527 612.527	.1392								.00003009	.03841	.774
622.527	.1193 .1026	4.796 5.668	24.1267	255.443	10.5559	1-107	1.109	1.002	.00003045	.03916	.772 .770
632.527	.0883	6.699	24.5111	257.786	10.6120	1.107	1.109	1.002	.00003117	• 04068	.768
642.527	.0761								.00003152	.04144	.767
652.527	.0657	9.301	25.2848	262.136	10.7216	1.106	1.110	1.004	.00003188	.04221	.765
662.527	.0568	10.927	25.6741	264.355	10.7752	1.106	1.111	1.005	.00003224		.764
672.527 682.527	• 04 92	12.813	26.0649	265.616	10.8282	1.106	1.112	1.006		.04375	.762
692.527	•0427 •0372	17.514	26.8508	271 206	10.8806	1.106	1 116	1 000	.00003295	.04452	.761 .759
702.527	.0324		27.2459	273.738	10.9837	1.106	1.118	1.010	.00003368	.04609	•758
712.527	.0283	23.756							.00003404		.757
722.527	.0248	27.587							.00003441		.756
732.527	.0217								.00003478		.754
742.527	•0191								.00003516		• 753
752.527 762.527	.0168	42.708 49.215							.00003554		.752 .751
772.527	.0131								.00003632		.750
782.527	.0117	64.999								.05271	.749
792.527	.0104		30.8688	301.739	11.4350	1.111	1.164	1.045	.00003714	.05359	.749
802.527	.0092	85.156							.00003758	.05449	•748
812.527	.0083	57.187							.00003803	.05541	•748
822.527 832.527									.00003851		•748 •748
842.527									.00003954		.749
844.814									.00003966		.749
		-									

T	v	p	H/RT <sub>O</sub>	· <b>A</b>	$c_p/R$	γ	G	$\mathbf{z}$	μ	k	$N_{\mathbf{Pr}}$
				S/F	R=36.50						
273.941			12.5471						.00001619		.761
283.941 293.941	65.5169 52.8802		12.8C47 13.0679						.00001670	01473	.762 .763
303.941	42.7721		13.3365						.00001770	.01622	.764
313.941	34.6698		13.6104						.00001819	.01696	.766
323.941	28.1602		13.8896						.00001867	.01770	•767
333.941	22.9185		14.1740						.00001914	.01844	•769
343.941 353.941	18.6888		14.4636						.00001961	.01918	.771 .773
363.941	12.4978		15.0577						.00002053	.02066	.775
373.941	10.2485			200.266					.00002098	.02140	.776
383.941	8.4193		15.6712						.00002143	.02214	.778
393.941	6.9289		15.9850	205.142					.00002187	.02288	.780
403.941	5.7124		16.3033		8.7596				.00002230	.02362	.781
413.941 423.941	4.7177 3.9031		16.6261 16.9532						.00002273		.783 .784
433.941	3.2348	.125		214.577					.00002318	.02585	.785
443.941	2.6855		17.6198						.00002399	.02659	
453.941	. 2.2334	.189	17.9591	219.155	9.3284	1.120	1.120	1.000	.00002440	.02733	.787
463.941	1.8607		18.3023						.00002481		.788
473.941 483.941	1.5528 1.2982	- 285	18.6491 18.9995		9.5323				.00002521	.02881 .02955	.788 .788
493.941	1.0872		19.3533						.00002501	.03030	788
503.941	.9122		19.7104						.00002640	.03104	.788
513.941	.7667	.625	20.0706		9.8953	1.113	1.113	1.000	.00002678	.03178	.788
523.941	.6455		20.4337						.00002717	• 03252	.787
533.941	.5445		20.7996						.00002755	.03327	.786 .785
543.941 553.941	.4602 .3896		21.1682						.00002792	.03401	.784
563.941	.3305								.00002867	.03550	.782
573.941	.2809									.03625	.781·
583.941	.2392								.00002940	.03700	•779
593.941	.2041	2.715			10.4218				.00002976	.03775	•776
603.941	.1745	3.229	23.8069						.00003013	.03850	•774 •771
623.941	.1286								.00003084	.04000	.769
633.941	.1106		24.5699						.00003120	.04076	.768
643.941	.0953								.00003155	.04151	.766
653.941	.0823								.00003190	.04227	.764 .763
663.941 673.941	.0711								.00003228		.761
683.941	.0535								.00003296		.760
693.941	.0465								.00003331		.759
703 -941	.0405	16.339							.00003367	.04612	•757
713.941	.0353	19.019							.00003402	. 04691	.756
723.941 733.941	.0309								.00003438	.04770	.754 .753
743.941	.0238								.00003511	.C4930	.752
753.941	.0209	34.278							.00003547	.05011	.751
763.941	•0184		29.7168	289.069	11.2703	1.107	1.133	1.022	.00003585	.05093	.749
773.941	.0163	45.508							.00003623	.05176	.748
783.941 793.941	.0144	52.288			11.3654				.00003661	.05260	•747
803.941	.0128 .0114	59.990 68.673							.00003700	.05346 .05432	•746 •745
813.941	.0101								.00003781	.05521	.745
823.941	.0091		32.1816	310.831	11.5553	1.111	1.176	1.055	.00003825	.05611	.744
833.941		101.873	32.6011	315.402	11.6028	1.113	1.187	1.064	.00003870	.05702	.744
843.941									.00003917	.05796	•744
844.814	•0072	111.026	23.0612	320.104	11.6045	1.114	1.201	1.074	.00003921	. 05804	.744

TABLE I.- THERMODYNAMIC PROPERTIES OF CF4 AT

CONSTANT ENTROPY — Continued

T	v	p	H/RT <sub>0</sub>	A	$c_p/R$	γ	G	$\mathbf{z}$	μ	k	$N_{Pr}$
				\$ / 5	R=36.75						
				37	(-304 )						
285.488	81.3911	.003	12.8451	177.090	7.1371	1.163	1.163	1.000	.00001678	.01485	.762
295.488	65.7011		13.1091						.00001728	.01559	.763
305.488	53.1656		13.3785						.00001777		.764
315.488	43.1082		13.6533						.00001826		•766
325.488 335.488	35.0251		13.9333						.00001874		•768 768
345.488	28.5142 23.2587		14.2185							.01855	.769 .771
355.488	19.0078		14.8042						.00002014	.02003	.773
365.488	15.5627			198.171					.00002060		.775
375.488	12.7653		15.4097							.02151	•777
385.488	10.4897		15.7195						.00002150		.778
395.488	8.6351	.043	16.0341	205.516	8.6556	1.131	1.131	1.000	.00002193	.02300	.780
405 • 488	7.1209		16.3531						.00002237		.781
415.488	5.8826		16.6766						.00002280	.02448	.783
425 - 488	4.8680		17.0043						.00002322	.02522	.784
435.488	4.0355		17.3363 17.6723							. 02596	• 785 784
445 • 488 455 • 488	3.3511 2.7877		18.0123						.00002446		•786 •787
465.488	2.3230		18.3560						.00002447	.02818	.788
475.488	1.9391			223.994					.00002527	.02892	.788
485 488	1.6215		19.0545	226.210					.00002567	.02967	.788
495 • 488	1.3583		19.4089						.00002607	.03041	.788
505.488	1.1399	.413	19.7665	230.590	9.8232	1.114	1.113	1.000	.00002646	.03115	.788
515.488	•9583		20.1272						.00002684		.788
525.488	.8071	.607		234.909					.00002722		.787
535.488	-6809		20.8574						.00002760	.03338	•786
545.488	•5756	.884		239.177					.00002798	.03412	.785
555.488 565.488	.4874 .4136	1.063							.00002835	.03487	•784 •782
575.488	.3515								.00002909	.03636	.780
585.488	•2994	1.824							.00002945		.778
595.488	.2555								.00002981		.776
605.488	•2185								.00003017		.773
615.488	.1876								.00003053	.03935	•770
625.488	.1610	3.626							.00003088		.769
635.488	.1385								.00003124		•767
645.488 655.488	•1193 •1030	5.951							.00003159		•766 •764
665.488	.0890								.00003194		.762
675.488	.0771								.00003263		.761
685.488	.0669								.00003298		.759
695.488	.0581	11.221	26.9830	270.792	10.9286	1.104	1.110	1.005	.00003333	.04541	.758
705.488	.0506	13.089	27.3800	273.020	10.9774	1.104	1.111	1.006	.00003368	.04618	.756
715.488	•0441								.00003403	• 04696	.755
725 • 488	.0385								.00003438	• 04774	•753
735 • 488	.0337								.00003473		•752
745.488 755.488	.0296 .0260								.00003508	.04931	.751 .749
765.488	•0229								.00003580		.748
775.488	.0202								.000033616		.747
785.488	.0178	42.063							.00003653		.745
795.488	.0158								.00003690		.744
805.488	.0140								.00003728		•743
815.488	•0125	63.293							.00003767		•742
825 • 488	.0111		32.2556						.00003807		.741
835-488	• 0099								.00003848		•740 •740
844.814	•0090	76.011	33.0034	317.310	11.0100	1.110	1.119	1.058	.00003888	10100	• 140

TABLE I.- THERMODYNAMIC PROPERTIES OF CF<sub>4</sub> AT

CONSTANT ENTROPY — Continued

T	· <b>v</b>	p	H/RT <sub>O</sub>	A	$c_p/R$	γ.	G	$\mathbf{z}$	μ	k	Npr
				S/F	R=37.00						
297.170	81.4244		13.1540		7.3110	1.158	1.158	1.000	.00001736	.01571	.763
307.170	65.9013		13.4244						.00001786		.765
317.170	53.4533		13.7000	185.734					.00001834		•766 •768
327.170 337.170	43.4450		14.2670						.00001929		.770
347.170	28.8686			193.551					.00001976		.771
357.170			14.8544		8.1596	1.140	1.140	1.000	.00002022	.02016	.773
367.170			15.1556						.00002068		•775
377.170			15.4615						.00002113		.777
387.170	13.0356		15.7722	203.506					.00002157		.779 .780
397.170 407.170	10.7340 8.8544		16.4073						.00002244		.782
417.170	7.3166		16.7315						.00002287		.783
427.170	6.0565		17.0600						.00002329		.784
437.170	5.0221		17.3927		9.1462	1.123	1.123	1.000	.00002371	.02608	.785
447.170	4.1716		17.7294						.00002413		.786
457.170	3.4711		18.0700						.00002453		•787
467.170	2.8933		18.4145							.02831	.788 .788
477.170 487.170	2.4159		18.7626						.00002574		.788
497.170	1.6932		19.4692							.03053	.788
507.170	1.4213		19.8274						.00002652		.788
517.170	1.1951	.403	2C-1887						•00002690	.03201	.788
527.170	1.0068	.488		235.261					.00002729		.787
537.170	-8497									.03350	•786
547.170	•7184		21.2896						.00002804		.785 .783
557.170 567.170	.6085 .5164								.00002878		.782
577.170	4391								.00002914		.780
587.170	.3740								.00002951	.03722	.778
597.170	.3192									.03797	.775
607.170	.2730								.00003022		.773
617.170	-2344	2.457							.00003058	.03946	•770 •768
627.170 637.170	.2013 .1731								.00003093	.04021	.767
647.170	.1491								.00003163	.04171	.765
657.170	.1287									04246	.763
667.170	.1112	5.607	25.8708	264.433	10.7817	1.104	1.107	1.002	.00003232	.04322	•762
677.170	.0963								.00003267		.760
687.170	.0835								.00003301		•759
697 .170	.0726		27.4529						.00003336	.04549	.757 .755
707.170 717.170	.0631 .0550								.00003310		.754
727.170	.0481									.04780	.752
737.170	.0420								.00003473	.04857	.751
747.170	.0368								.00003507	.04936	.749
757.170	.0323								.00003542		.748
767.170	•0284								.00003577		.747
777.170	•0251								.00003612		•745 •744
787.170 797.170	.0221 .0196		30.6853						.00003648	.05335	.743
807.170	.0173								.00003721	.05417	.741
817.170	.0154								.00003757	.05501	.740
827.170	.0137	58.305	32.3355	304.622	11.5127	1.106	1.147	1.035	.00003795	.05585	.739
837.170	.0122								.00003833		.738
844.814	.0112	13.464	33.0727	311.088	11.5883	1.108	1.160	1.045	.00003863	.05737	.737

TABLE I.- THERMODYNAMIC PROPERTIES OF CF<sub>4</sub> AT

CONSTANT ENTROPY — Continued

T	v	p	H/RT <sub>o</sub>	A	$c_p/R$	γ	G	$\mathbf{z}$	μ	k	$N_{\mathbf{Pr}}$
				S/R	=37.25						
309.023			13.4751						.00001795		•765
319.023	53.7018		13.7517 14.0336						.00001843		•766 •768
339.023		.007								.01881	.770
349.023	35.7095		14.6128							.01955	.772
359.023	29.2022	.011	14.9099	196.554	8.1844	1.139	1.139	1.000	.00002031	.02029	•774
369.023			15.2120						.00002076		•775
	19.6368		15.5188						.00002121	.02178	•777
389.023	16.1462		15.8303							• 02252	.779
399.023	13.2997		16.1465						.00002209	.02326	.781
409.023 419.023	10.9743 9.0713		16.4671						.00002252	.02400	•782 •783
429.023	7.5113		17.1214						.00002337		.785
439.023	6.2304		17.4549							.02622	.786
449.023	5.1769		17.7924						.00002420		.787
459.023	4.3089		18.1338							.02770	.787
469.023	3.5927		18.4789							.02844	.788
479.023	3.0008		18.8277						.00002541		.788
489.023	2.5108		19.1800						.00002581	.02993	.788
499.023	2.1044 1.7670		19.5357						.00002620	.03067	•788 •788
509.023 519.023	1.4863		20.2565						.00002697		.787
529.023	1.2524	.394							.00002736		.787
539.023	1.0572	.475							.00002773		.786
549.023	.8941	.573								.03438	.785
559.023	.7576			242.001	10.2234	1.109	1.109	1.000	.00002848	.03512	.783
569.023	.6431									.03586	.781
579.023	•5469								.00002921		.779
589.023	•4660								.00002957		•777
599.023	•3979								.00002993		•775 •772
609.023 619.023	•3404 •2923								.00003026	.03959	.769
629.023	2510								.00003099		.768
639.023	.2159									.04108	.766
649.023	.1860								.00003168	.04183	.765
659.023	.1605	3.835	25.5545	262.585	10.7368	1.104	1.106	1.002	.00003203	.04258	•763
669.023	.1387								.00003237		.761
679.023	.1201								.00003271	-04409	•760
689.023	.1041								.00003305		.758
699.023	.0905 .0787								.00003339	.04560 .04636	•756 •755
709.023 719.023	.0686								.00003407		.753
729.023	•0599								.00003441	.04789	.752
739.023	.0523								.00003475	· C4866	.750
749.023	•0458	15.363	29.1402	281.601	11.1614	1.102	1.112	1.008	.00003509	• 04943	.748
759.023	.0402		29.5457						.00003543	.05021	•747
769.023	.0353	20.525							.00003577	• 05 0 9 9	• 745
779.023	.0311								.00003611		•744
789.023	• 02 74								.00003646	.05257	•743
799.023 809.023	•0242 •0214								.00003681	.05417	.741 .740
819.023	.0190								.00003752	.05499	.738
829.023	.0169								.00003788		.737
839.023	.0150								.00003824		.736
844.814	.0141								.00003845		.735
•											

T	v	р	$H/RT_{O}$	Α	$c_{\mathbf{p}}/\mathbf{R}$	γ	G	${f z}$	$\mu$	k	$N_{\mathbf{Pr}}$
					-,						
				\$/1	R=37.50						
221 215	01 2072	004	12 0075	104 155	7 / 577	1 150	1 150	1 000	00001.052	01.740	.767
321.015 331.015			13.8075						.00001853		.768
341.015	53.9492		14.3785						.00001947		.770
351.015	44.0515		14.6716						.00001994		.772
	36.0373		14.9697						.00002040		.774
371.015			15.2727						.00002085		.776
381.015	24.2504		15.5805	202.007					.00002130		.778
391.015	19.9467		15.8930	204.439	8.5995	1.132	1.131	1.000	.00002174	. 02266	.779
401.015	16.4359		16.2100		8.7234	1.129	1.129	1.000	.00002217	.02340	.781
411.015	13.5668	.028	16.5316	209.222	8.8444	1.127	1.127	1.000	.00002261	.02415	.782
421.015	11.2181		16.8575						.00002303		•784
431.015	9.2921		17.1876						.00002345		.785
441.015	7.7101		17.5219						.00002387		.786
451.015	6.4085		17.8602						.00002428		.787
461.015	5.3359		18.2023						.00002469		.787
471.015	4.4505		18.5483						.00002509		.788
481.015	3.7184		18.8578						.00002549		.788 .788
491.015 501.015	3.1122 2.6094		19.2508	227.422					.00002589		.788
511.015	2.1917		19.9667						.00002627		.788
521.015	1.8441		20.3293						.00002705		.787
531.015	1.5545	.319							.00002743		.787
541.015	1.3127								.00002781		.786
551.015	1.1105	. 463							.00002818	.03452	.784
561.015	.9412	• 556							.00002855	.03526	.783
571.015	• 7992	.666	22.1822	244.493	10.2953	1.108	1.108	1.000	.00002891	.03601	.781
581.015	•6799									•03675	.779
591.015	•5795								.00002964		•777
601.015	.4949								.00003000		•774
611.015	.4235								.00003035		.771
621.015	.3638								.00003070		.769
631.015	.3124								.00003105		.767
641.015	.2687 .2315								.00003140		.766 .764
651.015 661.015	.1998								.00003174	.04197	.762
671.015	.1727									.04346	.761
681.015	.1496								.00003277		.759
691.015	-1297								.00003311		.758
701.015	.1126									.04572	.756
711.015	.0980								.00003378	-04648	•754
721.015	•0854	7.906	28.0159	275.051	11.0304	1.102	1.106	1.004	.00003411	.04724	.753
731.015	• C745	9.192	28.4181	277.140	11.0750	1.102	1.107	1.005	.00003445	• 04800	.751
741.015	.0651								.00003478	.04876	•749
751.015	.0570									•04953	•748
761.015	.0500								.00003545		.746
771.015	• 0439									.05107	.744
781.015	-0386								.00003612		.743
791.015	.0340									• 05263	•741
801.015	.0300								•00003679		•740
811.015	.0266								.00003714		•738
821.015 831.015	•0235 •0209									.05501	•737 •736
841.015	.0186								.00003783		• 734
844.814	.0178								.00003832		.734
2		,,,,,,	2340071	200000	-402761	~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~			- 50003032		•154

TABLE I.- THERMODYNAMIC PROPERTIES OF CF<sub>4</sub> AT

CONSTANT ENTROPY — Continued

T	v	p	H/RTo	A	$c_p/R$	γ	G	${f z}$	μ	k	$N_{\mathbf{Pr}}$
				S/F	R=37.75			•			
333.140	81.3857	.004	14. 1512	189.937	7.8293	1.146	1.146	1.000	.00001910	.01838	.769
	66.3360		14.4403						.00001957		.771
353.140			14.7345						.00002004		.773
			15.0337						.00002049	. 02 060	•774
373.140			15.3377							.02134	.776
393.140	29.8722		15.6465 15.9600						.00002139	.02208	.778 .780
	20.2613		16.2780						.00002237	.02356	.781
413.140			16.6005						.00002270	. 02430	.783
	13.8391		16.9273						.00002312	.02504	.784
433.140	11.4673	•035	17.2584	214.396	9.1009	1.123	1.123	1.000	.00002354	.02578	.785
443.140	9.5184		17.5935						.00002396	.02652	.786
453.140	7.9144		17.9326						.00002437	.02727	.787
463.140	6.5921		18.2756						.00002478	.02801	.788
473.140	5.5002 4.5971		18.6223						.00002518	.02875	-788
483.140 493.140	3.8491		19.3264						.00002558	.02949	•788 •788
503.140	3.2284		19.6835						.00002636	.03097	.788
513.140	2.7125		20.0437						.00002675	. 03 1 71	.788
523.140	2.2832	-214	20.4070	234.382					.00002713	.03245	.787
533.140	1.9252	.258	20.7731	236.516	10.0439	1.111	1.111	1.000	.00002751	.03319	.786
543.140	1.6263								.00002788	.03394	•785
553.140	1.3763								.00002826	.03468	.784
563.140	1.1669								.00002863	.03542	.782
573.140 583.140	•9912 •8435								.00002899	.03616	.781 .779
593.140	•7192								.00002931	.03765	.776
603.140	.6144								.00003007	.03839	.774
613.140	.5259								.00003042	.03913	.771
623.140	.4519								.00003077		.769
633.140	.3882	1.522	24.5501	257.193	10.5980	1.105	1.105	1.001	.00003112	.04062	.767
643.140	.3340								.00003147	.04137	.765
653.140	.2878	2.118							.00003181	.04211	. 764
663.140 673.140	•2484 •2148								.00003215	.04286	•762
683.140	.1860								.00003249	.04361	•760 •759
693.140	.1613								.00003203		.757
703.140	.1401								.00003350	.04586	.755
713.140	.1219								.00003383	.04661	.754
723.140	.1062	6.371	28.1048	275.182	11.0354	1.101	1.105	1.003	.00003416	.04737	.752
733.140	•0926								.00003449	.04812	•750
743.140	.0809								.00003482	.04888	•749
753.140	.0708								.00003515	. 04964	•747
763.140	•0621								.00003548	.05041	.745
773.140 783.140	•0545 •0479								.00003581	.05117 .05194	•744 •742
793.140	.0422								.00003647	.05272	.740
803.140	.0372								.00003680		.739
813.140	.0329	23.353							.00003714		.737
823.140	.0291	26.768							.00003747		.736
833.140	.0258	30.636							.00003781		.734
843.140	•0229	35.009	33.0264	302.523	11.5197	1.102	1.125	1.021	.00003815	. 05666	.733
844.814	•0225	35. (97	33.0964	302 - 584	11.5259	1.102	1.126	1.022	.00003821	.05680	.732

T	. <b>V</b>	p	H/RT <sub>o</sub>	A	$c_p/R$	γ	G	$\mathbf{z}$	$\mu$	k	$N_{\mathbf{Pr}}$
				S/F	R=38.00						
345.399	81.3935	•004	14.5064	193.100	7.9995	1.143	1.143	1.000	.00001968	.01929	.771
355.399	66.4952		14.8017							.02003	.773
365.399	54.4578		15.1020	198.151					.00002060		.775
375.399	44.6673		15.4071	200.629					.00002105	.02151	.777
385.399	36.7035		15.7170	203.078					.00002149	.02225	.778
395.399	30.2132		16.0315	205.498	8.6541				.00002193		.780
.405 .399	24.9144		16.3505	210.258					.00002236	.02447	.781 .783
415.399 425.399	20.5809		16.6740	212.600					.00002219		.784
435.399	14.1173	.029	17.3338	214.918					.00002364		.785
445.399	11.7226	•C35	17.6699						.00002405		.786
455.399	9.7509		18.0099	219.487					.00002446		.787
465.399	8.1248	.053	18.3537	221.739	9.4457	1.118	1.118	1.000	.00002487	.02817	.788
475.399	6.7817	• 06:5	18.7013	223.972					.00002527		.788
485.399	5.6704		19.0524						.00002567		.788
495.399	4.7495	.097		228.380					.00002606	.03040	.788
505.399	3.9851		19.7648						.00002645	.03114	.788 .788
515.399	3.3497 2.8205	•143 •174	20.1257						.00002683		.787
525.399 535.399	2.3793		20.4597						.00002722		.786
545.399	2.0106		21.2258	239.107					.00002797		.785
555.399	1.7022		21.5978						.00002834		.784
565.399	1.4438	.365	21.9720						.00002871	. 03 558	.782
575.399	1.2268	.437	22.3485	245.376	10.3190	1.107	1.108	1.000	.00002907	.03633	.780
585.399	1.0445	.523								.03707	.778
595.399	.8909	.623							.00002979		.776
605.399	.7614								.00003015		•773
615.399	.6532								.00003050	.03930	•770
625.399	.5603								.00003085	• 04 004	•768
635.399 645.399	.4814 .4143	1.453							.00003120	.04078	.767 .765
655.399	.3572								.00003134	04227	.763
665.399	.3084	2.C14							.00003222	.04302	.762
675.399	.2666									. 04377	.760
685.399	.2309								.00003290	.04451	.758
695.399	.2003	3.242							.00003323	•04526	•756
705.399	.1740	3.788							.00003356	.04601	•755
715.399	.1513	4.417							.00003389	.04676	.753
725.399	.1318									• 04751	.751
735.399	.1150	5.979								• 04827	•750
745.399	.1005		29.0068						.00003488	•04902	•748
755.399 765.399	.0880 .0771	8.041 9.303							.00003520	.04978 .05054	•746 •744
775.399	.0677	10.747							.00003585	.05130	.743
785.399	.0595	12.396								.05206	.741
795.399	.0524	14.277								.05283	739
805.399	.0462		31.4639						.00003683		.738
815.399	.0408	18.851	31.8779						.00003715		.736
825.399	.0361	21.612	32.2931	296.625	11.4417	1.100	1.114	1.013	.00003748	• 05516	.735
835.399	.0319									.05594	.733
844.814	.0285	28.061	33.1028	301.366	11.5125	1.100	1.119	1.017	.00003812	.05668	.731

TABLE I.- THERMODYNAMIC PROPERTIES OF CF<sub>4</sub> AT

CONSTANT ENTROPY — Continued

T	v	p	H/RT <sub>O</sub>	A	$c_p/R$	γ	G	$\mathbf{z}$	μ	k	$N_{\mathbf{Pr}}$
				\$/1	R=38.25						
367.796 377.796 387.796 397.796 407.796 417.796	54.7172 44.9807 37.0423 30.5586 25.2538	.005 .006 .008 .010 .012 .015	14.8733 15.1747 15.4810 15.7919 16.1076 16.4277	198.748 201.219 203.661 206.074 208.461 210.821	8.3009 8.4313 8.5589 8.6837 8.8056 8.9245	1.137 1.134 1.132 1.130 1.128 1.126	1.137 1.134 1.132 1.130 1.128 1.126	1.000 1.000 1.000 1.000 1.000		.02094 .02168 .02243 .02317 .02391 .02465	.773 .775 .777 .779 .780 .782 .783
437.796	20.9062 17.3370 14.4020 11.9845 9.9901 8.3420 6.9779 5.8470	.024 .029 .036 .044 .053	17.0810 17.4140 17.7510 18.0920 18.4368 18.7852 19.1372 19.4925	215.470 217.760 220.029 222.276 224.504 226.712	9.1527 9.2619 9.3676 9.4698 9.5683 9.6631	1.123 1.121 1.119 1.118 1.117 1.115	1.123 1.121 1.119 1.118 1.117	1.000 1.000 1.000 1.000 1.000	.00002332 .00002374 .00002415 .00002456 .00002496 .00002576 .00002576	.02613 .02687 .02761 .02835 .02909 .02983	.784 .786 .786 .787 .788 .788
.507.796 517.796 527.796 537.796 547.796 557.796 577.796	4.9080 4.1271 3.4766 2.9339 2.4804 2.1008 1.7826 1.5153	.117 .142 .171 .206 .248 .297	20.9449 21.3150 21.6875 22.0624	233.231 235.372 237.497 239.607 241.705 243.789	9.9241 10.0030 10.0776 10.1479 10.2137 10.2751	1.112 1.111 1.110 1.109 1.109	1.112 1.111 1.110 1.109 1.109	1.000 1.000 1.000 1.000 1.000	.00002879	.03205 .03280 .03354 .03428 .03502	.788 .788 .787 .786 .785 .783 .782
587.796 597.796 607.796 617.796 627.796 637.796 647.796	1.2906 1.1013 .9416 .8081 .6934 .5960 .5131	.425 .506 .602 .713 .844 .998	22.8183 23.1990 23.5814 23.9596 24.3451 24.7324 25.1217	247.924 249.976 252.018 254.049 256.048 258.037 260.016	10.3837 10.4308 10.4730 10.5133 10.5675 10.6205 10.6725	1.107 1.106 1.106 1.105 1.105 1.104 1.104	1.107 1.106 1.106 1.106 1.105 1.105	1.000 1.000 1.000 1.000 1.000 1.000	.00002952 .00002987 .00003023 .00003058 .00003093	.03724 .C3799 .03873 .03947 .04021 .04096	.777 .775 .772 .769 .768 .766
667.796 677.796 687.796 687.796 697.796 707.796 717.796 727.796	.3821 .3304 .2862 .2483 .2157 .1877 .1635	1.631 1.914 2.243 2.624 3.064 3.572 4.158	25.9056 26.3001 26.6964 27.0943 27.4937 27.8948 28.2973	263.949 265.906 267.858 269.808 271.757 273.708 275.663	10.7729 10.8215 10.8691 10.9156 10.9612 11.0057 11.0494	1.103 1.102 1.102 1.102 1.101 1.101	1.104 1.103 1.103 1.103 1.103 1.103	1.001 1.001 1.001 1.001 1.002 1.002	.00003230 .00003263 .00003297 .00003330 .00003363 .00003396	.04543 .04617 .04692 .04767	.763 .761 .759 .758 .756 .754 .752
747.796 757.796 767.796 767.796 787.796 797.796 807.796 817.796	.1247 .1091 .0956 .0839 .0737 .0649 .0572	5.609 6.498 7.518 8.684 10.016 11.535 13.265 15.231	29.1067 29.5136 29.9218 30.3313 30.7421 31.1542 31.5675 31.9820	279.595 281.579 283.580 285.602 287.649 289.727 291.842 294.000	11.1340 11.1750 11.2152 11.2546 11.2933 11.3313 11.3686 11.4054	1.100 1.100 1.099 1.099 1.099 1.099	1.103 1.104 1.105 1.106 1.107 1.108 1.109	1.003 1.003 1.004 1.005 1.006 1.007 1.008	.00003461 .00003494 .00003556 .00003558 .00003659 .00003622 .00003654 .00003718	.04918 .04993 .05069 .05144 .05220 .05296 .05373 .05450	.749 .747 .746 .744 .742 .740 .739 .737
837.796 844.814	.0446 .0395 .0363	19.996	32.8148	298.476	11.4771	1.099	1.112	1.012	.00003751 .00003783 .00003805		.733 .732 .731

TABLE I.- THERMODYNAMIC PROPERTIES OF  $CF_4$  AT CONSTANT ENTROPY — Continued

Т	v	p	H/RTo	A	$c_p/R$	γ	G	Z	μ	k	$N\mathbf{p_r}$
				s/1	R=38.50						
370.338	81.4244		15.2521						.00002082		•776
380.338 390.338	66.8444 54.9744		15.5596						.00002127		•777 •779
400.338	45.2926		16.1885								.781
410.338	37.3814		16.5098								.782
420.338	30.9058		16.8354						.00002300		.784
430.338	25.5963	.016	17.1653	213.748					.00002343		.785
440.338	21.2357	.019	17.4993	216.055	9.1807	1.122	1.122	1.000	.00002384	.02632	.786
450.338	17.6483	•024	17.8374	218.339						.02706	.787
460.338	14.6923		18.1793						.00002466		.787
470.338	12.2526		18.5251						.00002507		.788
480.338	10.2357		18.8744						.00002547		.788
490.338	8.5656		19.2273							.03002	•788 700
500.338	7.1806		19.5835						.00002625		.788 .788
510.338 520.338	6.0301 5.0729		20.3054						.00002664		.787
530.338	4.2752										.787
540.338	3.6094		21.0389						.00002778	.03372	.786
550.338	3.0528		21.4097							.03446	.784
560.338	2.5868								.00002852		.783
570.338	2.1959								.00002889	.03595	.781
580.338	1.8676								.00002925	.03669	.779
590.338	1.5913	• 346	22.9153	248.435	10.3958	1.107	1.107	1.000	.00002961	.03743	•777
600 • 338	1.3585	•412	23.2965	250.482	10.4416	1.106	1.106	1.000	•00002996	.03817	•774
610.338	1.1620	• 490							.00003032		• 772
620.339	.9977								.00003067		.769
630.338	8565								.00003102		•767
640.338	.7364								.00003136		.766
650.338	.6341	.957							.00003170		.764
660.338 670.338	•5469 •4725								.00003204	.04203	.762 .761
680.338	.4087		26.4018							.04412	.759
690.338	.3541	1.819							.00003305		.757
700.338	.3073								.00003338	.04561	.755
710.338	.2670								.00003371		.754
720.338	.2324								.00003403	.04710	.752
730.338	.2025	3.369	28.4017	275.996	11.0580	1.100	1.102	1.002	.00003436	.04785	.750
740.338	.1767	3.914	28.8063	277.929	11.1002	1.100	1.102	1.002	.00003468	.04860	.748
750.338	•1544		29.2123						.00003500		.747
760.338	.1351								.00003532		.745
770.338	.1184	6.C85								.05085	.743
780.338	.1039	7.027	30.4385							.05160	.741
790.338	.0913	8.104								.05236	.740
8.00.338	.0804								.00003660		.738
810.338	.0708	10.731							.00003691		•736
820.338 830.338	.0625 .0552	12.322							.00003723		.734 .733
840.338	.0489								.00003786		.731
844.814	.0463								.00003780		.730
3446314	•0,05	11.100	22.1122	2774121	FF # 4 70 3	1.070		1.010	100003000	* 07072	21,50

т	v	p	H/RT <sub>o</sub>	A	c <sub>p</sub> /R	γ	G	Z	μ	k	$N_{\mathbf{Pr}}$
				S/S	R=38.75						
393.045 403.045 413.045 423.045 433.045 453.045 463.045 463.045 503.045 513.045 523.045 533.045 563.045 633.045	45.5889 37.7092 31.2455 25.9345 21.5634 17.9600 14.9846 12.5238 10.4853 8.7940 8.7940 8.7940 8.1770 2.6983 2.2959 1.9573 1.6718 1.4306 1.2289 1.9573 1.6718 1.4306 1.2289 1.9573 1.6718 1.4306 1.2289 1.9573 1.6718 1.4306 1.2289 1.9573 1.6718 1.4306 1.2289 1.9573 1.6718 1.4306 1.2289 1.9573 1.6718 1.4306 1.2289 1.9573 1.6718 1.4306 1.2289 1.9573 1.9079 1.8184 1.90994	.005 .007 .010 .013 .016 .020 .024 .029 .036 .078 .078 .078 .078 .138 .165 .198 .233 .336 .400 .403 .559 .661 .797 .71.263 .717 .727 .737 .737 .737 .737 .737 .737 .73	21.1392 21.5106 21.8844 22.2605 22.6386 23.0186 23.4003 23.7835 24.1626 24.5492 24.5492 24.57203 26.1142 26.5099 27.7068 28.1089 28.1089 28.1089 28.1089 28.1089 28.1089 28.1089 28.1089 28.1089 28.1089 28.1089 28.1089 28.1089 28.1089 28.1089 28.1089 28.1089 28.1089 28.1089 29.7321 30.1414 30.5521 30.9640 31.3772	202.505 204.931 207.330 209.703 212.051 214.375 216.675 218.554 221.211 223.4488 225.665 227.863 230.044 232.207 234.354 236.485 238.601 240.702 242.790 244.866 246.929 244.866 257.065 257.065 257.065 257.065 257.066 257.065 257.065 257.065 257.066 268.72 269.82 270.668 270.	8.4986 8.6248 8.7481 8.9856 9.0996 9.2104 9.3177 9.4216 9.5219 9.6184 9.7112 9.8850 9.9658 10.0424 10.1147 10.11426 10.2460 10.3049 10.3590 10.4528 10.4528 10.4528 10.4923 10.5408 10	1.131 1.129 1.127 1.125 1.123 1.122 1.120 1.116 1.115 1.114 1.113 1.112 1.111 1.110 1.106 1.105 1.106 1.105 1.104 1.103 1.102 1.101	1.131 1.129 1.127 1.125 1.123 1.120 1.117 1.116 1.115 1.114 1.110 1.100 1.106 1.106 1.106 1.106 1.106 1.106 1.106 1.106 1.106 1.107 1.108 1.109	1.000 1.000	-00002517 -00002597 -00002636 -00002674 -00002713 -00002788 -00002898 -00002898 -00002898 -00002970 -00003016 -00003016 -00003179 -00003179 -00003179 -00003179 -00003179 -00003179 -00003179 -00003179 -00003508 -00003508 -00003508 -00003508 -00003603 -00003603 -00003603 -00003603	.02281 .02355 .02429 .02578 .02578 .02578 .02652 .02726 .02874 .03922 .03096 .03170 .03318 .03318 .03318 .03515 .03615 .03683 .03541 .03615 .03683 .03837 .03981 .04060 .041208 .041208 .044508 .04654 .04654 .04653 .04653 .04653 .04653 .055103 .055259	.780 .781 .783 .7881 .7886 .7888 .7888 .7888 .7888 .7888 .7888 .7887 .7865 .7765 .7765 .7765 .7765 .7755 .77
813.045 823.045 833.045	•0994 •0876 •0773 •0683	8.69 <b>7</b> 9.585	31.7916	291.876 293.884	11.3771	1.098	1.104	1.005	.00003666 .00003697 .00003728 .00003760	.05405	.737 .735 .733
843.045 844.814	.0604 .0591	13.108	33.0420	297.993	11.4806	1.098	1.106	1.008	.00003791 .00003796	.05633	.730 .730
				\$/1	R=39.00		,				
405.896 415.896 425.896 435.896 445.896 455.896 465.896 475.896	45.8915 38.0440 31.5929 26.2809 21.8999 -18.2807 15.2862 12.8044	.006 .007 .009 .011 .013 .016 .020 .024 .030 .036 .044 .053 .064 .078 .054 .113	21.2449 21.6171 21.9916 22.3683	208.010 210.375 212.716 215.033 217.327 219.599 221.851 224.082 226.293 228.486 230.661 234.561 237.088 239.199 241.296 243.380 245.451	8.7826 8.9021 9.0184 9.1315 9.2413 9.3476 9.4505 9.5497 9.6452 9.8826 9.9880 10.0633 10.1344 10.2010 10.2631 10.3206	1.128 1.126 1.125 1.123 1.121 1.120 1.118 1.117 1.116 1.114 1.113 1.112 1.111 1.110 1.109 1.109 1.109	1.128 1.126 1.123 1.121 1.120 1.118 1.117 1.116 1.114 1.113 1.112 1.110 1.109 1.109 1.109	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	.00002195 .00002239 .0000236 .00002366 .00002407 .00002489 .00002529 .00002569 .00002608 .00002647 .00002798 .00002798 .00002798 .00002836 .00002872 .00002995	.02377 .02451 .02552 .02599 .02673 .02747 .02895 .02969 .03043 .03117 .03191 .03265 .03488 .03488 .03562	.780 .782 .783 .784 .785 .786 .788 .788 .788 .788 .788 .788 .788

T	v	р	H/RTo	A	$c_p/R$	γ	G	Z	μ	k	$Np_r$
				\$/1	₹=39.00						
595.896 615.896 625.896 635.896 645.896 655.896 655.896 675.896 715.896 725.896 735.896 745.896 785.896 896.896 896.896 896.896 896.896	2.4023 2.0529 1.7611 1.5106 1.2978 1.1167 .9624 .8307 .7180 .6216 .5389 .4679 .4068 .3542 .3088 .2696 .2357 .2063 .1809 .1587 .128 .1082 .0955 .0844 .0756	. 275 . 326 . 386 . 457 . 539 . 636 . 748 . 678 1. 205 1. 408 1. 642 1. 913 2. 225 2. 583 2. 995 3. 468 4. 009 4. 628 5. 335 6. 141 7. 059 8. 289	23.5096 23.8877 24.2730 24.6602 25.0493 25.4402 25.8330 26.2275 26.6237 27.0216 27.4211 27.8222 28.6291 29.0347 29.4418 29.8503 30.2601 30.6713 31.0837 31.4974 31.4974 31.4974 32.3285 32.7458	251.594 253.622 255.613 257.591 259.556 261.509 263.452 265.384 267.307 269.222 271.129 273.031 274.927 276.820 278.711 280.601 282.493 284.389 286.291 292.058 290.122 292.058 294.011 295.987	10.4643 10.5016 10.5558 10.6608 10.7611 10.8095 10.9484 10.9926 11.0358 11.193 11.1596 11.193 11.1596 11.193 11.3481 11.3481 11.3481 11.3481 11.3481 11.4516	1.106 1.105 1.105 1.104 1.103 1.103 1.102 1.101 1.101 1.100 1.100 1.100 1.100 1.099 1.099 1.099 1.099 1.098 1.098 1.098 1.098	1.106 1.105 1.105 1.104 1.103 1.103 1.102 1.102 1.102 1.101	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.001 1.001 1.001 1.001 1.002 1.002 1.002 1.003 1.003 1.003 1.004 1.005	.00003120 .00003155 .00003189 .00003223 .00003256 .00003289 .00003355	.03858 .03932 .04006 .04081 .04155 .04229 .04377 .04452 .04526 .04601 .04675 .046749 .04824 .04824 .04899 .04973 .050198 .05123 .05198 .05348 .05423 .05429 .05574	.775 .773 .768 .766 .766 .7663 .761 .756 .756 .754 .755 .751 .749 .745 .744 .742 .744 .742 .738 .734 .734 .734 .734
				\$/1	R=39.25						
418.895 428.895 438.895 448.895 458.895 468.895 478.895 488.895	81.3903 67.2703 55.7026 46.2007 38.3863 31.9486 26.6365 22.2460 18.6115 15.5980 13.0952 11.0135 9.2791 6.6222 5.6095 4.7605 4.7605 4.7605 4.7605 1.8529 1.5926 1.3710 1.1820 1.0206 .8826 .7644 .6629 .5757 .5007 .4361 .8303 .3321 .2904 .2543 .2230	.006 .007 .009 .011 .013 .016 .020 .024 .030 .036 .044 .053 .064 .077 .093 .111 .133 .159 .190 .226 .247 .316 .374 .441 .717 .843 .849 .849 .849 .849 .849 .849 .849 .849	20.9859 21.7593 22.1045 22.4818 22.8611 23.2421 23.6247 24.0033 24.3892 24.7770 25.5582 25.9515 26.3466 26.7434 27.1419 27.5419 27.9436 28.7515 29.1573 29.9773	211.080 213.414 215.724 218.011 220.277 222.522 224.747 226.953 229.140 231.310 233.463 235.600 237.721 239.828 241.920 243.999 246.065 248.120 250.163 252.195 254.211 256.196 258.167 260.125 262.072 264.006 257.845 262.072 264.006 271.646 273.536 271.646 273.536 271.646 273.536 277.298 277.298 277.298 279.172 281.044 282.915	8.9373 9.0526 9.1648 9.2735 9.3788 9.4806 9.5787 9.6731 9.7636 9.8501 9.9326 10.0109 10.1548 10.2200 10.1548 10.2200 10.3368 10.4345 10.4760 10.5717 10.6757 1	1.126 1.124 1.122 1.121 1.119 1.118 1.116 1.115 1.114 1.111 1.110 1.109 1.108 1.107 1.107 1.106 1.105 1.105 1.105 1.101 1.100 1.100 1.100 1.100 1.100 1.100 1.100 1.100	1.126 1.124 1.122 1.119 1.118 1.116 1.115 1.114 1.113 1.112 1.111 1.100 1.108 1.107 1.106 1.105 1.105 1.104 1.103 1.102 1.101 1.101 1.101 1.101 1.101 1.101 1.101 1.101 1.101 1.101 1.101 1.101 1.101 1.101 1.101 1.101 1.100	1.000 1.000	.00002251 .00002378 .00002378 .00002420 .00002501 .00002541 .00002541 .00002658 .00002677 .00002772 .00002810 .00002847 .00002810 .00002847 .00002810 .00002810 .00003165 .00003165 .00003165 .00003165 .00003165 .00003165 .00003165 .00003166 .00003191 .00003266 .00003191 .00003266 .00003191 .00003266 .00003193 .00003299 .000035257 .00003462 .00003493 .00003462	.02473 .02547 .026621 .02695 .02769 .02843 .02991 .03103 .03139 .03287 .03352 .03510 .03510 .03510 .03558 .03732 .03806 .03510 .03806 .03806 .03806 .03906 .04107 .04251 .04325 .04427 .04627 .04627 .04627 .04697 .04920 .04990 .04990	.782 .783 .785 .787 .788 .788 .788 .788 .787 .785 .785
788.895 798.895 808.895 818.895 828.895 838.895 844.814	.1958 .1721 .1515 .1335 .1178 .1041	3.765 4.339 4.993 5.739 6.586 7.548	30.7963 31.2093 31.6235 32.0390 32.4556 32.8734	286.663 288.542 290.429 292.326 294.236 296.161	11.2841 11.3204 11.3559 11.3906 11.4245 11.4577	1.098 1.098 1.098 1.097 1.097	1.100 1.100 1.101 1.101 1.101 1.102	1.002 1.002 1.003 1.003 1.004 1.004	.00003619 .00003650 .00003681 .00003712 .00003773	.05219 .05293 .05368 .05443 .05519	.739 .737 .736 .734 .732 .730

TABLE I.- THERMODYNAMIC PROPERTIES OF CF<sub>4</sub> AT

CONSTANT ENTROPY — Continued

T	v	p	H/RT <sub>0</sub>	A	$c_p/R$	γ	G	Z	μ	k	$N_{\mathbf{Pr}}$
				SZF	R <b>≠39</b> •50						
422.046			16.8915						.00002308		•78 <u>4</u>
442.046	67.4235		17.2222 17.5569						.00002350		.785 .786
	46.5167		17.8956						.00002331		.787
462.046	38.7366		18.2383						.00002473		.787
472.046			18.5846						.00002513		.788
482.046			18.9346						.00002553		.788
502.046	22.6027		19.2881						.00002593	.03015	•788 •788
512.046			20.0049						.00002670		.788
522.046			20.3679						.00002709		.787
532.046									.00002747		.786
542.046	9.5377								.00002784		.785
552.046 562.046	8.0691 6.8391	-077	21-8474	240.481	10.2396	1.109	1.108	1.000	.00002821 .00002858	03459	•784 •783
572.046	5.8072	.092	22.2233	244.649	10.2988	1.108	1.108	1.000	.00002895	.03607	.781
582.046	4.9402	.110	22.6012	246.711	10.3533	1.107	1.107	1.000	.00002931	.03681	.779
592.046	4.2105								.00002967		.776
602.046	3.5954								.00003002		•774
612.046 622.046	3.0760 2.6416								.00003037		.771 .769
632.046	2.2680								.00003107		.767
642.046	1.9503	.307	24.8999	258.773	10.6403	1.104	1.104	1.000	.00003141	.04126	.765
652.046	1.6797	.362	25.2902	260.725	10.6914	1.103	1.103	1.000	.00003176	• 04200	.764
662.046	1.4488								.00003209		.762
672.046 682.046	1.2515 1.0827								.00003243		.760 .758
692 •046	.9381	.688	26.8693	268-415	10.8843	1.101	1.102	1.000	.00003278	-04423	.757
702.046	.8139	. 805	27.2683	270.311	10.9297	1.101	1.101	1.000	.00003342	.04571	755
712.046	.7071	•939	27.6689	272.199	10.9742	1.100	1.101	1.000	.00003375	. 04645	.753
722.046 732.046	•6152 5340	1.095	28.0712	274.078	11.0175	1.100	1.101	1.001	.00003407	• 04720	.751
742.046	•5360 •4676	1.481	28.8802	277.815	11.1012	1.099	1.100	1.001	.00003439 .00003471	. 04794	.750 .748
752.046	-4085	1.718	29.2869	279.676	11.1416	1.099	1.100	1.001	.00003503	.04943	.746
762.046	.3573	1.991	29.6950	281.532	11.1810	1.099	1.100	1.001	.00003534	.05017	.744
772.046	-3130	2.303	30.1045	283.386	11.2195	1.098	1.100	1.001	.00003566	.05092	.742
782.046 792.046	.2745 .2410	3.060	30.5154	285 • 239	11.2571	1.098	1.100	1.001	.00003597 .00003628	05166	.740
802.046	.2119	3.536	31.3411	288.946	11.3296	1.098	1.100	1.002	.00003659	-05315	.739 .737
812.046	-1866	4.068	31.7558	290.805	11.3646	1.097	1.100	1.002	.00003690	. 05390	.735
822.046	•1644	4.673	32.1717	292.669	11.3988	1.097	1.100	1.003	.00003720	.05465	.733
832.046	.1451								.00003751		.731
842.046 844.814	.1282 .1240	6.378	33.0071	296.050	11.4738	1.097	1.101	1.004	.00003781 .00003789	.05615	.729
01.1011	•12.10	C. 310	33.1231	270.350	11.4750	1.077	1.101	1.004	•00003189	• 05 6 5 6	•729
				S/!	R=39.75						
435.356	81.3926	.005	17.3325	214, 900	9,1254	1.122	1.122	1.000	00002343	02505	705
445.356			17.6686						.00002363		.785 .786
455.356			18.0086						.00002446		.787
465.356			18.3525		9.4450	1.118	1.118	1.000	.00002487	.02817	.788
475.356			18.7001		9.5444	1.117	1.117	1.000	.00002527	.02891	.788
485.356 495.356			19.0513 19.4058		9.0401 9.7210	1.116	1.116	1.000	.00002566	02965	•788 708
505.356			19.7637		9.8199	1.113	1.113	1.000	.00002645	.03113	.788 .788
515.356	19.3070	• 025	20.1247	232.702	9.9038	1.112	1.112	1.000	.00002683	.03187	.788
525.356			20.4888		9,9836	1.111	1.111	1.000	.00002721	.03261	.787
535.356 545.356		.036	20.8556	236.571	10.0592	1.110	1.110	1.000	.00002759	.03335	.786
555.356	9.8083	.053	21.5972	241.178	10.1973	1.109	1.109	1.000	.00002796 .00002833	. 03409	.785 .784
565.356	8.3182	•063	21.9716	243.261	10.2596	1.108	1.108	1.000	.00002870	. 03557	.782
575.356	7.0674	.076	22.3482	245.331	10.3173	1.107	1.107	1.000	.00002907	.03632	.780
585.356 595.364	6.0159	.091	22.7269	247.388	10.3702	1.107	1.107	1.000	.00002943	. 03 706	.778
595.356 605.356	5.1305 4.3837	. 108	23.4805	251.467	10.4614	1.106	1.106	1.000	.00002978	.03780	•776
2020370		+ + 4 - 7		2714701	10.4010	1.100	1.100	1.000	.00003014	• 05 854	.773

T	v	p	H/RT <sub>O</sub>	A	$c_p/R$	γ	G	z	, μ	k	$\mathtt{Np_r}$
				S/1	R=39.75						
615.356 625.356 635.356 645.356 655.356 675.356 675.356 705.356 715.356 725.356 745.356 745.356 745.356 745.356 855.356 805.356 805.356 815.356 825.356	3.7599 3.2246 2.7699 2.3830 2.0534 1.7720 1.5314 1.3255 1.1489 .9972 .8667 .5738 .5015 .5738 .5015 .4388 .3373 .2962 .2962 .2023 .1785	.181 .214 .253 .298 .350 .411 .482 .564 .660 .770 1.043 1.212 1.405 1.628 1.882 2.174 2.507 2.887 3.320 3.813 4.373	24.2528 24.6400 25.4200 25.4200 25.8127 26.6036 27.0015 27.4011 27.8024 28.2051 28.6095 29.0153 29.0153 30.2412 30.6526 31.4793 31.8945 32.3109 32.7285	255.480 257.452 259.411 261.357 263.290 267.120 269.018 270.906 272.785 274.655 276.517 280.220 282.063 283.901 285.737 287.571 289.405 291.240 293.C78	10.5522 10.6053 10.6053 10.7077 10.7573 10.8056 10.8529 10.8990 10.9441 11.0310 11.139 11.1538 11.12309 11.2680 11.3343 11.3343 11.3742 11.3742 11.4079 11.4408	1.105 1.104 1.103 1.103 1.102 1.102 1.101 1.100 1.009 1.099 1.098 1.098 1.098 1.098 1.098 1.098	1.105 1.104 1.103 1.103 1.102 1.102 1.101 1.101 1.100 1.100 1.100 1.100 1.100 1.099 1.099 1.099 1.099 1.099	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.001 1.001 1.001 1.001 1.001 1.002 1.002 1.002	.00003353 .00003385 .00003418 .00003450 .00003481	.04002 .04076 .04150 .04224 .04298 .04373 .04521 .04595 .04669 .04744 .04818 .04892 .04967 .05041 .05115 .05190 .05264 .05339 .05414 .05488 .05563	.770 .768 .766 .765 .761 .760 .758 .751 .753 .751 .749 .747 .745 .745 .740 .738 .734 .732 .732
044.014	•1503	4.713	73.1247		R=40.00		1.100	1.003	.00003700	.05054	• ( 2 )
458.831 468.831 498.831 508.831 518.831 528.831 538.831 558.831 568.831 608.831 618.831 628.831 648.831 648.831 658.831 658.831 668.831 678.831 678.831	81.4244 67.7473 56.4815 47.1711 33.0732 27.7660 23.3515 10.6047 14.0397 14.0397 14.0397 14.5882 62366 5.3323 4.5766 5.3323 4.5766 5.3323 4.5766 5.3325 1.8698 1.6191 1.4040 1.2192 1.06032	.006 .009 .009 .012 .014 .017 .021 .025 .030 .036 .044 .053 .063 .075 .090 .126 .149 .176 .245 .288 .339 .397 .464	20.9837 21.3542 21.7271 22.1023 22.4796 22.8589 23.2400 23.6227 24.0013 24.3872 24.7751 25.1648 25.5564 25.9469 26.3450 26.7419 27.5407 27.5407	217.957 220.262 222.507 224.732 226.938 229.126 231.295 233.448 237.705 239.811 241.902 243.980 246.045 248.097 250.138 252.168 254.180 256.161 258.127 260.080 262.019 263.946 267.763 269.654 271.535 273.406	9.2728 9.3781 9.4799 9.5780 9.6724 9.7629 9.8495 10.0103 10.0844 10.1541 10.2801 10.3362 10.4753 10.5169 10.5707 10.6232 10.6746 10.7249 10.8687 10.8687 10.9144 10.9591 11.0026	1.119 1.118 1.116 1.115 1.114 1.113 1.112 1.111 1.110 1.109 1.108 1.106 1.106 1.106 1.106 1.105 1.104 1.101 1.101 1.101 1.101 1.101	1.119 1.118 1.116 1.115 1.114 1.113 1.112 1.111 1.110 1.109 1.108 1.107 1.106 1.105 1.105 1.105 1.105 1.101 1.101 1.101 1.102 1.102 1.102 1.102 1.102 1.102	1.000 1.000	.00002619 .00002658 .00002734 .00002772 .00002809 .00002883 .00002919 .0000295 .00003026 .0000306 .00003164 .00003164 .00003298 .00003298 .00003298 .00003298 .00003298	. 02 769 . 02 843 . 02 991 . 03 065 . 03 1 39 . 03 287 . 03 361 . 03 435 . 03 509 . 03 587 . 03 731 . 03 805 . 03 805 . 03 805 . 03 805 . 03 805 . 04 102 . 04 102	
728.831 738.831 748.831 758.831 768.831 778.831 808.831 818.831 828.831 838.831 844.814	. 9232 .8049 .7028 .6144 .5378 .4714 .4136 .3634 .3197 .2816 .2484 .2193 .2037	.856 .994 1.152 1.334 1.542 1.780 2.C52 2.362 2.715 3.117 3.574	28.7507 29.1571 29.5649 29.9741 30.3847 30.7566 31.2098 31.6242 32.0400 32.4569 32.8749	277.120 278.964 280.802 282.633 284.459 286.280 288.099 289.915 291.730 293.546 295.364	11.0867 11.1272 11.1668 11.2053 11.2430 11.2797 11.3155 11.3504 11.3845 11.4177 11.4501	1.099 1.099 1.099 1.098 1.098 1.097 1.097 1.097	1.100 1.099 1.099 1.099 1.099 1.099 1.099 1.099 1.099	1.000 1.001 1.001 1.001 1.001 1.001 1.001 1.002 1.002	.00003428 .00003460 .00003 492 .00003555 .00003556 .00003617 .00003648 .00003709 .00003709	. 04843 . 04918 . 04992 . 05066 . 05141 . 05215 . 05289 . 05364 . 05438 . 05513	.750 .748 .746 .745 .743 .741 .739 .737 .735 .733 .732 .730

T	v	p	H/RT <sub>O</sub>	A	$c_p/R$	γ	G	$\mathbf{z}$	μ	k	$N_{\mathbf{Pr}}$	
\$/R=40•25												
472.476 482.476 492.476 502.476 512.476 522.476 532.476 542.476	81.4244 67.9129 56.7532 47.5102 39.8420 33.4700 28.1668 23.7459 20.0548 16.9679 14.3824	.006 .008 .010 .012 .014 .017 .021 .025	21.4899	223.321 225.539 227.737 229.918 232.082 234.228 236.359 238.474 240.574	9.5161 9.6129 9.7058 9.7949 9.8800 9.9610 10.0378 10.1103	1.117 1.116 1.115 1.114 1.113 1.112 1.111 1.110	1.117 1.116 1.115 1.114 1.113 1.112 1.111 1.110	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	.00002633 .00002672 .00002710 .00002748	.02870 .02944 .03018 .03092 .03166 .03240 .03314 .03388 .03462	.787 .788 .788 .788 .788 .788 .787 .786 .785 .784	
572.476	12.2132 10.3904 8.8562 7.5628 6.4706 5.5571 4.7712 4.1029 3.5337 3.0480	.044 .C52 .062 .074 .C88 .104 .124 .146 .172	22.2396 22.6177 22.9977 23.3794 23.7626 24.1418 24.5285 24.9170 25.3075 25.6998	244.733 246.793 248.641 250.877 252.902 254.900 256.875 258.835 260.781 262.715	10.3010 10.3553 10.4049 10.4495 10.5365 10.5368 10.6420 10.6929 10.7427	1.107 1.106 1.106 1.105 1.105 1.105 1.104 1.104 1.103	1.107 1.107 1.106 1.106 1.105 1.105 1.104 1.104 1.103 1.103	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	.00002896 .00002932 .00002968 .00003004 .00003074 .00003108 .00003177 .00003211	.03610 .03684 .03758 .03832 .03906 .03981 .04055 .04129	.781 .779 .776 .774 .771 .769 .767 .765	
672.476 682.476 692.476 702.476 712.476 722.476 732.476 752.476 762.476	2.6330 2.2778 1.9734 1.7121 1.4874 1.2940 1.1273 .9834 .8589 .7512	.238 .279 .327 .383 .447 .521 .606 .704	26.0938 26.4897 26.8872 27.2864 27.6872 28.0896 28.4936 28.8990 29.3060	264.635 266.543 268.439 270.323 272.197 274.060 275.914 277.758 279.594	10.7913 10.8388 10.8852 10.9305 10.9747 11.0179 11.0600 11.1011 11.1412	1.102 1.101 1.101 1.100 1.100 1.009 1.099 1.099	1.102 1.101 1.101 1.101 1.100 1.100 1.100 1.099	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	.00003244 .00003277 .00003310 .00003343	.04351 .04425 .C4499 .04573 .04648 .04722 .04796 .04870	.760 .758 .757 .755 .753 .751 .749 .748	
772.476 782.476 792.476 802.476 812.476 822.476 832.476 842.476 844.814	.6578 .5768 .5063 .4451 .3917 .3451 .3044 .2689 .2612	1.096 1.266 1.460 1.683 1.936 2.225 2.553 2.526	30.1241 30.5352 30.9476 31.3614 31.7763 32.1925 32.6099 33.0285	283.243 285.057 286.866 288.670 290.471 292.269 294.067 295.864	11.2185 11.2557 11.2919 11.3273 11.3618 11.3955 11.4283 11.4602	1.098 1.098 1.097 1.097 1.097 1.096	1.099 1.098 1.098 1.098 1.098 1.098 1.098	1.001 1.001 1.001 1.001 1.001 1.001 1.002	.00003566 .00003597 .00003628 .00003658 .00003719 .00003749 .00003779 .00003786	.05093 .05167 .05241 .05316 .05390 .05465 .05539	.742 .740 .738 .736 .735 .733 .731 .729	
				\$/1	R=40.50							
	81.4244 68.0819 57.0311 47.8582 40.2312 33.8795 28.5814 24.1552 20.4514 17.3471 14.7411 12.5499 10.7045 9.1478 7.8474 6.7309 5.7824	.007 .008 .010 .012 .014 .017 .021 .025 .030 .036 .044 .052 .062 .073 .087	21.2602 21.6325 22.0072 22.3840 22.7628 23.1435 23.5258 23.9040 24.2895	226.381 228.573 230.747 232.904 235.644 237.169 239.278 241.373 243.454 245.521 247.576 249.619 251.650	9.6488 9.7403 9.8279 9.9114 9.9908 10.0660 10.1368 10.2032 10.3253 10.3748 10.4651 10.5029 10.5570	1.116 1.114 1.113 1.112 1.111 1.110 1.109 1.109 1.107 1.107 1.106 1.106 1.105	1.116 1.114 1.113 1.112 1.111 1.109 1.109 1.107 1.107 1.107 1.106 1.105 1.105	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	.00002687 .00002725 .00002763 .00002800 .00002837	.02972 .03046 .03120 .03194 .03268 .03342 .03416 .03490 .03564 .03638 .03713 .03787	.788 .788 .788 .788 .787 .786 .785 .783 .782 .775 .773 .775 .773 .776 .768	

T V	p H/RT <sub>O</sub>	A	$c_{\mathbf{p}}/\mathbf{R}$	γ	G	Z	μ	. k	$N_{\mathbf{Pr}}$				
	S/R=40.50												
646.299 4.9754 656.299 4.2875 666.299 3.1083 686.299 2.7683 696.299 2.3829 716.299 1.8105 726.299 1.5759 736.299 1.3735 746.299 1.1987 756.299 1.0475 766.299 7043 796.299 8029 786.299 7043 799.299 6185 806.299 4788 826.299 4788 826.299 4788 826.299 3724 844.814 3351	1.591 31.9359 1.827 32.3526 2.096 32.7705	261.516 263.443 265.357 267.259 269.148 271.026 272.893 274.749 276.596 278.432 280.260 282.C79 283.890 285.695 287.492 289.285 291.072	10.7120 10.7613 10.8095 10.8565 10.9025 10.9473 11.0338 11.0755 11.1162 11.1558 11.1945 11.3049 11.3049 11.3338 11.3739 11.471 11.435	1.103 1.102 1.102 1.101 1.101 1.100 1.100 1.009 1.099 1.099 1.098 1.097 1.097 1.097	1.103 1.103 1.102 1.102 1.101 1.100 1.100 1.100 1.099 1.099 1.099 1.098 1.098 1.098 1.098 1.098	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.001 1.001 1.001 1.001	.00003190 .00003223 .00003257 .00003290 .00003323 .00003388 .00003420 .00003452 .00003515 .00003517 .00003578 .00003679 .00003679 .00003639 .00003700 .00003700	.04231 .04305 .04379 .04453 .04527 .04602 .04676 .04750 .04824 .04828 .04972 .05047 .05121 .05121 .05195 .05269 .05344 .05418 .05418	.765 .763 .761 .759 .758 .754 .752 .751 .747 .745 .743 .739 .738 .736 .736 .730 .728				
844.814 .3351 2.353 33.1272 296.152 11.4664 1.096 1.097 1.001 .00003786 .05630 .728 S/R=40.75													
490.309 81.4244 500.309 68.2543 510.309 57.3156 520.309 48.2155 530.309 40.6321 540.309 34.3026 550.309 29.0113 560.309 24.58C7 570.309 20.8650 580.309 17.7436 590.309 12.9042 610.309 11.0360 620.309 6.0181 640.309 6.9900 650.309 6.0181 660.309 3.3562 700.309 4.4811 680.309 3.3562 700.309 2.9108 710.309 2.5280 720.309 2.1986 730.309 1.9146 740.309 1.9146 740.309 1.6696 750.309 1.9146 740.309 1.6696 750.309 1.9157 770.309 1.9157 770.309 1.9157 770.309 1.9157 770.309 1.9157 770.309 1.9166 750.309 779 790.309 8581 800.309 .9779 790.309 8581 800.309 5841 830.309 5841	.006 19.2265 .007 19.5828 .008 19.9422 .010 20.3047 .012 20.6702 .015 21.0384 .018 21.4C92 .021 21.7825 .025 22.1581 .030 22.5357 .036 22.9153 .043 23.2967 .052 23.6796 .061 24.0584 .C72 24.4447 .085 24.8329 .101 25.2229 .119 25.6148 .139 26.0C86 .164 26.4040 .192 26.8012 .224 27.2001 .262 27.6006 .306 28.4064 .144 28.816 .480 29.2182 .556 25.6264 .414 28.816 .480 29.2182 .556 25.6264 .414 28.816 .480 29.2182 .556 25.6264 .414 28.816 .480 29.2182 .556 25.6264 .414 28.816 .480 29.2182 .556 25.6264 .414 28.816 .480 29.2182 .556 28.4064 .414 28.816 .480 29.2182 .556 28.4064 .414 28.816 .480 29.2182 .556 28.4064 .414 28.816 .480 29.2182 .556 28.4064 .414 28.816 .480 29.2182 .556 28.4064 .414 28.816 .480 29.2182 .556 28.4064 .414 28.816 .480 29.2182 .556 28.4064 .414 28.816 .480 29.2182 .556 28.4064 .414 28.816 .480 29.2182 .556 28.4064 .414 28.816 .480 29.2182 .556 28.4064 .414 28.816 .480 29.2182 .556 28.4064 .414 28.816	229.447 231.614 233.764 235.898 238.016 240.119 242.208 244.284 246.346 250.433 252.460 254.465 256.442 262.286 264.206 264.206 264.206 264.206 264.206 264.206 262.386 264.206 263.371 277.313 279.142 280.562 282.773 284.576 286.371 288.159 289.941 291.717 289.941 291.717 289.941 291.717	9.7759 9.8619 9.9438 10.0215 10.0949 10.1640 10.2286 10.3439 10.3944 10.5782 10.6306 10.6306 10.6306 10.7318 10.7318 10.8283 10.8283 10.8283 10.8283 10.9204 11.0504 11.0504 11.0504 11.1319 11.1319 11.2466 11.2830 11.3184 11.3529 11.3184 11.3529	1.114 1.113 1.112 1.110 1.109 1.108 1.106 1.106 1.105	1.114 1.113 1.112 1.110 1.108 1.108 1.106 1.106 1.105 1.105 1.104 1.105 1.104 1.103 1.102 1.101 1.101 1.101 1.101 1.101 1.101 1.101 1.101 1.101 1.109 1.099 1.099 1.098	1.000 1.000	.0002778 .0002815 .00002818 .00002924 .0000296 .00003031 .00003101 .00003135 .0003169 .00003270 .0003270 .0003333 .00003401 .0003401 .0003403 .0003401 .0003528 .0003528 .0003559 .0003682 .0003682 .0003682 .0003682	.03076 .03176 .03150 .03224 .03298 .03372 .03446 .03520 .03564 .03742 .03816 .03742 .03890 .04033 .04113 .04261 .04335 .04409 .04409 .04409 .044557 .04409 .044557 .04631 .04775 .04779 .04854 .04928 .05076 .050224 .05299 .05373 .05447	. 788 . 788 . 788 . 787 . 786 . 787 . 778 . 777 . 771 . 769 . 760 . 769 . 755 . 755 . 755 . 755 . 755 . 755 . 744 . 744 . 744 . 744 . 743 . 744 . 743 . 744 . 743 . 744 . 744				

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T	v	p	H/RT <sub>o</sub>	A	c <sub>p</sub> /R	γ	G	Z	μ	k	$N_{\mathbf{Pr}}$	
S/R=41.00												
514.516 524.516 534.516	81.4244 68.4298 57.6069 48.5828 41.0458	.008 .010	19.7336 20.0944 20.4581 20.8248 21.1941	232.520 234.663 236.791	9.8968 9.9770 10.0529	1.112 1.111 1.110	1.112 1.111 1.110	1.000 1.000 1.000	.00002641 .00002680 .00002718 .00002756 .00002793	.03181 .03255 .03329	.788 .788 .787 .786	
554.516 564.516 574.516 584.516 594.516	34.7407 29.4577 25.0240 21.2971 18.1592 15.5130	.015 .018 .021 .026 .031	21.5660 21.9402 22.3167 22.6952 23.0755	240.999 243.082 245.152 247.209 249.253	10.1917 10.2544 10.3124 10.3657 10.4142	1.109 1.108 1.107 1.107	1.109 1.108 1.107 1.107	1.000 1.000 1.000 1.000	.00002830 .00002867 .00002904 .00002940 .00002975	.03477 .03551 .03625 .03699 .03773	.784 .782 .780 .778 .776	
614.516 624.516 634.516 644.516 654.516	13.2778 11.4070 9.7967 8.4270 7.2599 6.2638	.043 .051 .060 .071	23.8411 24.2207 24.6078 24.9968 25.3876	253.308 255.297 257.267 259.222 261.163	10.4964 10.5473 10.6004 10.6522 10.7029	1.105 1.105 1.104 1.104 1.103	1.105 1.105 1.104 1.104 1.103	1.000 1.000 1.000 1.000	.00003046 .00003081 .00003115 .00003150	.03921 .03996 .C4070 .04144 .04218	.770 .768 .767 .765	
664.516 674.516 684.516 694.516 704.516 714.516	5.4124 4.6835 4.0586 3.5220 3.0605	.116 .136 .160 .197 .218	26.1748 26.5710 26.9689 27.3685 27.7697	265.005 266.907 268.796 270.673 272.538	10.8007 10.8480 10.8941 10.9391 10.9830	1.102 1.102 1.101 1.101 1.100	1.102 1.102 1.101 1.101 1.100	1.000 1.000 1.000 1.000	.00003217 .00003251 .00003284 .00003317 .00003350 .00003382	.04366 .04440 .04514 .04588 .04662	.761 .760 .758 .756 .754	
724.516 734.516 744.516 754.516 764.516 774.516	2.6632 2.3205 2.0245 1.7686 1.5471 1.3549	.254 .295 .343 .398	28.1725 28.5768 28.9826 25.3899 29.7987	274.391 276.234 278.067 279.889 281.701	11.0259 11.0677 11.1085 11.1482 11.1870	1.100 1.099 1.099 1.099	1.100 1.099 1.099 1.099	1.000 1.000 1.000 1.000	.00003414 .00003446 .00003478 .00003509 .00003541	.04736 .04810 .04885 .04959 .05033	.751 .749 .747 .745 .744	
784.516 794.516 804.516 814.516 824.516	1.1882 1.0432 .9170 .8070	.616 .710 .818 .942 1.682	30.6203 31.0330 31.4471 31.8625 32.2790	285.300 287.086 288.865 290.637 292.403	11.2617 11.2976 11.3326 11.3667 11.3999	1.098 1.097 1.097 1.097	1.098 1.098 1.097 1.097	1.000 1.000 1.000 1.001	.00003603 .00003633 .00003664 .00003694 .00003724	.05181 .05255 .05330 .05404	.740 .738 .736 .734	
834.516 844.516 644.814	.6273 .5540 .5518	1.423	33.1157	295.918 295.970	11.4637	1.096	1.097	1.001	.00003754 .00003784 .00003785	.05627	.730 .728 .728	
518.929	81 4244	006	20,2545	233 660	0 0227	1 112	1 112	1 000	00003407	03317	707	
528.929 538.929 548.929 558.929 568.929	68.6084 57.9055 48.9611 41.4732 35.1948	.007 .009 .010 .013	20.6196 20.9874 21.3579 21.7309 22.1061	235.604 237.724 239.829 241.920 243.997	10.0110 10.0850 10.1547 10.2199 10.2805	1.111 1.110 1.109 1.108 1.108	1.111 1.110 1.109 1.108 1.108	1.000 1.000 1.000 1.000	.00002697 .00002735 .00002772 .00002810 .00002847 .00002883	.03288 .03362 .03436 .03510	.787 .787 .786 .785 .783	
588.929 598.929 608.929 618.929 628.929	21.7495 18.5957 15.9600 13.6948	.022 .026 .031 .036	22.8628 23.2440 23.6267 24.0053 24.3913	248.112 250.151 252.178 254.188 256.166	10.3877 10.4340 10.4754 10.5171 10.5708	1.106 1.106 1.105 1.105 1.104	1.106 1.106 1.105 1.105 1.104	1.000 1.000 1.000 1.000	.00002919 .00002955 .00002991 .00003026 .00003061	.03732 .03806 .03880 .03954 .04028	.779 .777 .775 .772 .769	
638.929 648.929 658.929 668.929 678.929 688.929	10.1310 8.7337 7.5403 6.5195 5.6451	.060 .C70 .083 .097	25.1691 25.5607 25.9542 26.3495 26.7465	260.078 262.013 263.934 265.842 267.737	10.6747 10.7248 10.7738 10.8216 10.8684	1.103 1.103 1.102 1.102	1.103 1.103 1.102 1.102	1.000 1.000 1.000 1.000	.00003131 .00003165 .00003199 .00003232 .00003265	.04176 .04250 .04324 .04399	.766 .764 .762 .761 .759	
698.929 708.929 718.929 728.929 738.929 748.929	4.8948 4.2502 3.6955 3.2176 2.8051 2.4488	.133 .156 .181 .211 .246	27.1451 27.5454 27.9474 28.3508 28.7558 29.1623	269.619 271.490 273.349 275.196 277.032 278.858	10.9140 10.9585 11.0019 11.0443 11.0856 11.1259	1.101 1.100 1.100 1.100 1.099 1.099	1.101 1.100 1.100 1.100 1.099 1.099	1.000 1.000 1.000 1.000 1.000	.00003331 .00003364 .00003396 .00003428 .00003460	.04547 .04621 .04695 .04769 .04843	.755 .754 .752 .750 .748	
758.929 768.929 778.929 788.929 798.929 808.929	2.1404 1.8732 1.6415 1.4402 1.2651 1.1126	.383 .443 .511 .589	29.9797 30.3904 30.8025 31.2159 31.6305	282.479 284.275 286.C62 287.841 289.612	11.2036 11.2409 11.2773 11.3128 11.3473	1.098 1.098 1.097 1.097	1.098 1.098 1.098 1.097	1.000 1.000 1.000 1.000	.00003523 .00003554 .00003585 .00003616 .00003647	.05065 .05140 .05214 .05288	.745 .743 .741 .739 .737	
818.929 828.929 838.929 844.814	.9796 .8636 .7621 .7085	.780 .895 1.027	32.0464 32.4635 32.8818	291.375 293.131 294.881	11.3810 11.4138 11.4457	1.096 1.096 1.096	1.097 1.097	1.000 1.001 1.001	.00003707 .00003737 .00003767 .00003785	.05436 .05510	.733 .731 .729	

T V	p H/RI	o A	$c_p/R$	γ	G	Z	$\mu$	k	$N_{Pr}$
		s/	R=41.50						
533.562 81.4244 543.562 68.7874 553.562 58.2096 563.562 49.3491 573.562 41.9146 583.562 30.4046 603.562 25.9693 613.562 12.1433 643.562 12.1433 643.562 12.1433 643.562 12.1433 643.562 67.846 703.562 7.8304 693.562 67.846 703.562 5.8866 713.562 7.8304 733.562 3.8767 743.562 3.3818 753.562 1.9834 773.562 2.5834 773.562 2.5834 773.562 1.9834 773.562 1.9834 773.562 1.9834 773.562 1.5308 813.562 1.3468 823.562 1.3468		88 238.701 040.800 45 242.884 07 244.954 91 247.012 91 251.091 46 253.113 40 255.106 09 257.074 09 257.074 10 268.606 11 272.346 42 274.195 84 276.032 16 272.346 17 278.885 18 279.888 19 283.296 11 285.085 10 288.636 11 285.085 10 288.636 11 279.688 11 279.688 11 279.688 11 279.688 11 279.688 11 279.688 11 279.688 11 279.688	10.1178 10.1854 10.2485 10.3070 10.3608 10.4928 10.4928 10.5421 10.5953 10.6472 10.6980 10.7476 10.9346 10.9346 10.9346 11.0634 11.1043 11.1043 11.1208 11.2577 11.2936 11.3627 11.3627 11.3627	1.110 1.109 1.108 1.107 1.106 1.105 1.105 1.105 1.103 1.103 1.103 1.101 1.101 1.101 1.100 1.099 1.099 1.098 1.097 1.097 1.097	1.110 1.109 1.107 1.106 1.106 1.105 1.105 1.104 1.103 1.102 1.101 1.101 1.100 1.100 1.009 1.099 1.099 1.099 1.099 1.097 1.097 1.097	1.000 1.000	.0002790 .0002864 .00002936 .00002936 .00002972 .00003007 .00003146 .00003146 .00003248 .00003214 .00003441 .00003441 .00003441 .00003441 .00003506 .0003506 .0003506 .0003506 .0003560	.03396 .03470 .03544 .03618 .03692 .03766 .03914 .03914 .03988 .04062 .04137 .04211 .04285 .04359 .04433 .04507 .04581 .04655 .04729 .04803 .04877 .04951 .05026 .051104 .05174 .05248 .05396	.786 .785 .784 .782 .780 .776 .773 .771 .765 .765 .765 .755 .755 .755 .755 .755
833.562 1.0461 843.562 .9237	743 32.65 852 33.07	74 293.902 63 295.642	11.4283 11.4598	1.096	1.096 1.096	1.000	.00003751	.05545 .05619	.732 .730 .728 .728
844.814 .9094			R=41.75	1.070	1.070	1.001	.00003764	• 0 0 0 2 5	• 720
548.424 81.4244 558.424 68.9734 568.424 58.5253 578.424 49.7524 588.424 42.3734 598.424 36.1557	.008 21.71 .009 22.08 .011 22.46 .013 22.84 .015 23.22	20 241.814 71 243.892 44 245.956 37 248.007 47 250.047	10.2167 10.2775 10.3338 10.3852 10.4318	1.108 1.108 1.107 1.106 1.106	1.108 1.108 1.107 1.106 1.106	1.000 1.000 1.000 1.000	.00002845 .00002881 .00002918 .00002954 .00002989	.03506 .03580 .03654 .03728 .03802	.785 .783 .781 .779 .777 .775
608.424 30.9106 618.424 26.5268 628.424 22.7599 638.424 19.5590 648.424 16.8343 658.424 14.5112 668.424 12.5273 678.424 10.8336	022 23.98 026 24.37 030 24.75 036 25.14 042 25.54 050 25.93	60 254.086 18 256.065 97 258.028 94 259.977 10 261.912 44 263.833 96 265.740	10.5143 10.5681 10.6207 10.6720 10.7222 10.7713 10.8191	1.105 1.104 1.103 1.103 1.102 1.102	1.105 1.104 1.103 1.103 1.102 1.102	1.000 1.000 1.000 1.000 1.000 1.000	.00003060 .00003094 .00003129 .00003163 .00003197 .00003230	. 03 9 5 0 . 04 0 2 4 . 04 0 9 8 . 04 1 7 3 . 04 2 4 7 . 04 3 2 1 . 04 3 9 5	.769 .768 .766 .764 .763 .761
688.424 9.3771 698.424 8.1302 708.424 7.0585 718.424 6.1371 728.424 5.3425 738.424 4.6577 748.424 4.0656 758.424 3.5533	080 27.12 094 27.52 109 27.92 127 28.33 148 28.73 172 29.14	51 269.516 53 271.386 72 273.243 06 275.089 56 276.923 20 278.746	10.9115 10.9561 10.9996 11.0420 11.0833	1.101 1.100 1.100 1.100 1.099 1.099	1.101 1.100 1.100 1.100 1.099 1.099	1.000 1.000 1.000 1.000 1.000	.00003330 .00003362 .00003395 .00003427 .00003459	.04543 .04617 .04691 .04765 .04839 .04913	.757 .756 .754 .752 .750 .748 .746
768.424 3.1095 778.424 2.7245 788.424 2.3901 798.424 2.0993 808.424 1.8466 818.424 1.6253 828.424 1.4325 838.424 1.2641 844.814 1.1678	230 29.95 .266 3C.36 .308 30.78 .355 31.19 .408 31.60 .470 32.02 .539 32.44 .619 32.86	92 282.361 99 284.153 19 285.935 53 287.708 99 289.472 58 291.228 28 292.975 11 294.714	11.2013 11.2387 11.2751 11.3106 11.3451 11.3787 11.4115	1.098 1.098 1.097 1.097 1.096 1.096	1.098 1.098 1.098 1.097 1.097 1.096 1.096	1.000 1.000 1.000 1.000 1.000 1.000	.00003553 .00003584 .00003614 .00003645 .00003675 .00003706 .00003765	.05061 .05136 .05210 .05284 .05358 .05432 .05506	.743 .741 .739 .737 .735 .733 .731 .729

T	V	p	H/RT <sub>O</sub>	A	$c_p/R$	γ	G	${f z}$	μ	k	$N_{\mathbf{Pr}}$
				S/F	R=42.00						
	50.1708 42.8514 36.6698 31.4978 27.0468 23.2614 20.0365 17.2847 14.9328 12.9197	.CC8 .009 .011 .013 .016 .018 .022 .026 .030 .036 .042 .049	22.2795 22.6578 23.0380 23.4199 23.8033 24.1828 24.5696 24.9585 25.3491 25.7417 26.1360 26.5321 26.9298 27.3293	244.947 247.005 249.050 251.683 253.106 255.098 257.068 259.024 260.965 262.893 264.806 266.707 268.594 270.469	10.3068 10.3606 10.4096 10.4536 10.4927 10.5419 10.5951 10.6470 10.6978 10.7474 10.7958 10.8431 10.8893 10.9344	1.107 1.107 1.106 1.105 1.105 1.105 1.104 1.103 1.103 1.103 1.102 1.101	1.107 1.107 1.106 1.105 1.105 1.105 1.104 1.103 1.103 1.103 1.102 1.101	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	.00002863 .00002900 .00002936 .00002972 .00003007 .00003042 .00003112 .00003146 .00003214 .00003247 .00003281 .00003314 .000033314 .00003346	.03618 .03692 .03766 .03840 .03914 .03988 .04062 .04136 .04210 .04284 .04358 .04433 .04507 .04581	.782 .780 .778 .773 .771 .768 .767 .763 .763 .760 .758 .755
723.530 733.530 743.530 753.530 763.530 773.530 783.530 803.530 813.530 823.530 833.530 844.814	7.3416 6.3958 5.5791 4.8731 4.2618 3.7318 3.2718 2.8719 2.5240 2.2208 1.9563 1.7253 1.5233	.092 .107 .124 .144 .167 .193 .223 .258 .297 .342 .393 .451	28.1330 28.5372 28.9430 29.3502 29.7588 30.1688 30.9829 31.4069 31.8222 32.2387 32.6564 33.0753	274.183 276.022 277.849 279.666 281.472 283.267 285.052 286.828 288.594 290.351 292.099 293.839 295.571	11.0213 11.0631 11.1040 11.1438 11.1826 11.2573 11.2932 11.3281 11.3622 11.3953 11.4570	1.100 1.099 1.099 1.098 1.098 1.097 1.097 1.097 1.096 1.096	1.100 1.099 1.099 1.098 1.098 1.097 1.097 1.097 1.096 1.096	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	00003411 00003443 00003506 00003537 00003569 00003569 00003691 00003691 00003721 00003784	.04729 .04803 .04877 .04951 .05025 .05099 .05173 .05247 .05396 .05470 .05544 .05618	. 751 . 749 . 747 . 746 . 744 . 742 . 738 . 736 . 734 . 732 . 730 . 728
				S/F	₹=42•25						
588.899 598.899 608.899 618.899 628.899 638.899 648.899 658.899 678.899 688.899	59.1861 50.6033 43.4303 37.2658 32.0270 27.5673 23.7647 20.5171 17.7393 15.3596 13.3180	. CO8 . CO9 . O11 . O13 . O16 . C19 . O22 . O26 . O30 . O36 . O42 . C49 . O57 . O78 . O90 . 105 . 122 . 141 . 163 . 188 . 217 . 249 . 287 . 378	22.8618 23.2429 23.6256 24.0043 24.3903 25.1680 25.5597 25.9532 26.3485 27.1441 27.5445 27.9464 28.3499 28.7549 29.5694 29.9788 30.8917 31.6298 32.0458 32.4629 32.8813	248.104 250.143 252.170 254.180 256.157 258.119 260.067 262.001 263.921 267.720 269.600 271.468 277.000 278.821 280.630 282.430 282.430 284.218 285.997 287.766 289.525 291.275 293.016	10.3875 10.4339 10.4752 10.5168 10.5706 10.6231 10.6744 10.7735 10.8213 10.8581 11.0851 11.0851 11.0851 11.1254 11.2402 11.2402 11.2402 11.2765 11.3464 11.3799 11.4126 11.4444	1.106 1.105 1.105 1.105 1.103 1.103 1.102 1.102 1.101 1.101 1.101 1.100 1.099 1.099 1.098 1.098 1.097 1.097 1.097	1.106 1.105 1.105 1.104 1.103 1.103 1.102 1.101 1.101 1.101 1.100 1.100 1.099 1.099 1.098 1.097 1.097 1.097	1.000 1.000	.00002919 .00002955 .00002991 .00003061 .00003066 .00003198 .00003198 .00003292 .00003298 .00003298 .00003394 .00003492 .00003492 .00003554 .00003554 .00003616 .00003677 .00003707	.03732 .03806 .03880 .03954 .04028 .04102 .04176 .04250 .04324 .04398 .04472 .04546 .04620 .04694 .04791 .05065 .05133 .05213 .05213 .05361 .05435 .05509 .05584	.779 .777 .775 .7769 .7668 .7664 .7652 .7557 .7555 .7554 .7550 .748 .7445 .7443 .7411 .7337 .7337 .7331 .7329 .728

T	<b>v</b>	p	H/RT <sub>O</sub>	A	cp/R	γ	G	z	$\mu$	k	$Np_r$
				\$/	R=42.50						
604.548 614.548 624.548 634.548 644.548 664.548 664.548 674.548 694.548 704.548 714.548	28.0833 24.2656 20.9974 18.1951 15.7890	.008 .010 .011 .013 .C16 .019 .C22 .026 .030 .036 .C42 .049 .057 .066 .C77 .C89 .103 .119 .137 .159 .183 .210	23.4589 23.8425 24.221 24.6092 25.3890 25.7818 26.1763 26.5725 27.3701 27.7713 28.1742 28.5785 28.9844 29.8006 30.6223 31.0351 31.4493 31.8647 32.6992	251.289 253.310 255.298 257.267 259.221 261.160 263.086 264.998 266.897 270.655 272.516 274.364 276.364 276.364 278.026 281.643 283.435 285.217 286.589 288.751 290.503 290.503	10.4578 10.4964 10.5473 10.6004 10.6522 10.7028 10.8006 10.8478 10.8939 10.9388 10.9388 10.9388 11.0672 11.1672 11.1476 11.12608 11.2240 11.2608 11.3314 11.3653 11.3984 11.4305	1.106 1.105 1.105 1.104 1.102 1.102 1.102 1.101 1.101 1.101 1.101 1.109 1.099 1.099 1.098 1.098 1.097 1.097 1.096 1.096	1.106 1.105 1.105 1.104 1.102 1.102 1.102 1.101 1.101 1.101 1.100 1.099 1.099 1.098 1.098 1.098 1.097 1.097	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	.0002975 .0003011 .00003081 .00003155 .00003157 .00003251 .00003251 .00003251 .00003350 .00003414 .00003446 .00003446 .00003572 .00003504 .00003604 .00003604 .00003754 .00003754 .00003754	.03848 .03922 .03996 .04070 .04144 .04218 .04292 .C4366 .04450 .04514 .04588 .04662 .04736 .04810 .04884 .05033 .05107 .05181 .05255 .05329 .05403 .05551	.776 .773 .770 .768 .767 .766 .766 .756 .756 .754 .753 .751 .749 .747 .743 .742 .740 .736 .734 .732 .732
844.814	2 • 4715								.00003784		•728
				\$/1	R=42.75						
620.517 630.517 640.517 650.517 660.517 670.517 700.517 710.517 720.517 730.517	44.3820 38.2691 33.0472 28.5795 24.7512 21.4660 18.6425 16.2125 14.1181	.008 .010 .012 .014 .016 .026 .030 .036 .041 .048 .055 .075 .087 .101 .117 .134 .155 .178 .234	24.0666 24.4529 24.8411 25.2313 25.6233 26.0170 26.8099 27.2088 27.6094 28.0116 28.4154 28.8207 29.2274 29.6357 30.4563 30.4563 30.8683 31.6872 32.1133 32.5307 32.9492	254.500 256.474 258.434 260.380 262.311 264.228 268.022 269.900 271.765 273.618 275.459 277.289 279.107 280.914 282.709 284.495 286.270 284.495 289.790 291.535 293.272	10.5256 10.5791 10.6826 10.7325 10.8754 10.8754 10.9208 10.9651 11.0916 11.1317 11.1708 11.2460 11.2822 11.3174 11.3517 11.3517 11.3851 11.4475	1.105 1.104 1.103 1.103 1.102 1.101 1.101 1.100 1.099 1.099 1.098 1.098 1.098 1.097 1.097 1.097	1.105 1.104 1.103 1.103 1.102 1.102 1.101 1.100 1.099 1.099 1.098 1.098 1.098 1.097 1.097 1.097	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	.00003032 .00003102 .00003170 .00003170 .00003204 .00003271 .00003204 .00003304 .00003401 .00003401 .00003401 .00003401 .00003401 .00003528 .00003528 .00003590 .00003691 .00003691 .00003691 .00003712 .00003712	.03966 .04040 .04114 .04188 .04262 .04336 .04410 .04484 .04558 .04632 .04706 .04780 .04855 .04929 .05003 .05077 .05151 .052299 .05373 .05547 .05521	.771 .769 .767 .766 .762 .769 .757 .755 .755 .755 .750 .748 .744 .744 .744 .743 .735 .731 .735 .731
				S/F	R=43.00						
626.870 636.870 646.870 656.870 666.870 676.870 686.870	69.9437 60.1840 51.8662 44.7648 38.6924	.008 .010 .012 .014	24.6994 25.0888 25.4801 25.8733 26.2682	257.721 259.671 261.608 263.530 265.438	10.6125 10.6640 10.7144 10.7636 10.8117	1.104 1.103 1.103 1.102 1.102	1.104 1.103 1.103 1.102 1.102	1.000 1.000 1.000 1.000	.00003089 .00003123 .00003158 .00003192 .00003225 .00003259 .00003292	.04087 .04161 .04235 .04309 .04383	.768 .766 .765 .763 .761 .759

TABLE I.- THERMODYNAMIC PROPERTIES OF  $CF_4$  AT CONSTANT ENTROPY — Continued

T	v	p	H/RTo	A	c <sub>p</sub> /R	γ	G	${f z}$	μ	k	$Np_{\mathbf{r}}$
				S/F	R=43.00						
696.870 716.870 726.870 726.870 746.870 756.870 766.870 776.870 786.870 786.870 806.870 816.870 826.870 826.870 836.370	25.2005	.026 .031 .036 .041 .048 .056 .064 .075 .086 .099 .114 .132	27.4632 27.8648 28.2680 28.6727 29.0790 29.4867 29.8958 30.3063 30.7181 31.1313 31.5458 31.9615 32.3784 32.7965	271.086 272.943 274.788 276.621 278.443 280.253 282.052 283.641 287.387 289.145 290.893 292.631 294.360	10.9491 10.9927 11.0352 11.0767 11.1172 11.1566 11.1951 11.2325 11.2690 11.3046 11.3392 11.3729 11.4376	1.100 1.100 1.100 1.099 1.099 1.098 1.098 1.097 1.097 1.097	1.100 1.100 1.100 1.099 1.099 1.098 1.098 1.097 1.097 1.097 1.096 1.096	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	.00003325 .00003357 .00003454 .00003454 .00003517 .0000357 .00003670 .00003670 .00003701 .00003701	.04605 .04679 .04753 .04827 .04902 .05950 .05124 .05198 .05272 .05346 .05420 .05568	.756 .754 .752 .750 .749 .747 .743 .741 .739 .737 .735 .734 .732
				\$/1	R=43.25						
663.406 673.406 683.406 693.406 703.406 713.406 723.406	70.1195 60.4865 52.2551 45.2094 39.1694 33.9840	.009 .010 .012 .014 .017 .019 .026 .031 .036 .048 .055 .064 .075 .098 .112 .129	25.3444 25.7369 26.1312 26.5272 26.9250 27.3244 27.7255 28.1282 28.5324 28.9381 29.7539 30.1640 30.5753 30.9881 31.4021 31.8174 32.2339 32.66516 33.0705	260.938 262.865 264.778 266.678 268.565 270.438 272.300 274.149 275.986 277.811 279.625 281.428 283.220 285.001 286.772 288.532 290.283 292.024 293.755 295.478	10.6971 10.7467 10.7951 10.8424 10.8886 10.9337 11.0206 11.0624 11.1033 11.1431 11.1818 11.2565 11.2923 11.3613 11.3944 11.4966 11.4966	1.103 1.102 1.102 1.101 1.101 1.100 1.100 1.099 1.099 1.098 1.097 1.097 1.097 1.097	1.103 1.103 1.102 1.101 1.101 1.100 1.099 1.099 1.098 1.097 1.097 1.097 1.097	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	.00003146 .00003180 .00003247 .00003248 .00003313 .00003378 .00003411 .00003473 .00003506 .00003506 .00003506 .00003506 .00003506 .00003600 .00003750 .00003750 .00003750	. 04209 . 04283 . 04357 . 04452 . 04506 . 04580 . 04654 . 04728 . 04876 . 04950 . 05024 . 05024 . 05320 . 053394 . 053468 . 05542 . 05617	.765 .763 .762 .760 .755 .755 .755 .755 .749 .744 .744 .742 .738 .736 .738 .732 .730
					R=43.50						
670.223 680.223 690.223 700.223 710.223 720.223 740.223 750.223	81.4244 70.2967 60.7891 52.6440 45.6545 39.6477 34.4782 30.0228 26.1776 22.8544 19.9785	.009 .010 .012 .014 .017 .019 .023 .026	26.0C55 26.4010 26.7982 27.1971 27.5977 27.9998 28.4036 28.8088 29.2155	264.170 266.074 267.965 269.843 271.7C8 273.561 275.401 277.230 279.047	10.7798 10.8275 10.8740 10.9195 10.9638 11.0070 11.0492 11.0904 11.1305	1.102 1.101 1.101 1.100 1.100 1.099 1.099	1.102 1.101 1.101 1.100 1.100 1.099 1.099	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	.00003203 .00003236 .00003270 .00003303 .00003363 .00003400 .00003400 .00003400 .00003400	.04334 .04408 .04482 .04556 .04630 .04704 .04778 .04852 .04926	.762 .760 .759 .757 .755 .753 .752 .750 .748 .746
770.223 780.223 790.223 800.223	17.4865 15.3242 13.4456 11.8114 10.3881 9.1469 8.0633 7.1160 6.7224	.041 .047 .055 .063 .073 .084 .096	30.0333 30.4443 30.8566 31.2702 31.6851 32.1012 32.5185 32.9370	282.649 284.433 286.206 287.570 289.723 291.466 293.200 294.924	11.2077 11.2448 11.2810 11.3162 11.3505 11.3839 11.4164 11.4480	1.098 1.098 1.097 1.097 1.097 1.096 1.096	1.098 1.098 1.097 1.097 1.096 1.096	1.000 1.000 1.000 1.000 1.000 1.000	.00003524 .00003558 .00003650 .00003650 .00003711 .00003714 .00003770	.05074 .05149 .05223 .05297 .05371 .05445 .05519	.742 .741 .739 .737 .735 .733 .731 .729

T	v	p	H/RT <sub>o</sub>	A	$c_p/R$	γ	G	Z	μ	k	$N_{Pr}$
				S/4	R=43.75						
687.325 697.325 707.325 717.325 727.325 747.325 747.325 757.325 767.325 787.325	61.0933 53.0342 46.1011 40.1282 34.9755 30.5240 26.6732 23.3376 20.4444	.009 .011 .012 .015 .017 .020 .023 .026 .035 .041 .047 .054	26.6829 27.0813 27.4814 27.8831 28.2864 28.0975 29.5053 29.5053 29.5053 29.7370 31.1502 31.5647 31.9805 32.3975 32.8157	267.418 269.299 271.168 273.024 274.868 276.700 278.521 280.330 282.128 283.915 285.691 287.457 289.213 290.559 292.695	10.8607 10.9064 10.9510 10.9946 11.0785 11.1189 11.1583 11.1967 11.2341 11.2706 11.3061 11.3743 11.4700 11.4389	1.101 1.100 1.100 1.100 1.009 1.099 1.098 1.098 1.097 1.097 1.097 1.096 1.096	1.101 1.101 1.100 1.100 1.100 1.099 1.098 1.098 1.097 1.097 1.097 1.096 1.096	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	.00003391 .00003423 .00003455 .00003487 .00003518	.04461 .04535 .04609 .04683 .04757 .04831 .04905 .05053 .05127 .05201 .05275 .05349 .05423 .05571	.759 .757 .756 .756 .754 .750 .749 .747 .743 .741 .737 .733 .733 .733 .733
				s/I	R=44.00						
704.716 714.716 724.716 734.716 744.716	53.4269 46.5505 40.6121 35.4768 31.0300 27.1745 23.8271 20.9174 18.3848 16.1777 14.2521 12.5699 11.0987	.009 .011 .013 .015 .017 .020 .023 .027 .031 .035 .041 .047	27.3769 27.7782 28.1810 28.5855 28.9914 29.3988 29.8076 30.2178 30.6294 31.0423 31.4565 31.8719 32.2886 32.7065 33.1255	270.681 272.541 274.388 276.223 278.046 279.853 281.659 283.448 285.227 286.996 288.154 290.502 292.240 293.968	10.9395 10.9833 11.0261 11.0678 11.1085 11.1481 11.2244 11.2611 11.2969 11.3317 11.3656 11.3985 11.4306 11.4619	1.101 1.100 1.009 1.099 1.098 1.098 1.097 1.097 1.097 1.096 1.096 1.096	1.101 1.100 1.100 1.099 1.099 1.098 1.098 1.097 1.097 1.096 1.096	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	.00003317 .00003350 .00003383 .00003445 .00003447 .00003510 .00003541 .00003541 .00003694 .00003694 .00003694 .00003754 .00003754	.04589 .04663 .04737 .04811 .04886 .04960 .05034 .05108 .05156 .05256 .05330 .05404 .05478 .05525 .05626	.756 .754 .753 .751 .747 .745 .743 .742 .740 .738 .736 .734 .732 .730 .728
				\$/9	R=44.25						
722.413 732.413 742.413 752.413 762.413 772.413 802.413 802.413 812.413 822.413 832.413 842.413	53.8141 46.9956 41.0931 35.9769 31.5364 27.6775 24.3197 21.3944	.010 .011 .013 .015 .017 .020 .023 .027 .031 .035 .041	28.0881 28.4922 29.3048 29.7133 30.1232 30.5345 31.3610 31.7762 32.1926 22.6101 33.0289	273.963 275.801 277.627 279.441 281.244 283.036 284.817 286.588 288.348 290.098 291.838 293.568 295.289	11.0163 11.0583 11.0992 11.1391 11.2780 11.2528 11.2528 11.3237 11.3578 11.3910 11.4233 11.4547	1.100 1.099 1.099 1.098 1.098 1.097 1.097 1.096 1.096 1.096	1.100 1.099 1.099 1.098 1.098 1.097 1.097 1.097 1.096 1.096	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	.00003375 .00003407 .00003439 .00003503 .00003553 .00003565 .00003627 .00003687 .00003717 .00003717 .00003747	.04720 .04794 .04868 .04943 .05017 .05091 .05165 .05239 .05313 .05387 .05461 .05535	.753 .751 .748 .746 .744 .742 .740 .738 .736 .734 .733 .731 .728

T	. <b>v</b>	p	H/RT <sub>o</sub>	A	$c_p/R$	γ	G	Z	μ	k	$\mathtt{N}\mathbf{p_r}$	
S/R=44.50												
740.440 750.440 760.440 770.440 780.440 800.440 810.440 820.440 830.440	61.9820 54.1838 47.4261 41.5624 36.4680 32.0362 28.1763 24.8101 21.8711 19.3020	.010 .011 .013 .015 .018 .020 .023 .027 .031 .035	28.8176 29.2244 29.6326 30.0422 30.4532 30.8656 31.2792 31.6942 32.1103 32.5277 32.9462	277.267 279.083 280.889 282.683 284.466 286.238 288.000 289.752 291.494 293.226 294.948	11.0912 11.1313 11.1704 11.2084 11.2455 11.2817 11.3169 11.3512 11.3845 11.4170	1.099 1.099 1.098 1.098 1.097 1.097 1.097 1.096 1.096	1.099 1.099 1.098 1.098 1.097 1.097 1.097 1.096 1.096	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	.00003433 .00003465 .00003496 .00003528 .00003559 .00003620 .00003651 .00003711 .00003711 .00003771	.04854 .04928 .05002 .05076 .05150 .05224 .05298 .05372 .05446 .05520	.750 .748 .746 .744 .742 .741 .739 .737 .735 .733 .731 .729	
S/R=44.75												
758.772 768.772 778.772 788.772 798.772 808.772 818.772 828.772 838.772	81.4244 71.1582 62.2691 54.5591 47.8619 42.0372 36.9649 32.5425 28.6821 25.3081 23.4803	.010 .012 .013 .015 .018 .020 .023 .027	29.5644 29.9738 30.3846 30.7967 31.2102 31.6249 32.0408 32.4580 32.8763	280.588 282.384 284.168 285.943 287.706 289.459 291.203 292.936 294.660	11.1639 11.2022 11.2394 11.2757 11.3111 11.3455 11.3790 11.4116 11.4433	1.098 1.098 1.098 1.097 1.097 1.096 1.096	1.098 1.098 1.098 1.097 1.097 1.096 1.096	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	.00003491 .00003523 .00003554 .00003615 .00003646 .00003676 .00003706 .00003766	. C4990 .05064 .05138 .05212 .05286 .05360 .05434 .05508	.746 .745 .743 .741 .739 .737 .735 .733 .731 .729	
S/R=45.00												
767.414 777.414 787.414 797.414 807.414 817.414 827.414 837.414 844.814	71.3324 62.5646 54.9417 48.3046 42.5189 37.4691 33.0564	.010 .012 .014 .016 .018 .021	30.3287 30.7407 31.1539 31.5685 31.9843 32.4013 32.8194	283.926 285.702 287.467 289.221 290.966 292.700 294.425	11.2344 11.2708 11.3063 11.3409 11.3745 11.4072 11.4391	1.098 1.097 1.097 1.096 1.096 1.096	1.098 1.097 1.097 1.096 1.096 1.096	1.000 1.000 1.000 1.000 1.000 1.000	.00003549 .00003580 .00003611 .00003642 .00003672 .00003702 .00003762 .00003784	.05128 .05202 .05276 .05350 .05424 .05498	.743 .741 .739 .737 .735 .733 .732 .730	
				\$/!	R=45.25							
796.380 806.380 816.380 826.380 836.380		.010 .012 .014 .016	31.1112 31.5256 31.9412 32.3581 32.7762	287.284 289.040 290.785 292.520 294.246	11.3027 11.3373 11.3710 11.4039 11.4358	1.097 1.097 1.096 1.096	1.097 1.097 1.096 1.096 1.096	1.000 1.000 1.000 1.000	.00003608 .00003639 .00003669 .00003699 .00003729 .00003759 .00003784	.05268 .05342 .05416 .05490	.739 .737 .736 .734 .732 .730	
S/R=45.50												
815.715 825.715 835.715	81.4244 71.6563 63.1324 55.6867 49.7277	.011 .012 .014	31.9135 32.3303 32.7483	290.669 292.404 294.131	11.3688 11.4017 11.4337	1.096 1.096 1.096	1.096 1.096 1.096	1.000 1.000 1.000	.00003667 .00003697 .00003727 .00003757	.05411 .05485 .05559	.736 .734 .732 .730 .728	
				S/1	R=45.75							
835.376	81.4244 71.8200 63.8611	.011	32.7341	294.C72	11.4326	1.096	1.096	1.000	.00003726 .00003756 .00003784	.05557	.732 .730 .728	

TABLE II.- TRANSPORT PROPERTIES OF CF4 AT CONSTANT TEMPERATURE

[Temperatures are in kelvins]

4														
· <b>v</b>	$\mu$	k	$c_n/R$	$c_{f v}/R$	$N_{\mathbf{pr}}$		v	$\mu$	k	$c_{f p}/{f R}$	$\mathrm{c_v/R}$	$\mathtt{N_{Pr}}$		
	·		P/	**						r,	•			
	T- 100							T- 400						
	T≈ 100						T= 400							
							*							
.1000	.00000604	.00123	5.3491	3.4394	2.483		8.0000	.00002213	.02333	8.7112	7.7115	.781		
	.00000600		4.6727	3.2977				.00002213		8.7111	7.7115	.781		
	.00000598		4.3980	3.2264				.00002213		8.7110	7.7115	.781		
	.00000598		4.3136	3.2026				.00002213		8.7109	7.7114	. 781		
	.00000597		4.2726 4.2484	3.1907 3.1835				.00002213		8.7108 8.7108	7.7114 7.7114	.781 .781		
	.CC000597		4.2008	3.1692			80.0000	.00002213	• 02333	6.1100	141114	• 101		
	.00000597		4.1774	3.1620										
	.00000597		4.1696	3.1596					T= 60	00				
8.0000	.00000597	.00111	4.1657	3.1584	2.107									
	.00000597		4.1634	3.1577										
	.00000597		4.1588	3.1563				.00003916			9.4469	.889		
	.00000557		4.1565	3.1556				.00003310			9.4445	• 821		
	.00000557		4.1557	3.1553				.00003171			9•4430 9•4422	.801 .793		
80.0000	.00000597	.00111	4.1553	3.1552	2.104			.00003115			9.4417	.788		
								.00003037			9.4405	.781		
		T= 20	0					.00003014			9.4399	.777		
								.00003007			9.4397	.776		
							.0800	.00003004	·C3828	10.4647	9.4396	.776		
	.00001369		9.2873	5.7094				.00003002			9.4395	• 775		
	.00001260		7.1771	5.2753	.937			.00002998			9.4394	. 775		
	.00001237		6.4287	5.0430	.853			.00002996			9 • 43 9 3	•775		
	.00001230		6.2078 6.1019	4.9633	.828			.00002996			9.4393 9.4393	•774 •774		
	.00001225		6.0397	4.8988	.810			.00002995			9.4393	.774		
	.00001221		5.9181	4.8500	.796			.00002995			9.4393	.774		
	.00001219		5.8586	4.8254	.790			.00002995			9.4393	.774		
•6000	.00001219	·0C854	5.8390	4.8172	.788			.00002995			9.4393	.774		
.8000	.00001219	.00853	5.8292	4.8131	.786		8.0000	.00002995	.03814	10.4389	9.4393	• 774		
	.00001218		5.8234	4.8106	. 786			.00002995			9 • 43 93	• 774		
	.00001213		5.8117	4.8057	. 785			.00002995			9.4393	• 774		
	.00001218		5.8059	4.8032	. 784			.00002995			9.4393	•774		
	.00001218		5.8039 5.8030	4.8024	• 784 • 784			.00002995 .00002995			9.4393 9.4393	•774 •774		
	.00001218		5.8024	4.8017	.784		80.0000	•00002993	•03014	10.4500	7 6 73 73	•117		
	.00001218		5.8012	4.8012	. 784									
	.00001218		5.8006	4.8010	.783				T= 80	30				
60.0000	.00001218	·00852	5.8004	4.8009	.783				, .					
80.0000	.00001218	·CC852	5.8003	4.8008	.783					•				
								.00004571				.832		
								.00003965				• 774		
		T= 4.0	00					.00003826				.758		
								.00003770				.751 .748		
• 00 20	.00003134	.03211	10.5876	7.8827	. 976			.00003741				.742		
	.00002529		9.7776	7.8280	.870			.00003669				.739		
	.00002390		9.4129	7.7960	.833			.00003662				.738		
.0080	.00002333	•02492	9.2294	7.7774	.817		• 08 00	.00003659	· C5309	11.3345	10.3160	.738		
	.00002364		9 <b>.</b> 120 <b>9</b>	7.7654	.808			.00003657				.738		
	.00002255		8.9101	7.7396	• 793			.00003653				.737		
	.00002233		8.8088	7.7258	.787			.00003651				. 737		
	.00002222		8.7757 8.7594	7.7211 7.7187	• 784 • 783			.00003651				•737		
	.00002222		8.7496	7.7173	.783			.00003650				•737 •737		
	.00002216		8.7301	7.7144	. 782			.CO003650				.737		
	.00002215		8.7204	7.7129	.781			.00003650				.737		
	.00002214		8.7172	7.7124	. 781			.00003650				.737		
	.00002214		8.7156	7.7122	.781		8.0000	.00003650	.05295	11.3155	10.3160	.737		
	.00002214		8.7146	7.7120	. 781			.00003650				.737		
	.00002213		8.7127	7.7117	.781			.00003650				• 737		
	.00002213		8.7117	7.7116	.781			.00003650				.737		
0.0000	.00002213	.02333	8.7114	7.7115	. 781			.00003650				•737		
							-90-0000	.00003650	• 45245	11.5155	10.2100	.737		

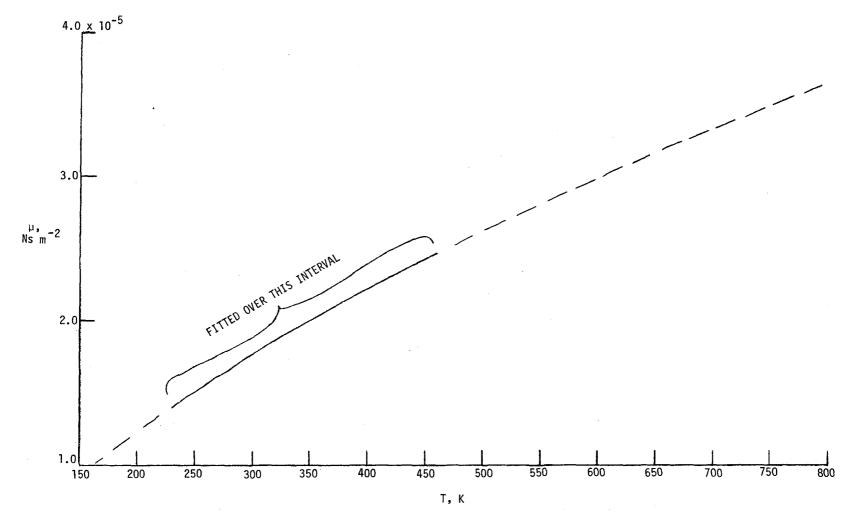


Figure 1.- Viscosity of  $CF_4$  at a pressure of 1 atmosphere.

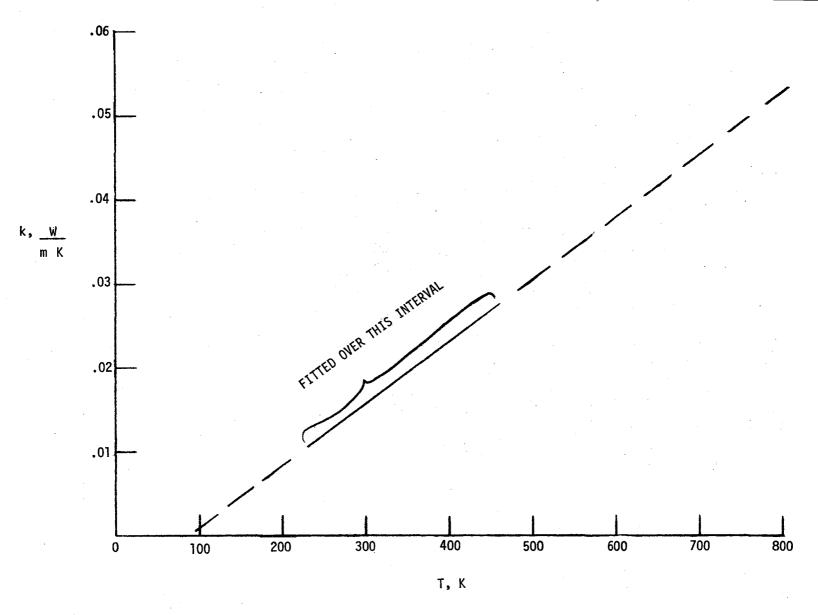


Figure 2.- Thermal conductivity of  ${\rm CF_4}$  at a pressure of 1 atmosphere.

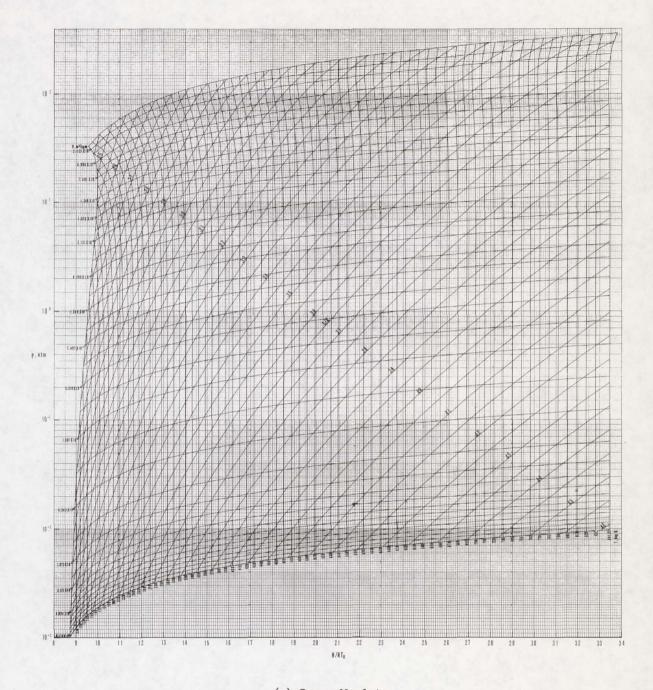
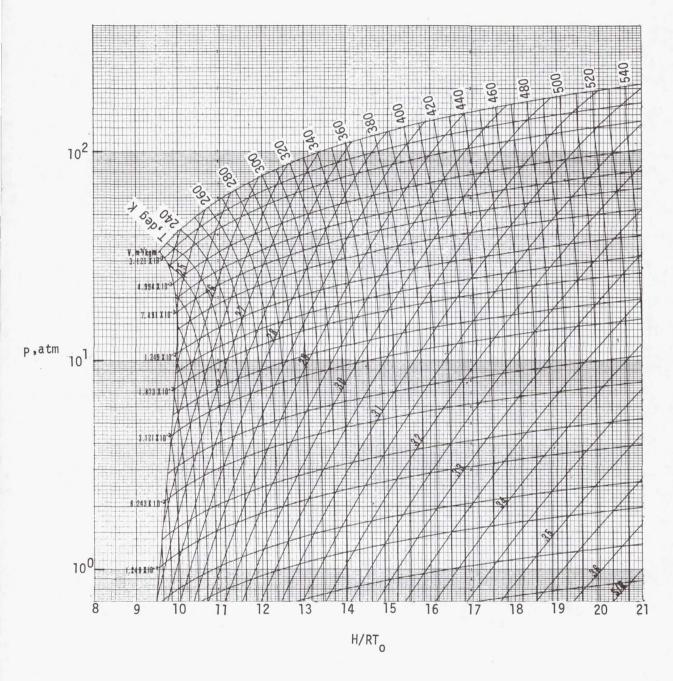
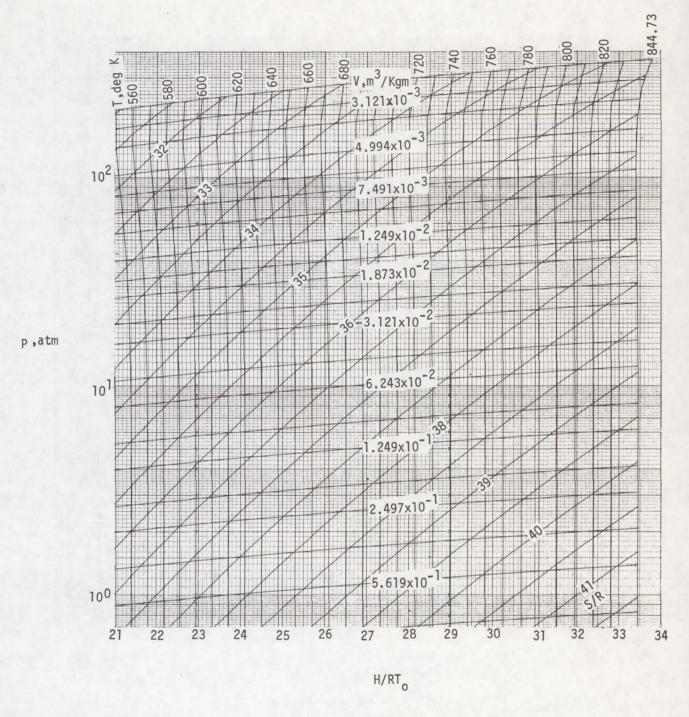


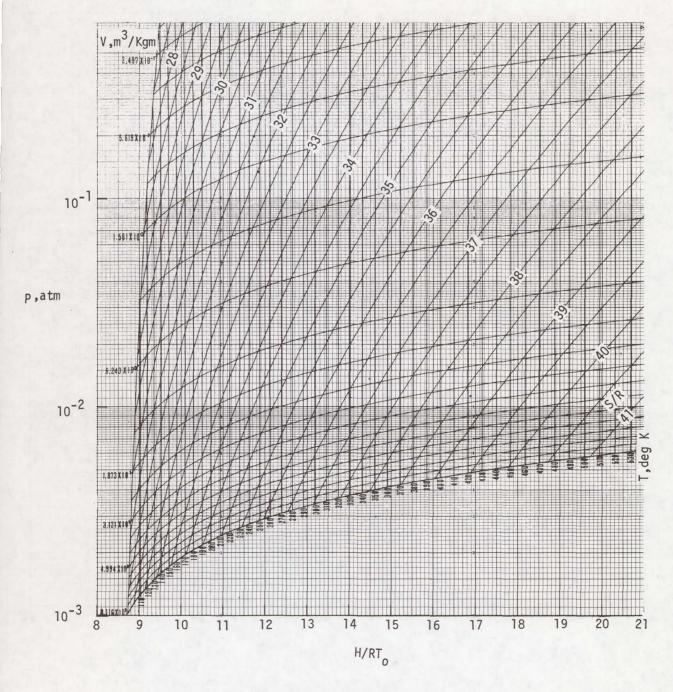
Figure 3.- Pressure enthalpy diagram for CF<sub>4</sub> with lines of constant entropy, volume, and temperature.



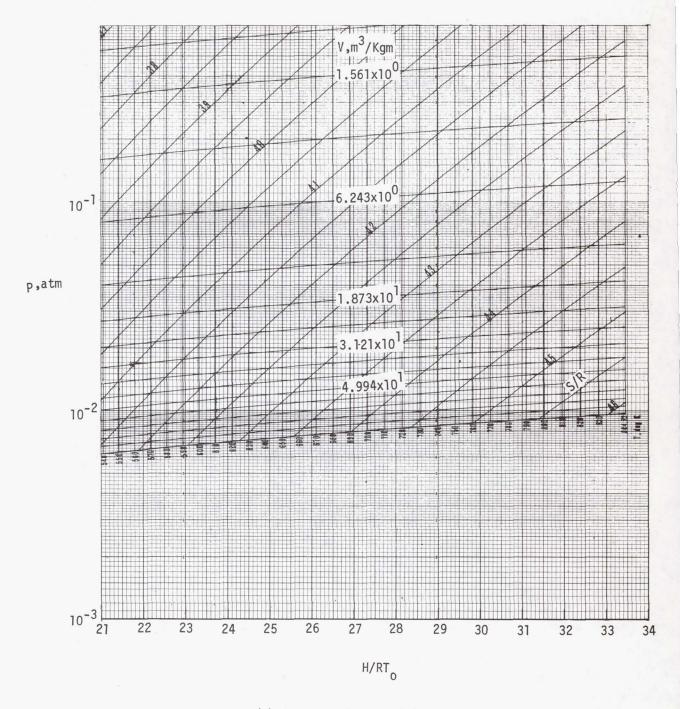
(b) Upper left quadrant.Figure 3.- Continued.



(c) Upper right quadrant.
Figure 3.- Continued.



(d) Lower left quadrant. Figure 3.- Continued.



(e) Lower right quadrant. Figure 3.- Concluded.

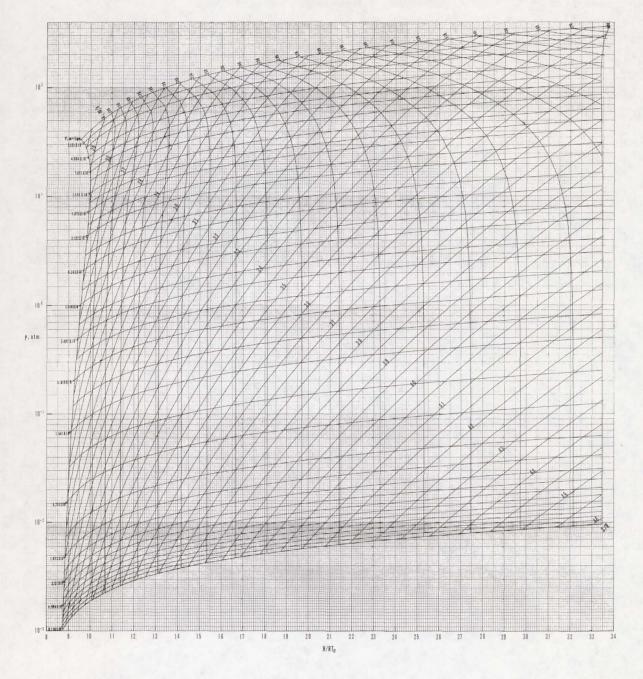
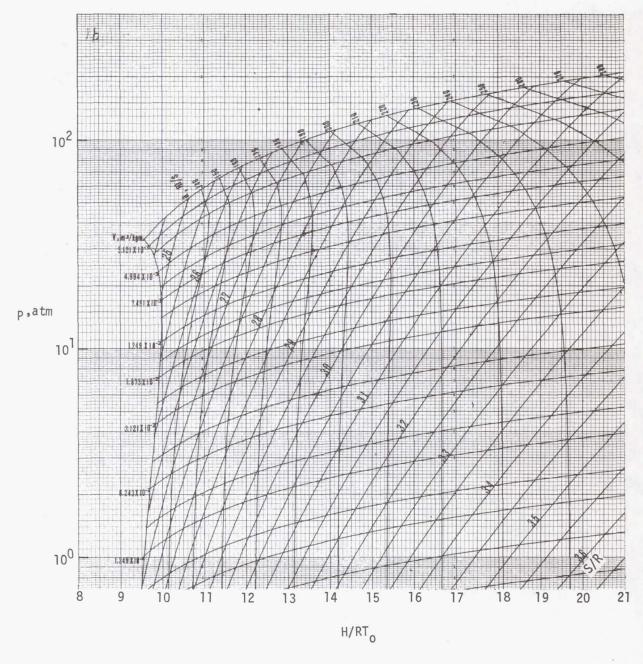
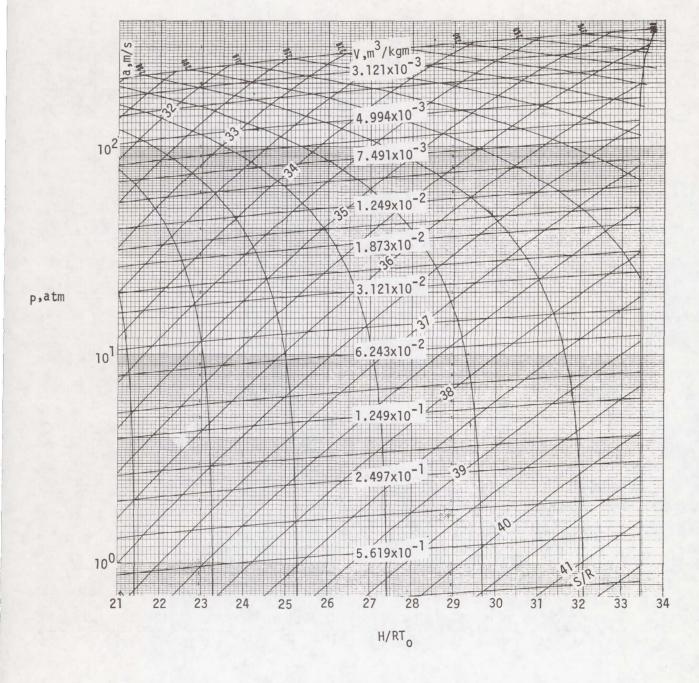


Figure 4.- Pressure enthalpy diagram for  $\text{CF}_4$  with lines of constant entropy, volume, and speed of sound.

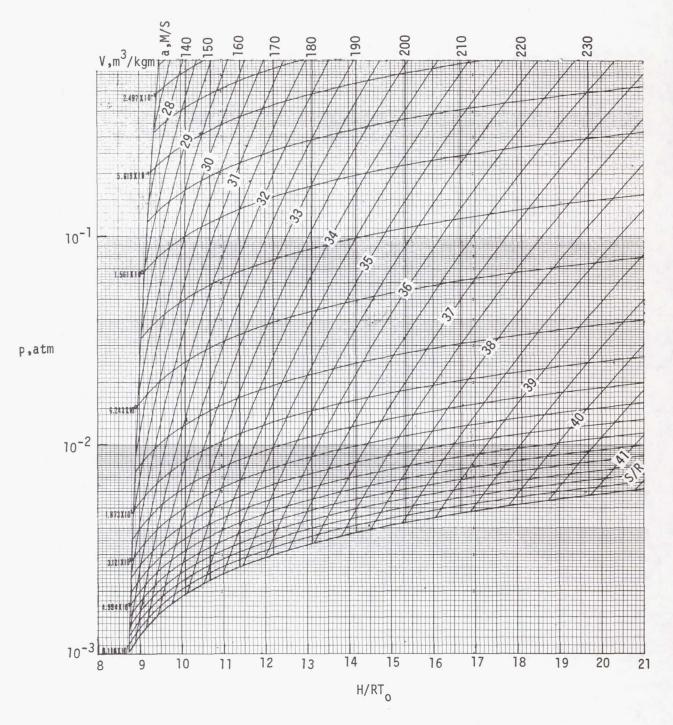


(b) Upper left quadrant.

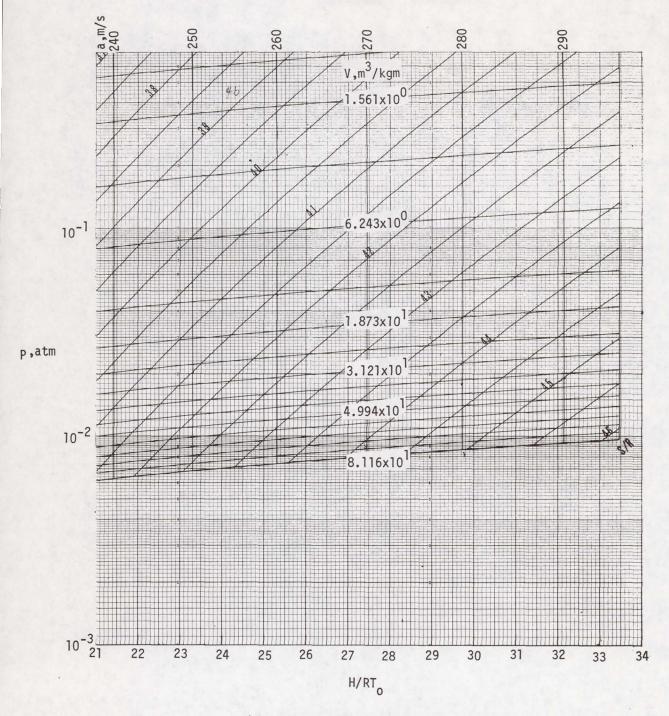
Figure 4.- Continued.



(c) Upper right quadrant.
Figure 4.- Continued.



(d) Lower left quadrant. Figure 4.- Continued.



(e) Lower right quadrant.

Figure 4.- Concluded.

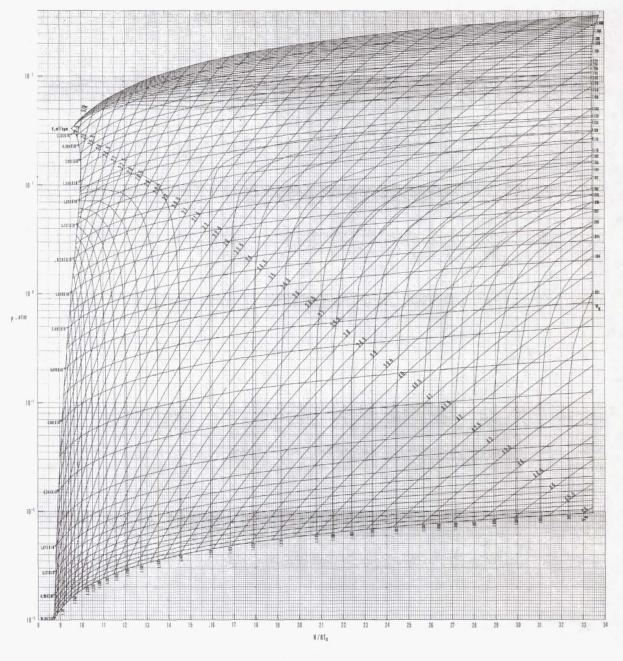
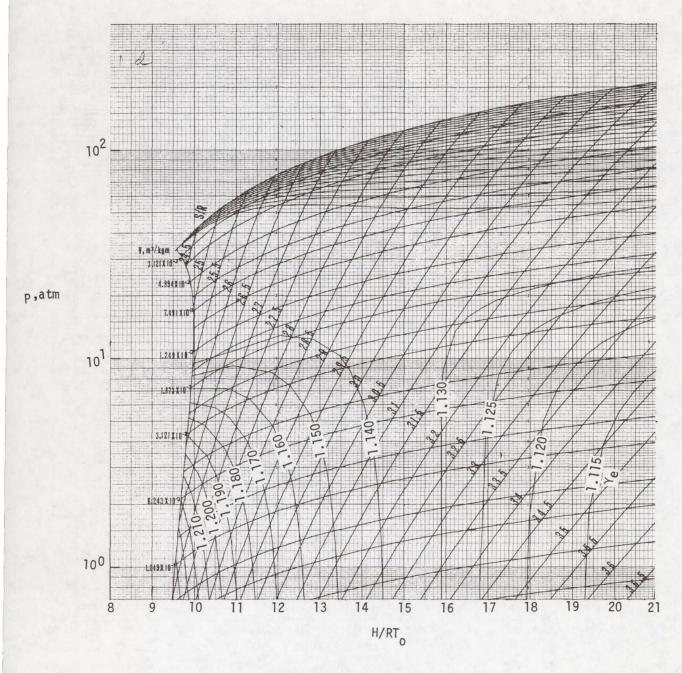
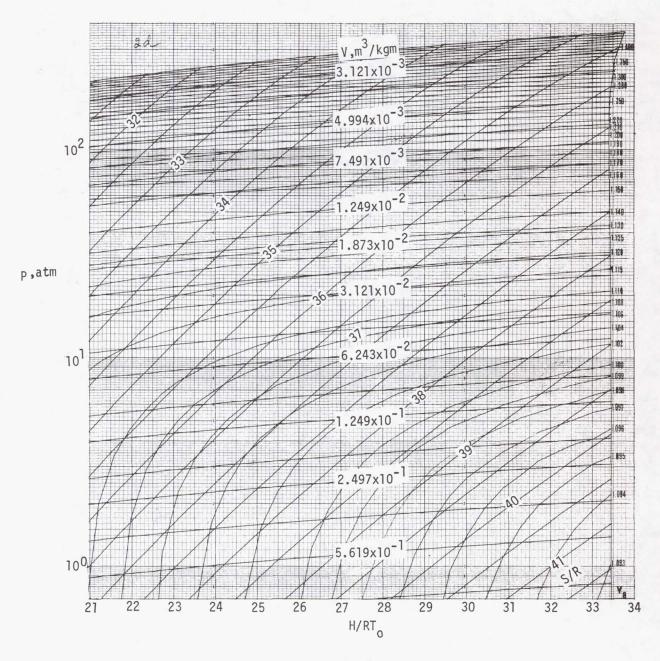


Figure 5.- Pressure-enthalpy diagram for  ${\rm CF}_4$  with lines of constant entropy, volume, and isentropic exponent.

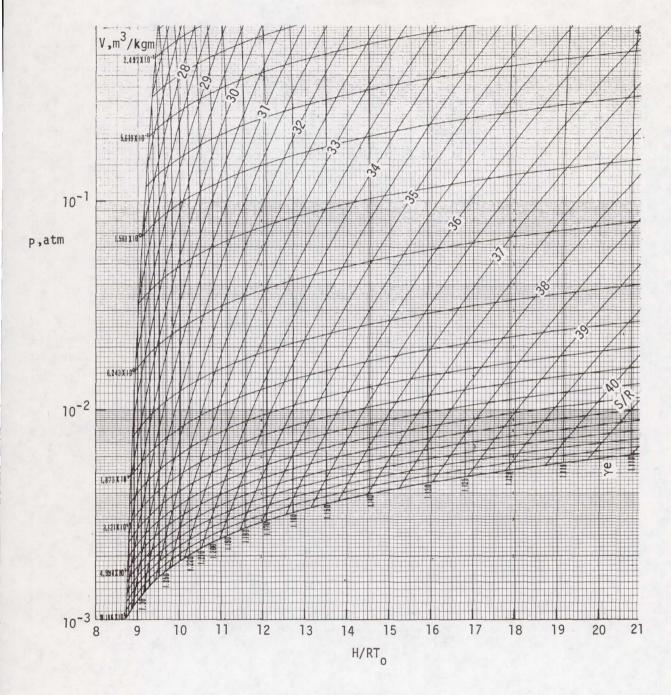


(b) Upper left quadrant. Figure 5.- Continued.



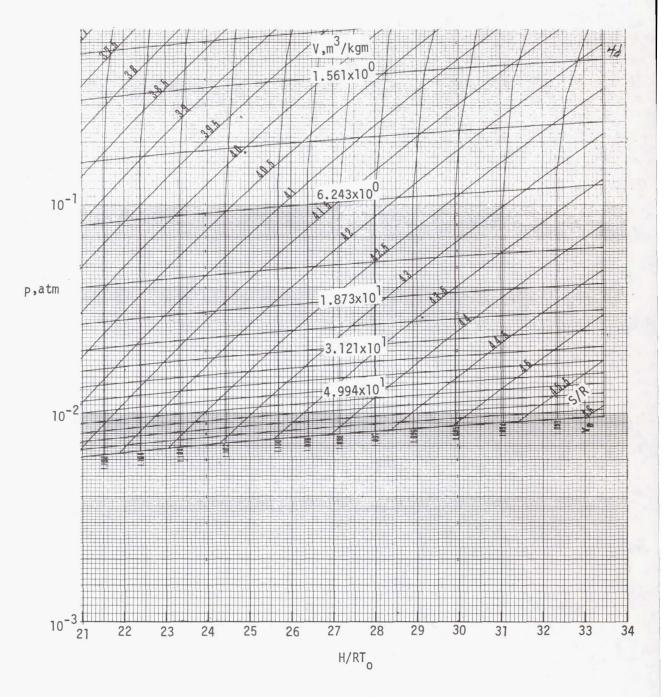
(c) Upper right quadrant.

Figure 5.- Continued.



(d) Lower left quadrant.

Figure 5.- Continued.



(e) Lower right quadrant.

Figure 5.- Concluded.

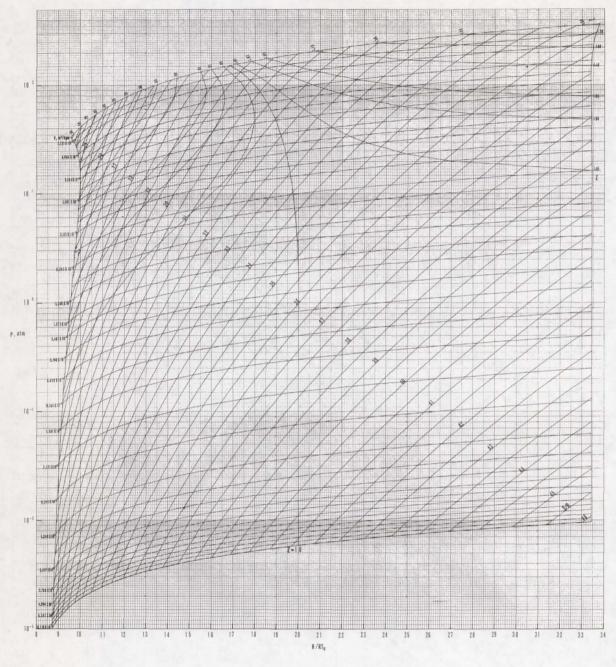
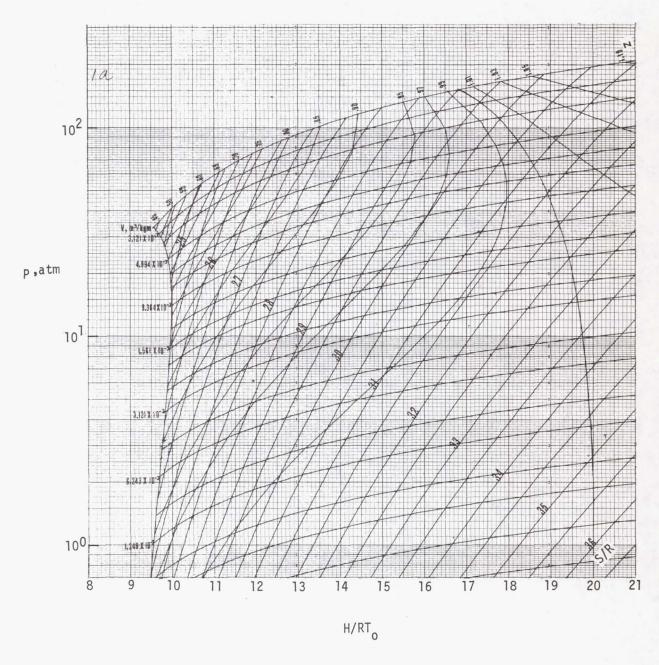
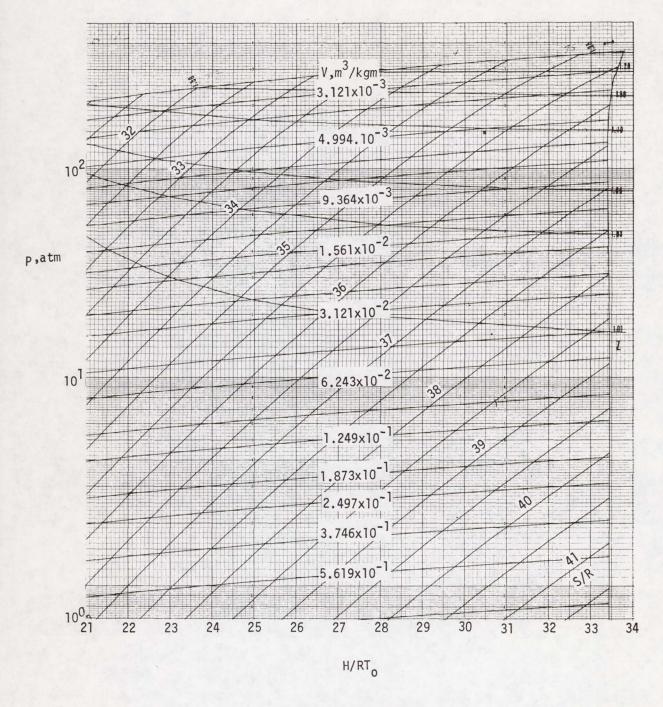


Figure 6.- Pressure enthalpy diagram for  $CF_4$  with lines of constant entropy, volume, and compressibility factor.



(b) Upper left quadrant. Figure 6.- Continued.



(c) Upper right quadrant.

Figure 6.- Continued.

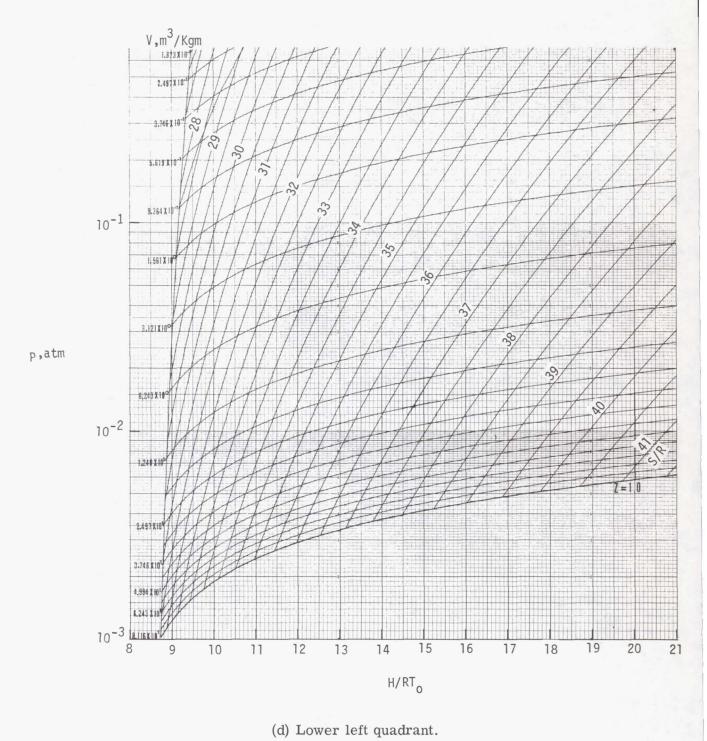
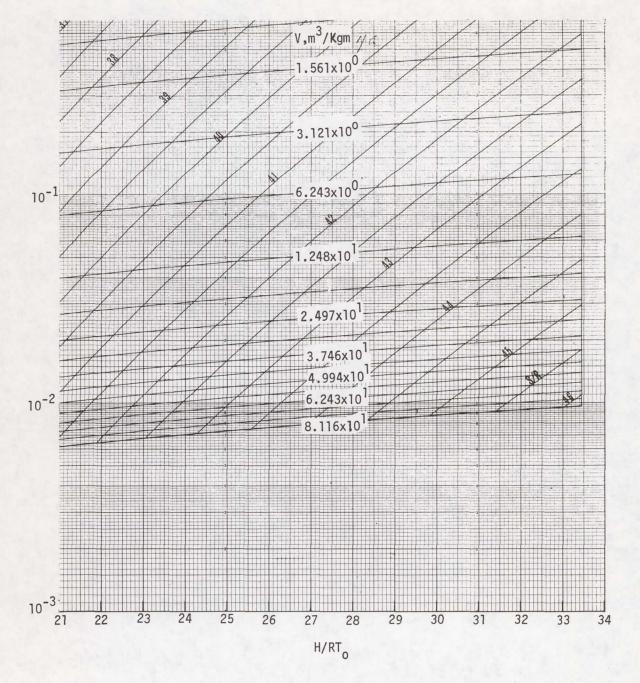


Figure 6.- Continued.



(e) Lower right quadrant. Figure 6.- Concluded.

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